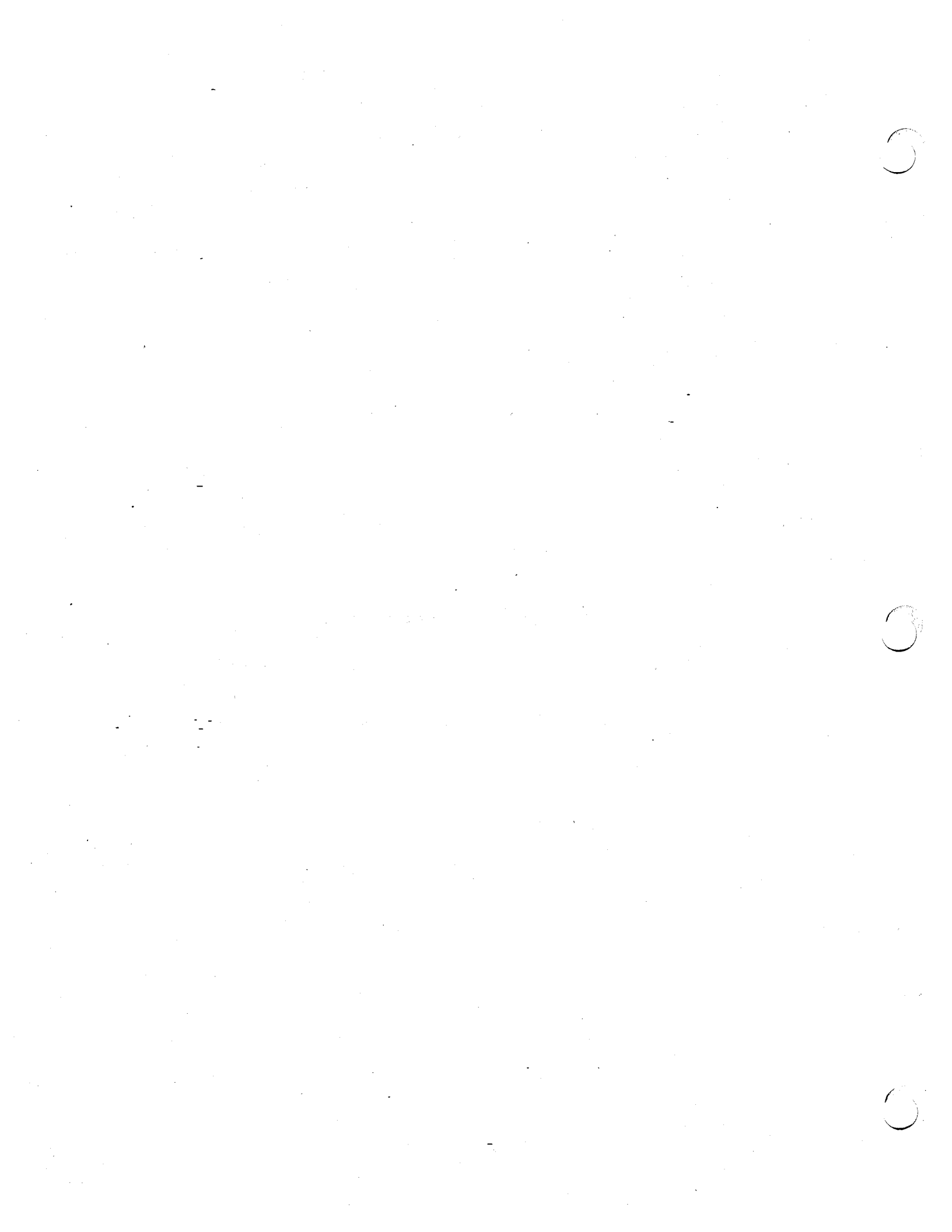


US EPA ARCHIVE DOCUMENT

**APPENDIX F – ATTACHMENT 3**

Analysis of Effluent Dissolved Oxygen Demand



## Analysis of Effluent Dissolved Oxygen Demand

Attached are the equations and descriptions of methods used to calculate the requested oxygen depression values due to the effluent. The information contained herein supports the answers provided in Part II-B of the application.

### Initial Dilution

The dissolved oxygen concentration immediately following initial dilution is calculated using the following equation:

$$DO_f = DO_a + \frac{(DO_e - IDOD - DO_a)}{S_a}$$

where:

- $DO_f$  = Final dissolved oxygen concentration of the receiving water at the plume trapping level (mg/L)
- $DO_a$  = Ambient dissolved oxygen concentration averaged from the diffuser port depth to the trapping level (mg/L) (assumed minimum of 5.848 mg/L)
- $DO_e$  = Dissolved oxygen concentration of the treatment plant effluent (mg/L) (assumed to be 0 mg/L)
- $IDOD$  = Immediate dissolved oxygen demand (mg/L) (assumed to be 5.0 mg/L)
- $S_a$  = Minimum initial dilution = 210

The dissolved oxygen water quality standard is expressed as a percent difference from ambient conditions. As a result, critical periods are expected to occur when ambient concentrations are low. However, the dissolved oxygen concentration immediately following initial dilution is calculated in this section using ambient concentrations from each quarterly receiving water sample. The above method yields a reduction of 0.052 mg/L or 0.88 percent. Field data show that reductions can be somewhat higher (up to 0.213 mg/L or 3.5 percent), but still far above levels that would violate water quality standards in Hawaii, which are based on the percent saturation (82.3 percent saturation versus a 75 percent standard).

The Amended Section 301(h) Technical Support Document (EPA, 1994) (TSD) indicates that the least favorable combination of parameter values should be used. The following values remained constant throughout the calculations. Dissolved oxygen concentration of the

effluent is assumed to be 0 mg/L, which is a conservative value, and IDOD was assumed to be 5.0 mg/L, based on primary treatment and a travel time of 100 minutes with an effluent BOD of 200 mg/L (worst-case assumption). Peak month flow rates result in a minimum initial dilution of 210:1, assuming a peak daily flow rate of 46.96 (in the year 2010) mgd and assuming receiving water density data from the month of January (actual peak flow projected to occur in March). Control sample station data used to calculate  $DO_a$  and  $DO_t$  are HB1 from Honouliuli monitoring program water column sampling. (See Table III.A.3-1 for initial dilution estimates.)

Ambient dissolved oxygen concentrations are averaged over the height of rise of the plume for each of the sampling dates. Dissolved oxygen concentrations are interpolated at the plume trapping level depth of 48.0 m below the surface (occurs in March, but there is no March profile to use and January is the worst case).

In Hawaii, water quality standards for dissolved oxygen are based on the federal regulations, which calculate percent dissolved oxygen depression using the following equation (Baumgartner, 1981):

$$DO_a (\%) = (DO_t + IDOD - DO_d) / (S_a \times DO_d)$$

The results using this equation show a depression of 1.86 percent. Actual field monitoring data for the Honouliuli discharge show a slightly higher percentage difference between the upcurrent reference station and the edge of the Zone of Mixing (ZOM), as summarized in Table F-1.

**Table F-1. Measured Dissolved Oxygen Depression Resulting from Honouliuli discharge**

Monitoring Date	Depth	Minimum DO, mg/L (% Saturation)		Difference, mg/L	Difference (percent depression)
		HB1	HM4		
17 Jan 1995	28m	5.933 (85.62)	5.708 (82.31)	0.255	3.8
3 Nov 1994	30m	5.860 (89.36)	5.709 (86.50)	0.150	2.6
15 Jul 1994	1m	6.202 (93.66)	6.016 (90.70)	0.180	3.0
14 Apr 1994	48m	6.361 (91.00)	6.250 (89.83)	0.110	1.7

The minimum dissolved oxygen value for the ZOM station was used for each comparison; often this was not at the trapping depth, but the worst case was taken for each situation.

As evidenced in Table F-1, the methods used to calculate the percent change in dissolved oxygen concentrations yield similar results for the theoretical calculation and the actual field data. This shows that the field monitoring program is accomplishing what can be predicted based on worst-case conditions.

### Farfield Oxygen Demand

EPA guidelines suggest that applicants calculate farfield oxygen demand based on use of equations. There is no substitute for actual monitoring data, and since the City has a good data base, this is used to address the farfield oxygen demand. Table F-1 presents data showing oxygen values at the upcurrent reference station (HB1) and compares this with data from the downcurrent ZOM station HM4. This provides one good way to show what actual dissolved oxygen suppression is in the field. These numbers were used in earlier calculations and clearly indicate that saturation is always maintained above 82 percent under worst-case conditions throughout the entire water column.

### Farfield Oxygen Demand

The following equation is used to estimate farfield dissolved oxygen demand:

$$DO(t) = DO_a + \frac{DO_f - DO_a}{D_s} - \frac{L_{fc}}{D_s} 1 - \exp(-k_c t) - \frac{L_{fn}}{D_s} 1 - \exp(k_n t)$$

where:

DO(t) = Dissolved oxygen concentration in a submerged wastefield as a function of travel time t, (mg/L)

DO<sub>a</sub> = Affected ambient dissolved oxygen concentration immediately updrift of diffuser (mg/L)

k<sub>c</sub> = CBOD decay rate coefficient

k<sub>n</sub> = NBOD decay rate coefficient

L<sub>fc</sub> = Ultimate CBOD concentration at completion of initial dilution (mg/L)

L<sub>fn</sub> = Ultimate NBOD concentration above ambient at the completion of initial dilution (mg/L)

D<sub>s</sub> = Dilution attained subsequent to initial dilution as a function of travel time.

The following assumptions are made in using the above equation to estimate the farfield dissolved oxygen depletion:

- Oxygen depletion is a function of distance from the discharge and is caused by carbonaceous oxygen demand. Because the discharge is into open coastal waters, the effects of nitrogenous oxygen demand are negligible.
- The wastewater plume does not surface during the critical case.

- The discharge is to an open coastal area, so the lateral diffusion coefficient increases as the 4/3 power of the wastefield width.
- The wastefield entrains ambient water as a function of travel time. Lateral diffusion is the predominant mechanism of entrainment.

Ambient dissolved oxygen concentrations averaged over the plume height of rise are calculated in the previous section. The critical ambient concentrations are calculated to occur in January when minimum  $DO_a$  is 5.848 mg/L and  $DO_f$  is measured to be 5.796 mg/L in January. In order to calculate  $k_c$ , the ambient temperature must be determined. This is estimated by averaging recorded temperatures over the height of rise of the plume. The decay rates are then corrected for temperature. In January,  $k_c$  is estimated to be 0.160/day.

$L_{fc}$  is defined as the following:

$$L_{fc} = 1.46 \times BOD_f$$

where:

$$BOD_f = \text{Final } BOD_5 \text{ concentration (mg/L)}$$

$BOD_f$  can be calculated using the following equation:

$$BOD_f = BOD_a + (BOD_e - BOD_a)/S_a$$

where:

$$BOD_a = \text{Ambient } BOD_5 \text{ concentration in the receiving water (mg/L)}$$

$$BOD_e = \text{Maximum monthly average } BOD_5 \text{ concentration (mg/L)}$$

$$S_a = \text{Initial dilution at the average flow rate}$$

$BOD_5$  monitoring of the receiving water was not required, so this value ( $BOD_a$ ) is assumed to be 0 mg/L. EPA indicates that the maximum monthly average effluent  $BOD_5$  concentration should be used with the initial dilution at the average flow rate. The projected peak month  $BOD_e$  concentration for 2000 is 238 mg/L and  $S_a$  is 210.  $BOD_f$  is 1.13 mg/L and consequently  $L_{fc}$  is assumed to be 1.66 mg/L for this calculation.

### **Sediment Oxygen Demand and Resuspension**

The dissolved oxygen depletion due to a steady sediment oxygen demand can be predicted by the following equation:

$$\Delta DO = \frac{\bar{S}_B X_M}{86,400 \text{ UHD}} = \frac{a \bar{S} k_d X_M}{86,400 \text{ UHD}}$$

where:

$\Delta DO$  = Oxygen depletion, mg/L

$\bar{S}_B$  = Average benthic oxygen demand over the deposition area, g  $O_2/m^2/day$

$X_M$  = Length of deposition are (generally measured in longshore direction, m)

$H$  = average depth of water column influenced by sediment oxygen demand, measured above bottom, m

$U$  = minimum sustained current speed over deposition area, m/sec

$k_d$  = sediment decay rate constant, 0.01/day

$a$  = oxygen:sediment stoichiometric ratio, 1.07 mg  $O_2/mg$  sediment

$\bar{S}$  = average concentration of deposited organic sediments over the deposition area, g/m<sup>2</sup>

$D$  = Dilution caused by horizontal entrainment of ambient water as it passes over the deposition area (always  $\geq$ ).

For the purposes of this approximation, the following values are used. The stoichiometric ratio  $a$  is 1.07.  $\bar{S}$  is estimated at 25g/m<sup>2</sup> based on flows from 2020 MER and January 1995 model results for steady state organics accumulation for the total area of deposition and total mass remaining. The sediment decay rate constant  $k_d$  is 0.01/day.  $X_M$  measures approximately 3,000 m, and  $U$  is .03 m/sec. A depth for  $H$  is calculated using the following equation:

$$H = 0.08 \left( \frac{e_z x_M}{U} \right)^{1/2}$$

When  $e_z$  is assumed to be 1 cm<sup>2</sup>/sec, then  $H$  is 2.53m.  $D$  is determined from Table B-5 of the TSD.

Using the above values, the maximum  $DO_{ss}$  is calculated to be .122 mg/L occurring at  $t = 2$  hours. This represents a 2.1 percent reduction in the dissolved oxygen concentration at the bottom resulting from sediment steady-state oxygen demand.



Dissolved oxygen depression resulting from sediment resuspension can be estimated using the following equation:

$$\Delta DO = \frac{\bar{S}_r}{DH} \left[ 1 - \exp\left(\frac{-k_r t}{24}\right) \right]$$

where:

$\Delta DO$  = Oxygen depletion, mg/L

$\bar{S}_r$  = Average concentration (in g/m<sup>2</sup>) of resuspended organic sediment (based on 90-day accumulation)

H = Depth of water volume containing resuspended materials, m

$k_r$  = Decay rate of resuspended sediments, 0.1/day

t = Elapsed time following resuspension, h (t varies from 0 to 24 h)

D = Dilution as defined previously (generally set equal to 1)

$\bar{S}_r$  can be approximated as the average concentration over the width of the deposition zone (EPA, 1982). This value is assumed to be 25g/m<sup>2</sup> based on 90-day accumulation and averaged by total mass over all model cells with accumulation (see Figure III.A.5.4). H is a function of travel time and is calculated using the following equation:

$$H = \frac{1.6}{100} (3,600 t \varepsilon'_z)^{1/2}$$

It is assumed that  $\varepsilon'_z$  is 5 cm<sup>2</sup>/sec,  $k_r$  is 0.01/day. The travel time t is varied in 3-hour increments from 0 to 24. The farfield dilution is assumed to increase as a function of the 4/3 law for open waters. The results are presented in Table F-2. The maximum dissolved oxygen depression due to sediment resuspension is .083 mg/L and it occurs at t = 3 hours. Using the lowest ambient bottom dissolved oxygen concentration (5.848 mg/L), the minimum concentration resulting from sediment resuspension is 5.765 mg/L. This represents 1.4 percent in ambient dissolved oxygen concentrations.

**Table F-2. Oxygen Depletion Resulting From Sediment Resuspension**

<b>Time (hrs.)</b>	<b>Delta DO (mg/L)</b>
0	0.0
3	0.083
6	0.059
9	0.048
12	0.042
15	0.037
18	0.034
21	0.031
24	0.029

**APPENDIX F- Attachment 3**  
**Supporting Model and Documentation for Analysis of Dissolved Oxygen**  
**Suppression Calculations**

**Visual Basic Program HONODO1**  
Written by Alex Steele of K. P. Lindstrom, Inc.

**Sub Command1\_Click ()**

**' Nearfield DO demand following Initial Dilution**

Debug.Print ""

Debug.Print " Nearfield DO demand following Initial Dilution"

Debug.Print ""

**' Equation from TTRTD, 1994**

**'  $DO_f = DO_a + (DO_e - IDOD - DO_a) / Sa$**

**' Where...**

**'  $DO_f$  = final DO conc.**

**'  $DO_a$  = ambient DO upcurrent of diffuser between  
diffuser depth and trapping depth**

**'  $DO_e$  = DO of eff.**

**'  $IDOD$  = imediate DO demand (typically 0 - 10 -  
TTRTD, 1994)**

**'  $Sa$  = Initial Dilution**

**' Using for Honolulu...**

**$DO_a = 5.848$**

**$DO_e = 0$**

**$IDOD = 5$ : 'see table B-3, TTRTD, 1994 -**

**'used Effl BOD=200 mg/L, travel time=100 min**

**$Sa = 210$ : 'ID in 2010**

Debug.Print "Ambient DO ( $DO_a$ ) =", Format\$( $DO_a$ , "####.000"); " mg/L"

**' calc #1**

**$DO_f = DO_a + (DO_e - IDOD - DO_a) / Sa$**

Debug.Print "Final DO ( $DO_f$ ) =", Format\$( $DO_f$ , "####.000"); " mg/L"

**' calc #2**

**$DO_{red} = DO_a - DO_f$**

Debug.Print "Reduction in ambient DO =", Format\$( $DO_{red}$ , "####.000"); " mg/L"

**' calc #3**

**$DO_{pred} = ((DO_a - DO_f) / DO_a) * 100$**

Debug.Print "% reduction in ambient DO =", Format\$( $DO_{pred}$ , "####.000"); " %"

**' no indication of entrainment reduction in DO**

**' use real data to check for compliance with % DO**

**' saturation - >75%**

End Sub

**Sub Command1 Click - RUN - output equals...**

Nearfield DO demand following Initial Dilution

Ambient DO (DO<sub>a</sub>) = 5.848 mg/L

Final DO (DO<sub>f</sub>) = 5.796 mg/L

Reduction in ambient DO = .052 mg/L

% reduction in ambient DO = .883 %

## Sub Command2\_Click ()

### ' Farfield DO demand following Initial Dilution

Debug.Print ""

Debug.Print " Farfield DO demand following Initial Dilution"

Debug.Print ""

' This discussion is organized as follows;

- ' I. find final BOD after initial dilution
- ' find ultimate BOD
- ' II. find decay constants for Carbonaceous and Nitrogenous BOD demand
- ' III. Find the Centerline dilution using 4/3 law (compare 4/3 law to other dilution methods)
- ' IV. Combine above to get Far field DO demand

' I.

' Equation from TTRTD, 1994

$$\text{BODf} = \text{BODa} + (\text{BODe} - \text{BODa}) / \text{Sa}$$

' Where...

' BODf = final BOD5 conc. (mg/L)

' BODa = ambient BOD5 upcurrent of diffuser between diffuser depth and trapping depth

' BODe = BOD5 of eff.

' Sa = Initial Dilution

' Using for Honolulu...

**BODa = 0**

**BODe = 238: 'see table B-3, TTRTD, 1994 -**

**'used Effl BOD=200 mg/L, travel time=100 min**

**'used worst case for honoululi effluent**

**Sa = 210: '2010 ID**

' First check whether

' DOstd <= DOf - BODfu

' Where...

' DOstd=DO standard

' DOf = DO conc after initial dilution

' BODfu = Ultimate BOD at completion of

' Initial dilution (=BODf \* 1.46)

Debug.Print "Ambient Ocean BOD assumed to equal = 0.000 mg/L"

Debug.Print "Effluent BOD = "; Format\$(BODe, "####.000"); "mg/L"

' get BODf

$$\text{BODf} = \text{BODa} + (\text{BODe} - \text{BODa}) / \text{Sa}$$

Debug.Print "BOD final after initial dilution = "; Format\$(BODf, "####.000"); "mg/L"

' convert BOD5 to Ultimate BOD (BODl)

$$\text{BODl} = \text{BODf} * 1.46$$

Debug.Print "Ultimate BOD (\* 1.46) = "; Format\$(BODl, "####.000"); "mg/L"

' II.

' BOD has two forms;  
' 1. Carbonaceous - CBOD  
' use temperature correction below  
'  $Kt=0.23*1.047^{(T-20)}/\text{day}$

' Where...  
' Kt = BOD decay rate at temp T (deg C)

t = 20: 'default  
KtCarb = .23 \* 1.047 ^ (t - 20)  
Debug.Print "at "; t; "deg C The Carbonaceous BOD decay constant = "; Format\$(KtCarb, "####.000")

t = 24.5: 'Honouliuli  
KtCarb = .23 \* 1.047 ^ (t - 20)  
Debug.Print "at "; t; "deg C The Carbonaceous BOD decay constant = "; Format\$(KtCarb, "####.000")

' 2. Nitrogenous - NBOD  
' NBOD1=4.57 (TKN)  
' NBOD5=NBOD1/2.54

' Where...  
' TKN = total Kjeldahl nitrogen  
' NBOD1 = ultimate NBOD  
' NBOD5 = 5 day NBOD

'  $Kt=0.10*1.047^{(T-20)}/\text{day}$

' Where Kt = BOD decay rate at temp T (deg C)  
' 0.10 = decay rate at 20 deg C

t = 20: 'default  
KtNitr = .1 \* 1.047 ^ (t - 20)  
Debug.Print "at "; t; "deg C The Nitrogenous BOD decay constant = "; Format\$(KtNitr, "####.000")

t = 24.5: 'Honouliuli  
KtNitr = .1 \* 1.047 ^ (t - 20)  
Debug.Print "at "; t; "deg C The Nitrogenous BOD decay constant = "; Format\$(KtNitr, "####.000")

' III.

' To determine additional dilution use 4/3 law  
' for lateral diffusion coefficient  
'  $E = E0*(L/b)^{(4/3)}$

' Where...  
' E = Lateral diffusion coefficient  $\text{ft}^2/\text{sec}$   
' E0 = Diffusion coeff when  $L=b$   
' L = Width of sewage field at any distance from  
' ZID in feet  
' b = Initial width of sewage field (approx as  
' longest dimension of the ZID), in feet

' E0 can be approximated as  
'  $E0 = .001 * b ^{(4 / 3)}$

' based on the 4/3 law the centerline dilution  
'  $Ds=1/erf((1.5/(1+(8*E0*t)/(b^2)))^3-1)^.5$

' Where...

' t = travel time, sec

' erf = the error function

' The TTRTD also recommends for coastal areas

'  $D=1/erf((1.5/(1+(12*E0*t)/(B^2)))^2-1)^.5$

' or most conservatively - assume diff coef const

'  $Ds=1/erf((b^2/(16*E0*t))^.5$

' Test above 3 possibilities to see what happens...

' Note can check/confirm calculations with data

' in TTRTD, 1994 Table B-5 pg. B-41...

t = 9000: '2.5 hours

' difuser length =1750' +

' 1/2 water depth at each end

b = 2000: 'based on 1750 + 60 \* 3.28

$E0 = .001 * b^{(4/3)}$

$Ds43 = 1 / (1.5 / ((1 + ((8 * E0 * t) / (b^2)))^3 - 1))^ .5$

Debug.Print "Given t="; t; "secs, b="; b; "feet, Then Ds43="; Format\$(Ds43, "####.000")

$Dcoast = 1 / (1.5 / ((1 + ((12 * E0 * t) / (b^2)))^2 - 1))^ .5$

Debug.Print "Given t="; t; "secs, b="; b; "feet, Then Dcoast="; Format\$(Dcoast, "####.000")

$Dcons = 1 / ((b^2) / (16 * E0 * t))^ .5$

Debug.Print "Given t="; t; "secs, b="; b; "feet, Then Dcons="; Format\$(Dcons, "####.000")

' Use above to plot Dilution versus time

' for t=0 to 300000 seconds

picture1.Scale (-34000, 300)-(-34000, -30)

picture1.Line (0, 0)-(300000, 0)

picture1.Line (0, 0)-(0, 250)

' hour and day tick marks

For t = 0 To 300000 Step 3600

picture1.Line (t, 0)-(t, -3), RGB(0, 0, 0)

Next t

daystep = 3600 \* 24#

For t = 0 To 300000 Step daystep

picture1.Line (t, 0)-(t, -6), RGB(0, 0, 0)

Next t

For t = 5000 To 300000 Step 5000

$Ds43 = 1 / (1.5 / ((1 + ((8 * E0 * t) / (b^2)))^3 - 1))^ .5$

If t = 5000 Then picture1.PSet (t, Ds43), RGB(255, 0, 0)

If t > 5000 Then picture1.Line -(t, Ds43), RGB(255, 0, 0)

Next t

For t = 5000 To 300000 Step 5000

$Dcoast = 1 / (1.5 / ((1 + ((12 * E0 * t) / (b^2)))^2 - 1))^ .5$

If t = 5000 Then picture1.PSet (t, Dcoast), RGB(255, 0, 0)

If t > 5000 Then picture1.Line -(t, Dcoast), RGB(0, 255, 0)

Next t

For t = 5000 To 300000 Step 5000

$Dcons = 1 / ((b^2) / (16 * E0 * t))^ .5$

```

If t = 5000 Then picture1.PSet (t, Dcons), RGB(255, 0, 0)
If t > 5000 Then picture1.Line -(t, Dcons), RGB(0, 0, 255)
Next t

```

IV.

```

' from TTRTD, 1994 (originally from Brooks, 1960)
'  $DO_{far}(t) = DO_a + ((DO_f - DO_a) / D_s) - (L_{fc} / D_s) * 1 - \exp(-k_c * t) - (L_{fn} / D_s) * 1 - \exp(-k_n * t)$ 

```

' Where...

```

'  $DO_{far}(t)$  = DO in submerged wastefield as function of time t
'  $DO_a$  = ambient DO
'  $DO_f$  = DO after initial dilution
'  $k_c$  = CBOD decay rate constant (KtCarb)
'  $k_n$  = NBOD decay rate constant (KtNitr)
'  $L_{fc}$  = Ultimate CBOD conc above ambient after initial
' dilution
'  $L_{fn}$  = Ultimate NBOD conc above ambient at completion
' of initial dilution
'  $D_s$  = Dilution attained after initial dilution
' as function of travel time

```

' Using for Honolulu...

```

 $DO_a = 5.848$ 
 $DO_e = 0$ 
 $IDOD = 5$ : 'see table B-3, TTRTD, 1994 -
'used Effl BOD=200 mg/L, travel time=100 min
 $S_a = 210$ : '2010 ID
' calc #1
 $DO_f = DO_a + (DO_e - IDOD - DO_a) / S_a$ 
 $L_{fc} = BODI$ 
 $t = 24.5$ : 'Honouliuli temperature (deg C)
 $KtNitr = .1 * 1.047 ^ (t - 20)$ 
 $KtCarb = .23 * 1.047 ^ (t - 20)$ 
 $b = 2000$ : '1750 + 60 * 3.28
 $E_0 = .001 * b ^ (4 / 3)$ 

```

Close 2

Open "dodemand.dat" For Output As #2

Print #2, "Farfield DO demand following Initial Dilution"

Print #2, " Time Subsequent DO"

Print #2, " hours Dilution mg/L"

For t = 0 To 72

' using Ds43 equation for Ds -

tsec = t \* 3600: ' convert t to seconds

If tsec = 0 Then tsec = 1:

$D_s = 1 / (1.5 / ((1 + ((8 * E_0 * tsec) / (b ^ 2))) ^ 3 - 1)) ^ .5$

$Carb_{red} = (L_{fc} / D_s) * (1 - \exp(1) ^ (-KtCarb / 24 * t))$

$Nitr_{red} = (L_{fn} / D_s) * (1 - \exp(1) ^ (-KtNitr / 24 * t))$

' Debug.Print "Carbred =", Carbred, " Nitrrred =", Nitrrred

$DO_{far} = DO_a + ((DO_f - DO_a) / D_s) - Carb_{red} - Nitr_{red}$

Debug.Print "At t="; t; "hours, Ds="; Format\$(Ds, "####.000"); " DOfar="; Format\$(DOfar, "####.000")

Print #2, " "; t; ", "; Format(Ds, "####.000"); ", "; Format(DOfar, "####.000")

Next t



Close 2

End Sub

**Sub Command2 Click - RUN - output equals...**

Farfield DO demand following Initial Dilution

‘ Compute Ultimate BOD of diluted effluent following initial dilution

Ambient Ocean BOD assumed to equal = 0.000 mg/L

Effluent BOD = 238.000mg/L

BOD final after initial dilution = 1.133mg/L

Ultimate BOD (\* 1.46) = 1.655mg/L

‘ test sensitivity of decay coefficient to changes in T

at 20 deg C The Carbonaceous BOD decay constant = .230

at 24.5 deg C The Carbonaceous BOD decay constant = .283

at 20 deg.C The Nitrogenous BOD decay constant = .100

at 24.5 deg C The Nitrogenous BOD decay constant = .123

‘compare three alternatives for farfield dilution

Given t= 9000 secs, b= 2000 feet, Then Ds43=1.175

Given t= 9000 secs, b= 2000 feet, Then Dcoast=1.103

Given t= 9000 secs, b= 2000 feet, Then Dcons=.952

‘Use 4/3 law centerline dilution get Dofar for 1 to 72 hours post initial dilution

Given t= 1 hours, Ds=.658 Then DOfar=5.740

Given t= 2 hours, Ds=1.010 Then DOfar=5.759

Given t= 3 hours, Ds=1.337 Then DOfar=5.766

Given t= 4 hours, Ds=1.661 Then DOfar=5.771

Given t= 5 hours, Ds=1.989 Then DOfar=5.774

Given t= 6 hours, Ds=2.325 Then DOfar=5.777

Given t= 7 hours, Ds=2.670 Then DOfar=5.780

Given t= 8 hours, Ds=3.026 Then DOfar=5.782

Given t= 9 hours, Ds=3.391 Then DOfar=5.784

Given t= 10 hours, Ds=3.767 Then DOfar=5.785

Given t= 11 hours, Ds=4.154 Then DOfar=5.787

Given t= 12 hours, Ds=4.551 Then DOfar=5.789

Given t= 13 hours, Ds=4.959 Then DOfar=5.790

Given t= 14 hours, Ds=5.377 Then DOfar=5.792

Given t= 15 hours, Ds=5.804 Then DOfar=5.793

Given t= 16 hours, Ds=6.242 Then DOfar=5.794

Given t= 17 hours, Ds=6.690 Then DOfar=5.795

Given t= 18 hours, Ds=7.147 Then DOfar=5.797

Given t= 19 hours, Ds=7.614 Then DOfar=5.798

Given t= 20 hours, Ds=8.090 Then DOfar=5.799

Given t= 21 hours, Ds=8.575 Then DOfar=5.800

Given t= 22 hours, Ds=9.069 Then DOfar=5.801

Given t= 23 hours, Ds=9.571 Then DOfar=5.802

Given t= 24 hours, Ds=10.083 Then DOfar=5.802

Given t= 25 hours, Ds=10.603 Then DOfar=5.803  
Given t= 26 hours, Ds=11.132 Then DOfar=5.804  
Given t= 27 hours, Ds=11.668 Then DOfar=5.805  
Given t= 28 hours, Ds=12.214 Then DOfar=5.806  
Given t= 29 hours, Ds=12.767 Then DOfar=5.806  
Given t= 30 hours, Ds=13.328 Then DOfar=5.807  
Given t= 31 hours, Ds=13.897 Then DOfar=5.808  
Given t= 32 hours, Ds=14.474 Then DOfar=5.809  
Given t= 33 hours, Ds=15.058 Then DOfar=5.809  
Given t= 34 hours, Ds=15.650 Then DOfar=5.810  
Given t= 35 hours, Ds=16.249 Then DOfar=5.810  
Given t= 36 hours, Ds=16.856 Then DOfar=5.811  
Given t= 37 hours, Ds=17.470 Then DOfar=5.812  
Given t= 38 hours, Ds=18.092 Then DOfar=5.812  
Given t= 39 hours, Ds=18.720 Then DOfar=5.813  
Given t= 40 hours, Ds=19.356 Then DOfar=5.813  
Given t= 41 hours, Ds=19.998 Then DOfar=5.814  
Given t= 42 hours, Ds=20.648 Then DOfar=5.814  
Given t= 43 hours, Ds=21.304 Then DOfar=5.815  
Given t= 44 hours, Ds=21.967 Then DOfar=5.815  
Given t= 45 hours, Ds=22.637 Then DOfar=5.816  
Given t= 46 hours, Ds=23.313 Then DOfar=5.816  
Given t= 47 hours, Ds=23.996 Then DOfar=5.817  
Given t= 48 hours, Ds=24.686 Then DOfar=5.817  
Given t= 49 hours, Ds=25.382 Then DOfar=5.817  
Given t= 50 hours, Ds=26.084 Then DOfar=5.818  
Given t= 51 hours, Ds=26.793 Then DOfar=5.818  
Given t= 52 hours, Ds=27.508 Then DOfar=5.819  
Given t= 53 hours, Ds=28.229 Then DOfar=5.819  
Given t= 54 hours, Ds=28.956 Then DOfar=5.819  
Given t= 55 hours, Ds=29.690 Then DOfar=5.820  
Given t= 56 hours, Ds=30.429 Then DOfar=5.820  
Given t= 57 hours, Ds=31.175 Then DOfar=5.820  
Given t= 58 hours, Ds=31.927 Then DOfar=5.821  
Given t= 59 hours, Ds=32.684 Then DOfar=5.821  
Given t= 60 hours, Ds=33.447 Then DOfar=5.821  
Given t= 61 hours, Ds=34.217 Then DOfar=5.822  
Given t= 62 hours, Ds=34.992 Then DOfar=5.822  
Given t= 63 hours, Ds=35.772 Then DOfar=5.822  
Given t= 64 hours, Ds=36.559 Then DOfar=5.823  
Given t= 65 hours, Ds=37.351 Then DOfar=5.823  
Given t= 66 hours, Ds=38.149 Then DOfar=5.823  
Given t= 67 hours, Ds=38.952 Then DOfar=5.823  
Given t= 68 hours, Ds=39.761 Then DOfar=5.824  
Given t= 69 hours, Ds=40.575 Then DOfar=5.824  
Given t= 70 hours, Ds=41.395 Then DOfar=5.824  
Given t= 71 hours, Ds=42.221 Then DOfar=5.825  
Given t= 72 hours, Ds=43.051 Then DOfar=5.825

## Sub Command3\_Click ()

### ' Steady State Sediment DO Demand

' Sediment DO demand  
Debug.Print ""  
Debug.Print " Steady State Sediment DO Demand"  
Debug.Print ""

### ' Equation B-24 from TTRTD, 1994

$$' dDO = (Sb * Xm) / (86400 * UHD) = (a * S * Kd * Xm) / (86400 * UHD)$$

' Where...

' dDO = Oxygen depletion (mg/L)  
' Sb = avg benthic oxygen demand over deposition  
' area, g o2/m2/day  
' Xm = length of deposition area, m  
' H = Average depth of water column influenced  
' by sediment demand, measured above bottom, m  
' U = Minimum sustained current speed over bottom  
' m/sec  
' Kd = Sediment decay rate constant, 0.01/day  
' a = Oxygen:sediment stoichiometric ratio,  
' 1.07 mg O2/mg sediment  
' S = Avg conc of deposited organic sediments  
' over the depositional area, g/m2  
' D = Dilution caused by the horizontal entrainment  
' of ambient water as it passes over the  
' depositional area (always >=1)

' S and Xm come from suspended solids deposition  
' analysis...  
' TTRTD recommends averaging highest and lowest  
' deposition values to get S.

' an estimate of the avg depth is eq B-26;

$$' H = 0.8 * ((Ez * Xm) / U) ^ .5$$

' Where...

' Ez = Vertical diffusion coeff (cm2/sec)  
' default value of Ez is 1  
' Ez can also be calculated by  
' Ez = 10^-4 / ((1/density) \* density gradient)

' Where...

' density = Ambient water density, kg/m3 (1024)  
' density gradient = Ambient density gradient, kg/m4  
' TTRTD recommends using the most severe stratification  
' condition during the critical period.

' The dilution D should be found from  
' TTRTD table B-5

' Using for Honolulu...

DOa = 5.848: 'used here only for comparison

Kd = .01

a = 1.07: '(From TTRTD, 1994)

S = 25: '(From Honouliuli 1995 draft)

Xm = 3000: '(conservative measure of 5g/m<sup>2</sup>

' isopleth from 1983 Honouliuli application

Ez = 1: '(From Honouliuli 1995 draft)

U = .03: '(From Honouliuli 1995 draft)

D = 1: '(From Honouliuli 1995 draft, originally from TT, 1984)

Debug.Print "Lowest observed ambient DO = "; Format\$(DOa, "####.000"); " mg/L"

' test calculation see TTRTD eq 8-27...

H = .8 \* ((Ez \* Xm \* 100) / (U \* 100)) ^ .5 \* (1 / 100)

Debug.Print "H = "; Format\$(H, "####.000"); "m"

dDO = (Sb \* Xm) / (86400 \* U \* H \* D)

Debug.Print "Eq1 delta DO due to steady state sediment demand ="; Format\$(dDO, "####.000"); " mg/L"

' or

dDO = (a \* S \* Kd \* Xm) / (86400 \* U \* H \* D)

Debug.Print "Eq2 delta DO due to steady state sediment demand ="; Format\$(dDO, "####.000"); " mg/L"

predDO = dDO / DOa \* 100

Debug.Print "Percent reduction in DO ="; Format\$(predDO, "####.000"); "%"

End Sub

### Sub Command3 Click - RUN - output equals...

Steady State Sediment DO Demand

Lowest observed ambient DO = 5.848 mg/L

H = 2.530m

Eq. 1. delta DO due to steady state sediment demand =.000 mg/L

(Eq. 1. doesn't work because Sb is not provided so use Eq. 2.)

Eq. 2. delta DO due to steady state sediment demand =.122 mg/L

Percent reduction in DO =2.093%

## Sub Command4\_Click ()

### ' Oxygen Demand due to Resuspension of Sediments

```
Debug.Print ""  
Debug.Print " Oxygen Demand due to Resuspension of Sediments"  
Debug.Print ""
```

' Equation from TTRTD, 1994, pg. B-42

$$' dDO = (Sb * Xm) / (86400 * U * H * D) = (a * S * Kd * Xm) / (86400 * U * H * D)$$

' Where...

' dDO = Oxygen depletion (mg/L)  
' Sb = avg benthic oxygen demand over deposition  
' area, g o2/m2/day  
' Xm = length of deposition area, m  
' H = Average depth of water column influenced  
' by sediment demand, measured above bottom, m  
' U = Minimum sustained current speed over bottom  
' m/sec  
' Kd = Sediment decay rate constant, 0.01/day  
' a = Oxygen:sediment stoichiometric ratio,  
' 1.07 mg O2/mg sediment  
' S = Avg conc of deposited organic sediments  
' over the depositional area, g/m2  
' D = Dilution caused by the horizontal entrainment  
' of ambient water as it passes over the  
' depositional area (always >=1)

$$' H = 1.6 / 100 * (3,600 * t * E1z) ^ .5$$

' Where

' E1z = Vertical diff coef when resuspension  
' is occurring (5 cm2/sec)  
' t = elapsed time following resuspension, hours

' For Honouliuli use

**DOa = 5.848: ' for estimating % reduction...**

**E1z = 5**

**t = 0 to 72 hours**

**Xm = 3000**

**D = 1: 'Honouliuli value (SI value = 2.5)**

**S = 25: 'Honouliuli value (SI value = 8.41)**

**Kd = .01: 'SI value**

**U = .03: 'SI value**

**a = 1.07: 'SI value**

For t = 0 To 72 Step 3

$$H = 1.6 / 100 * (3600 * t * E1z) ^ .5$$

```
Debug.Print "t="; t; "hrs, H="; Format$(H, "####.000");
```

' eq 1

$$' dDO = (Sb * Xm) / (86400 * U * H * D)$$

'Debug.Print "eq 1. dDO ="; dDO

'eq 2

If H > 0 Then dDO = (a \* S \* Kd \* Xm) / (86400 \* U \* H \* D)

Debug.Print "m, dDO="; Format\$(dDO, "####.000");

Debug.Print "mg/L, Estimated ambient DO reduction="; Format\$(dDO / DOa \* 100, "####.000"); "%"

Next t

End Sub

### **Sub Command4 Click - RUN - output equals...**

Oxygen Demand due to Resuspension of Sediments

Using lowest observed ambient DO = 5.848 mg/L

t= 3 hrs, H=3.718m, dDO=.083mg/L, Estimated ambient DO reduction=1.424%  
t= 6 hrs, H=5.258m, dDO=.059mg/L, Estimated ambient DO reduction=1.007%  
t= 9 hrs, H=6.440m, dDO=.048mg/L, Estimated ambient DO reduction=.822%  
t= 12 hrs, H=7.436m, dDO=.042mg/L, Estimated ambient DO reduction=.712%  
t= 15 hrs, H=8.314m, dDO=.037mg/L, Estimated ambient DO reduction=.637%  
t= 18 hrs, H=9.107m, dDO=.034mg/L, Estimated ambient DO reduction=.581%  
t= 21 hrs, H=9.837m, dDO=.031mg/L, Estimated ambient DO reduction=.538%  
t= 24 hrs, H=10.516m, dDO=.029mg/L, Estimated ambient DO reduction=.503%  
t= 27 hrs, H=11.154m, dDO=.028mg/L, Estimated ambient DO reduction=.475%  
t= 30 hrs, H=11.758m, dDO=.026mg/L, Estimated ambient DO reduction=.450%  
t= 33 hrs, H=12.331m, dDO=.025mg/L, Estimated ambient DO reduction=.429%  
t= 36 hrs, H=12.880m, dDO=.024mg/L, Estimated ambient DO reduction=.411%  
t= 39 hrs, H=13.406m, dDO=.023mg/L, Estimated ambient DO reduction=.395%  
t= 42 hrs, H=13.912m, dDO=.022mg/L, Estimated ambient DO reduction=.381%  
t= 45 hrs, H=14.400m, dDO=.022mg/L, Estimated ambient DO reduction=.368%  
t= 48 hrs, H=14.872m, dDO=.021mg/L, Estimated ambient DO reduction=.356%  
t= 51 hrs, H=15.330m, dDO=.020mg/L, Estimated ambient DO reduction=.345%  
t= 54 hrs, H=15.774m, dDO=.020mg/L, Estimated ambient DO reduction=.336%  
t= 57 hrs, H=16.207m, dDO=.019mg/L, Estimated ambient DO reduction=.327%  
t= 60 hrs, H=16.628m, dDO=.019mg/L, Estimated ambient DO reduction=.318%  
t= 63 hrs, H=17.038m, dDO=.018mg/L, Estimated ambient DO reduction=.311%  
t= 66 hrs, H=17.439m, dDO=.018mg/L, Estimated ambient DO reduction=.304%  
t= 69 hrs, H=17.831m, dDO=.017mg/L, Estimated ambient DO reduction=.297%  
t= 72 hrs, H=18.215m, dDO=.017mg/L, Estimated ambient DO reduction=.291%

