June 2000

Environmental Technology Verification Report

SIGRIST WTM500 ON-LINE TURBIDIMETER

Prepared by

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June 2000

Environmental Technology Verification Report

ETV Advanced Monitoring Systems Pilot

Sigrist
WTM500 On-Line Turbidimeter

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Notice

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Foreword

The U.S. Environmental Protection Agency (EPA) is charged by Congress with protecting the Nation's air, water, and land resources. Under a mandate of national environmental laws, the Agency strives to formulate and implement actions leading to a compatible balance between human activities and the ability of natural systems to support and nurture life. To meet this mandate, the EPA's Office of Research and Development (ORD) provides data and science support that can be used to solve environmental problems and to build the scientific knowledge base needed to manage our ecological resources wisely, to understand how pollutants affect our health, and to prevent or reduce environmental risks.

The Environmental Technology Verification (ETV) Program has been established by the EPA to verify the performance characteristics of innovative environmental technology across all media and to report this objective information to permitters, buyers, and users of the technology, thus substantially accelerating the entrance of new environmental technologies into the marketplace. Verification Organizations oversee and report verification activities based on testing and Quality Assurance protocols developed with input from major stakeholders and customer groups associated with the technology area. At present, there are twelve environmental technology areas covered by ETV. Information about each of the environmental technology areas covered by ETV can be found on the Internet at http://www.epa.gov/etv.htm.

Effective verifications of monitoring technologies are needed to assess environmental quality and to supply cost and performance data to select the most appropriate technology for that assessment. In 1997, through a competitive cooperative agreement, Battelle was awarded EPA funding and support to plan, coordinate, and conduct such verification tests for "Advanced Monitoring Systems for Air, Water, and Soil" and report the results to the community at large. Information concerning this specific environmental technology area can be found on the Internet at http://www.epa.gov/etv/07/07_main.htm.

Acknowledgments

The authors wish to acknowledge the support of all those who helped plan and conduct the verification test, analyze the data, and prepare this report. In particular we would like to thank the staff at the Dublin Road Water Plant, including Tom Camden and Terry Nichols. We also acknowledge the participation of T.J. Medland of Peak Process Controls, Inc., and Dr. Arnd Rogner of Sigrist in this verification test. We would like to thank the Hach Company for supplying the two reference turbidimeters used in this test.

Contents

Figures

Tables

List of Abbreviations

AMS	Advanced Monitoring Systems
CU	color unit
DC	direct current
DRWP	Dublin Road Water Plant
EPA	U.S. Environmental Protection Agency
ETV	Environmental Technology Verification
FNU	formazin nephelometric unit
gpm	gallons per minute
LOD	limit of detection
NIST	National Institute of Standards and Technology
NPT	normal pipe thread
NTU	nephelometric turbidity unit
OD	outer diameter
PE	performance evaluation
QA	quality assurance
QC	quality control
QMP	Quality Management Plan
RSD	relative standard deviation

Chapter 1
Background

The U.S. Environmental Protection Agency (EPA) has created the Environmental Technology Verification (ETV) Program to facilitate the deployment of innovative environmental technologies through performance verification and dissemination of information. The goal of the ETV Program is to further environmental protection by substantially accelerating the acceptance and use of improved and cost-effective technologies. ETV seeks to achieve this goal by providing high quality, peer-reviewed data on technology performance to those involved in the design, distribution, permitting, purchase, and use of environmental technologies.

ETV works in partnership with recognized testing organizations; with stakeholder groups consisting of regulators, buyers and vendor organizations; and with the full participation of individual technology developers. The program evaluates the performance of innovative technologies by developing test plans that are responsive to the needs of stakeholders, conducting field or laboratory tests (as appropriate), collecting and analyzing data, and preparing peer-reviewed reports. All evaluations are conducted in accordance with rigorous quality assurance protocols to ensure that data of known and adequate quality are generated and that the results are defensible.

The EPA's National Exposure Research Laboratory and its verification organization partner, Battelle, operate the Advanced Monitoring Systems (AMS) pilot under ETV. The AMS pilot has recently evaluated the performance of on-line turbidimeters for use in water treatment facilities. This verification report presents the procedures and results of the verification test for the Sigrist WTM500 on-line turbidimeter.

Chapter 2
Technology Description

The following description of the Sigrist WTM500 turbidimeter is based on information provided by the vendor.

The WTM500 is an on-line turbidimeter, designed to meet ISO 7027[(1)], manufactured by Sigrist-Photometer AG, that provides non-contact measurement of the 90° scattered light in a free-falling water stream. Automatic adjustment using a fixed internal reference standard enhances measurement reliability and minimizes the need for cleaning and calibration. The WTM500 has a nominal range of 0 to 500 formazin nephelometric units (FNUs) in eight scale ranges, with a maximum resolution of 0.001 FNU. The control unit has a two-line liquid-crystal display.

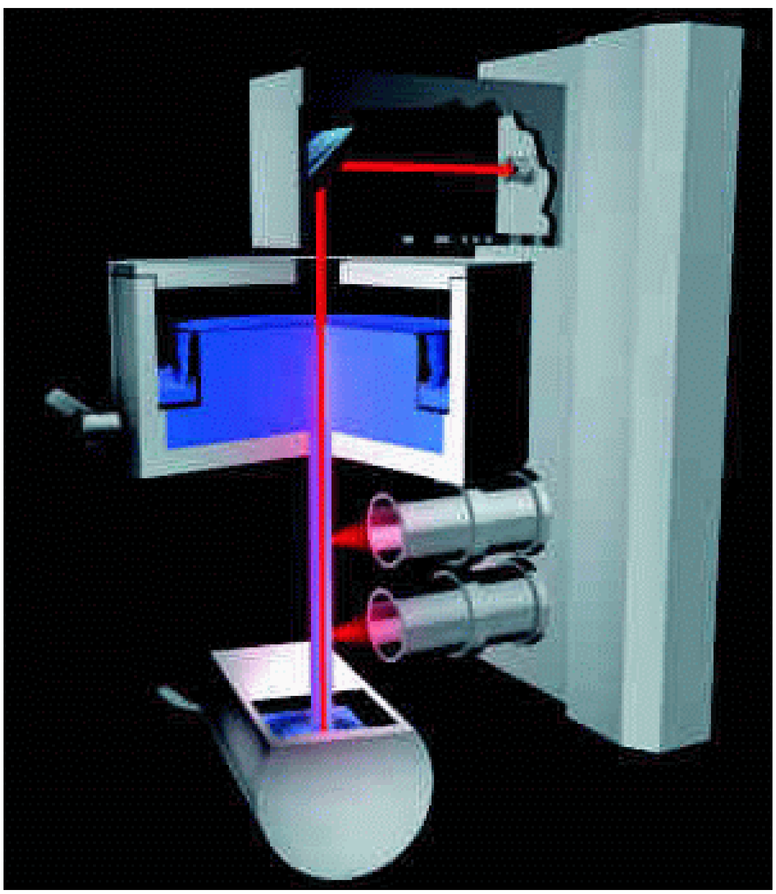

Figure 2-1. Sigrist WTM500 On-Line Turbidimeter

Because the flow cell and windows have been eliminated, the turbidimeter optics do not need to be cleaned regularly. The turbidimeter is adjusted using a solid internal reference standard. The formazin calibration is checked at regular intervals against a built-in solid reference, and any deviations are corrected automatically.

The WTM500 turbidimeter's measuring wave length is 880 nm, and it has eight configurable scale ranges. The turbidimeter is designed to be operated at temperatures between 0 and 40°C and at a flow rate between 0.84 and 1.06 gallons per minuts (gpm).

Chapter 3
Test Design and Procedures

3.1 Introduction

The verification test was conducted according to procedures specified in the *Test/QA Plan for Verification of On-Line Turbidimeters*.[2] Performance characteristics evaluated in the verification test are listed in Table 3-1 along with the dates that data were collected for these evaluations. The test was conducted at a full-scale municipal water treatment facility in Columbus, Ohio. The verification test described in this report was conducted from September 9 through October 26, 1999, as indicated in Table 3-1.

Table 3-1. Performance Characteristics Evaluated and Schedule of Verification Test

Performance Characteristic	Date Data Collected
Off-Line Phase	
Linearity	September 9 to 10; October 20 to 21
Accuracy	September 9 to 10
Precision	September 9 to 10
Water temperature effects	September 10, 14 to 15
Flow rate sensitivity	September 15 to 16
Color effects	October 25 to 26
On-Line Phase	
Accuracy	September 17 to October 18
Calibration checks	September 23, 24, 27, 30 and October 6, 8, 12, 18

3.2 Test Design Considerations

Since turbidity is a measurement of light scattering, a number of factors can influence the measurement of turbidity in a given sample solution. Instrument design, including light source selection and geometric differences, may result in significant differences between the responses of different turbidimeters. Further differences may result from the variable nature of both the size and composition of particles typically found in water streams, relative to those in standard solutions made with formazin or with polymer beads. These issues were addressed in this verification test in two ways: (1) by using different instrumental designs for the reference turbidimeters, and (2) by evaluating a variety of samples.

To avoid potential bias associated with a single method of comparison, the verification test used two reference methods for data comparisons: ISO 7027, "Water Quality—Determination of Turbidity,"[(1)] and EPA Method 180.1, "Determination of Turbidity by Nephelometry."[(3)] Both of these methods measure turbidity using a nephelometric turbidimeter, but they differ in the type of light source and the wavelength used. ISO 7027 calls for an infrared light source, whereas Method 180.1 calls for a visible light source. The Sigrist WTM500 is designed to conform to the requirements of ISO 7027, and thus that method is the appropriate reference for verification of the WTM500's performance. Verification results presented in this report, and summarized in the Verification Statement, are based on comparisons with the ISO 7027 data. However, secondary comparisons also are shown in this report, based on data from the WTM500 and Method 180.1. These secondary comparisons are of interest because Method 180.1 is widely recognized in the U.S. and is designated as the required method for drinking water compliance measurements. These secondary comparisons are shown only to illustrate the performance capabilities of the WTM500 and should not be taken as having equal weight as the comparisons with ISO 7027.

Additionally, to assess the response of the Sigrist WTM500 turbidimeter to both prepared solutions and real-world water samples, verification involved both off-line and on-line phases. The off-line phase challenged the turbidimeter with a series of prepared standards and other test solutions to verify performance under controlled conditions. The on-line phase assessed long-term performance under realistic operating conditions by monitoring a sample stream in a municipal water treatment plant under normal operation. With the cooperation of the City of Columbus' Water Division, both off-line and on-line phases were performed at the division's Dublin Road Water Plant in Columbus, Ohio.

3.3 Experimental Apparatus

On-line turbidimeters measure turbidity continuously on flowing sample streams, as opposed to the static grab samples analyzed by the bench-top reference turbidimeters. Consequently, great care was taken to ensure that the samples collected for reference analysis were representative of the sample flow measured by the Sigrist WTM500 turbidimeter. A cylindrical distribution manifold provided identical sample streams to sample ports spaced equally around the circumference of the manifold. Throughout the verification test, three ports were used for the turbidimeters being verified and one port provided a stream for the grab samples. A single port centered in the bottom of the distribution manifold introduced the sample stream to the manifold. All the ports were tapped for ½" male NPT fittings, and hard plastic compression fittings were used to connect the distribution manifold to the tubing (½" OD polyethylene) used in the recirculation system. Using a consistent tubing size and fitting style enabled rapid switching of the turbidimeters on a scheduled basis among the ports on the distribution manifold. Providing

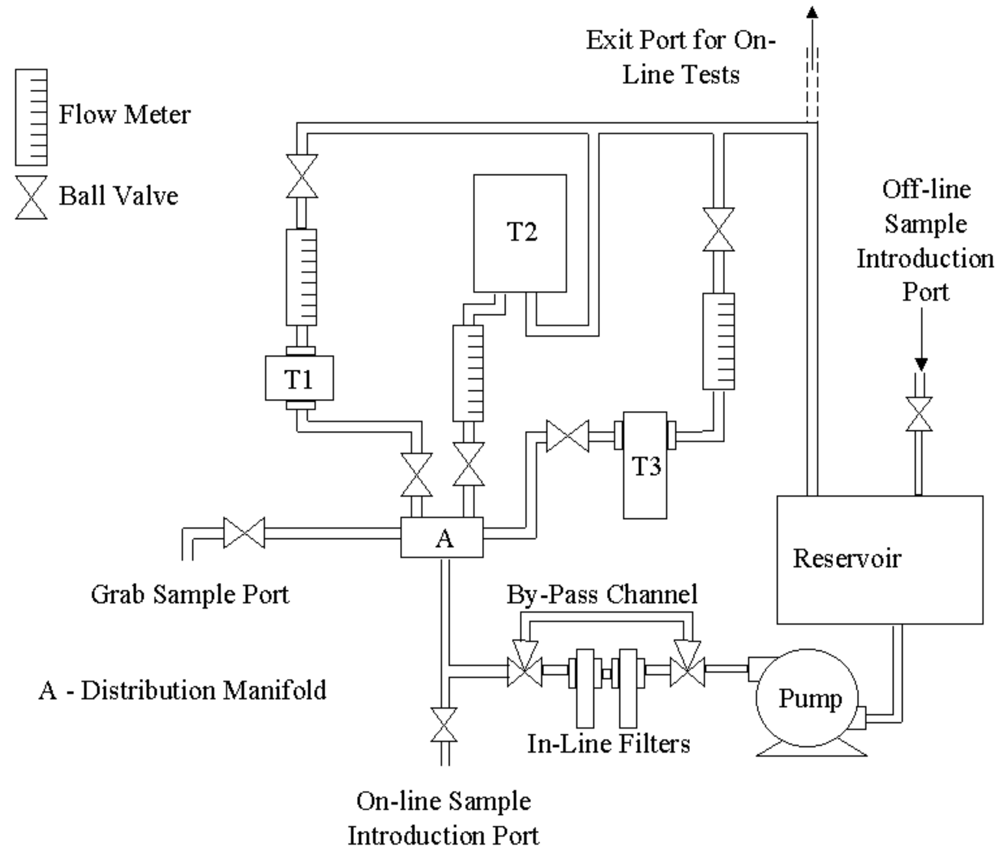

Figure 3-1. Schematic Representation of Recirculation System

identical samples to each of the manifold ports minimized biases arising from water quality or turbulence issues; rotation of the technologies to each of these ports was used to identify if biases existed.

A schematic representation of the recirculation system is provided in Figure 3-1, where T1 through T3 represent the three on-line turbidimeters undergoing verification testing. T2 represents the Sigrist WTM500 turbidimeter. Prepared solutions were supplied to all three turbidimeters simultaneously in a closed-loop recirculation system that used a 40-L reservoir and a centrifugal pump. Stream water from the plant was sampled from a pressurized source in a once-through configuration (i.e., without the use of the pump or reservoir). In-line particle filters were inserted into the water flow, using appropriate valving, when reduction of turbidity levels was needed.

Before verification testing began, a series of five grab samples was collected from each port on the cylindrical manifold while recirculating a formazin solution with a nominal turbidity of 0.5 NTU. These samples were analyzed with the reference turbidimeters and compared to ensure uniformity of the turbidity of the solution. Comparison of the sample analyses indicated agreement in turbidity readings within ± 5% of the average turbidity among all of the ports.

Before verification testing began, the on-line turbidimeters verified in this test were installed in the test apparatus at the Dublin Road Water Plant. Much of the recirculation system, including the flow meters and the distribution manifold, was mounted to a ¼"-thick aluminum panel installed in the water plant specifically for this verification test. The WTM500 turbidimeter (Serial Number 980952), installed by a representative of Sigrist, was mounted on an "L" bracket bolted to the aluminum panel. The bracket was secured to the panel using two bolts (~ ½" diameter), and the WTM500 turbidimeter was secured to the bracket with two similar bolts. During installation, the turbidimeter was leveled to optimize the optical qualities of the falling water stream in the turbidimeter and to ensure that the sample was properly collected and discharged. The sample inlet line entered the WTM500 at the base of the turbidimeter housing. The turbidimeter and the recirculation system were connected with soft plastic tubing that was connected at one end to a nipple in the base of the turbidimeter housing and at the other end to a barbed fitting on the tubing in the recirculation system. A 1"-diameter flexible hose was connected to the outlet of the turbidimeter. To prevent overflow of the sample stream inside the turbidimeter housing, the outlet line was significantly larger than the inlet; no flow obstructions were added to the outlet stream. Consequently, the flow meter was installed on the inlet line of the WTM500, as illustrated in Figure 3-1.

The control unit for the Sigrist WTM500 was installed above the turbidimeter and mounted to the aluminum panel using two of four available bolt holes in the back of the control unit housing. The output was converted from a 4-20 mA signal to a DC voltage using a precision resistor, and was recorded every 10 seconds throughout the test using LabTech Notebook software, which was run on a personal computer at the test site. Since the intent of the verification test was to assess performance in routine unattended operation, the WTM500 was operated in its 0 to 10 NTU range throughout all test activities. In this range the smallest observable increment in turbidity was approximately 0.006 NTU.

3.4 Reference Instruments

Owing to the nature of turbidity measurement and the inherent differences in response arising from different instrumental designs, separate bench-top turbidimeters meeting the design criteria detailed in ISO 7027[1] and EPA Method 180.1[3] were used as reference instruments in this test. Both methods measure the nephelometric light scattering of a formazin solution, albeit with different prescribed instrumental designs. The primary difference between these two methods is in the choice of light source. Method 180.1 requires the use of a broadband visible incandescent tungsten lamp, while ISO 7027 requires the use of a narrowband IR source. Since the WTM500 is designed to comply with ISO 7027 requirements, that reference method is the basis for this verification. Comparisons of data with Method 180.1 are also shown because of the widespread recognition and use of that method. However, Method 180.1 comparisons are secondary to the ISO 7027 comparisons used for verification. The bench-top turbidimeters used as the reference methods were the Hach 2100AN (Serial Number 980300001366) and the Hach 2100AN IS

(Serial Number 950700000173), which, according to the manufacturer's literature, comply with the design specifications described in EPA Method 180.1[3] and ISO 7027[1], respectively. Throughout the test the reference turbidimeters were operated in the non-ratio mode.

3.5 Off-Line Testing

The off-line phase of the verification test involved off-line sample introduction aimed at assessing the linearity, accuracy, and precision of the on-line turbidimeter relative to the reference methods. Additionally, response to various upset conditions was quantified. As a means of testing these parameters, the off-line test phase included the introduction of standard formazin solutions or other samples and the intentional manipulation of flow and water quality parameters.

Throughout the verification test, continuous turbidity measurements from the Sigrist WTM500 turbidimeter were recorded at preset intervals using LabTech Notebook software. Grab samples were collected simultaneously with some of these recorded measurements and analyzed using the bench-top reference turbidimeters to provide a basis of comparison for the performance evaluations. The collection of grab samples was timed to coincide within 10 seconds with the recording of real-time turbidity measurements from the Sigrist WTM500, and the grab samples were analyzed within three minutes after collection to minimize possible temperature and settling effects.

Additionally, off-line testing included monitoring the instrumental responses of the Sigrist turbidimeter to variations in water temperature, flow rate, and color. Each of these parameters was varied within a range consistent with conditions encountered under typical plant operation. The following subsections describe the procedures used for the off-line phase of the verification test.

Table 3-2 provides a summary of the parameters tested in the off-line phase, the test solutions used, and the number of readings recorded for each parameter.

3.5.1 Linearity

Linearity was measured in the range from approximately 0.05 to 5 NTU as an initial check in the off-line phase. The recirculation system was filled with distilled, deionized water, which was then recirculated and filtered in the test apparatus using a 0.2-µm pleated polypropylene filter for 24 hours. After filtering, the in-line filter was bypassed and the turbidity of the water in the recirculation system was measured by the reference turbidimeters to be approximately 0.05 NTU. A series of five turbidity measurements was taken at that turbidity level, with intervals of at least five minutes between successive measurements. A corresponding set of five measurements also was recorded at approximately 0.3, 0.5, 2, and 5 NTU. To reach each turbidity level, a small amount of 4000 NTU StablCal formazin stock solution was diluted in the recirculation system and allowed to flow through the recirculation system unfiltered for at least 15 minutes before

Table 3-2. Summary of Measurements for Off-Line Testing

Parameter Tested	Test Solution	Number of Readings
Linearity	Filtered Water (< 0.1 NTU)	5
Linearity (accuracy, precision)[a]	0.3 NTU Formazin	5
Linearity (accuracy, precision)	0.5 NTU Formazin	5
Linearity (accuracy, precision)	2 NTU Formazin	5
Linearity (accuracy, precision)	5 NTU Formazin	5
Water Temperature Effect	0.3 NTU Formazin	5 each at 16, 21, 27°C
Water Temperature Effect	5 NTU Formazin	5 each at 16, 21, 27°C
Flow Rate Effect	0.3 NTU Formazin	5
Flow Rate Effect	5 NTU Formazin	5
Color Effect	~ 0.1 NTU	5 each at 5, 15, 30 CU
Color Effect	5 NTU Formazin	5 each at 35, 45, 60 CU

a: ( ) indicates additional parameters analyzed using collected data.

turbidity readings were recorded. At each turbidity level, a series of five turbidity readings was recorded with at least a five-minute interval between successive readings.

These readings were compared to the reference measurements of grab samples collected simultaneously with each reading; that is, the turbidity of the solutions was determined by measurement with the reference turbidimeters, rather than simply by calculations based on the dilution process. After the prescribed measurements were recorded at each turbidity level, additional formazin stock solution was added to the recirculation system to increase the turbidity of the solution to the next value in the series.

Before measurements were recorded, the calibration of the reference turbidimeters was checked using a 0.5 NTU StablCal formazin solution purchased from Hach Company, Loveland, Colorado. Pursuant to the requirements of the test/QA plan,[2] agreement between the reference measurement and the certified turbidity of the standard was required to be within 10% before recording any series of measurements. After each series of measurements, the calibration of the reference turbidimeters was again checked with the same standard, and the same acceptance limits were applied. In addition to the 0.5 NTU calibration checks, before and after the measurements on the filtered water level, a < 0.1 NTU blank standard also was measured to ensure proper calibration of the reference instruments at low levels. The < 0.1 NTU standard also was purchased from Hach Company; agreement between the reference measurement and the turbidity reported on the certificate of analysis was required to be within 0.02 NTU.

3.5.2 Accuracy and Precision

Data obtained from the linearity measurements were used to establish the accuracy and precision of the Sigrist WTM500 turbidimeter in measuring formazin solutions. Accuracy was assessed by comparing continuous turbidity measurements with those from the ISO 7027 reference turbidimeter. Precision was assessed from the five replicate results at each turbidity level.

3.5.3 Water Temperature

Variations in the temperature of the water stream were introduced to simulate a range of conditions under which the on-line turbidimeters may typically operate. During off-line testing, the temperature of the recirculating water equilibrated in the range from 27 to 29°C, which was approximately 3 to 6°C above the room temperature at the water plant during testing. To assess the effect of temperature on the turbidimeter performance, the temperature of the recirculating solution was lowered using an immersion type chiller, and replicate turbidity measurements were recorded at approximately 21°C and again at 16°C. In these tests, the solution temperature in the reservoir was held within 2.5°C of the nominal 16°C and 21°C targets, while a series of five measurements was recorded at each temperature. To ensure equilibration, the solution was allowed to recirculate for one hour before the turbidity measurements were recorded. For the temperature tests at 16°C and 21°C, the temperature of the sample stream was recorded at the grab sample port within 30 seconds of sample collection, and the temperature of the grab sample was measured within 30 seconds of completion of the reference measurement. To assess temperature effects at different turbidities, this test was conducted with both 0.3 and 5 NTU solutions.

3.5.4 Flow Rate

The flow rate of the sample stream through the Sigrist WTM500 turbidimeter was manipulated to assess the response of the turbidimeter to various realistic operational conditions. A manual ball valve and needle valve were included upstream of the WTM500 turbidimeter and were adjusted to vary the flow rate through the turbidimeter. Owing to the nature of the WTM500 design, the flow requirements for the sample stream cover a narrow range of approximately 0.8 to 1.0 gpm. Flow rates below the minimum specification may result in an unsteady or uneven column of falling water, whereas flow rates above the maximum specification may result in overflow of the capture reservoir and subsequent flooding of the turbidimeter housing. During normal testing, the flow rate was held in the range from 0.85 to 0.95 gpm. The flow test was performed at a minimum flow rate of 0.85 gpm and at a maximum flow rate of 0.95 gpm. To assess the effect of flow rates on performance, measurements were made at both the minimum and maximum flow rates at turbidity levels of both 0.3 NTU and 5 NTU.

3.5.5 Color

Changes in water color were introduced by spiking the sample stream with colored solutions prepared from commercial food coloring dye. Stock solution was added to the system reservoir to give sample solutions approximately 5, 15, and 30 color units (CU) successively, and the instrumental response to these color changes was monitored. Five measurements were made for each color level at both low turbidity (~ 0.1 NTU) and higher turbidity (~ 5 NTU).

The color of the recirculated solution was determined by analyzing the grab samples instrumentally using the Hach 2100AN reference turbidimeter with the supplied light filter. The reference turbidimeter was calibrated for color measurements according to the instrument manual. Solutions used in the color calibration of the reference turbidimeter were prepared by dilution of a commercial cobalt-platinum color standard[4] (Hach Company, Loveland, Colorado).

At ~ 0.1 NTU, the color of the solution before addition of the dye was approximately 0 CU. However, at the 5 NTU level, light scattering from the presence of formazin introduced an apparent color to the solution of approximately 30 CU. Consequently, for the 5 NTU test, dye solution was added to increase the color by 5, 15, and 30 CU; i.e., to bring the absolute color to approximately 35, 45, and 60 CU, respectively.

3.6 On-Line Testing

The on-line test phase focused on assessing the long-term performance of the Sigrist turbidimeter under realistic unattended operating conditions and assessing its accuracy in monitoring an actual sample stream. Specifically, this phase of testing addressed the calibration and drift characteristics of the turbidimeter over a five-week period of monitoring a sample stream from the water plant. Routine reference measurements were used for comparison with the on-line readings to assess accuracy, and a re-evaluation of the calibration at the end of the test period helped establish drift characteristics. Natural meteorological and demand changes contributed to the variability of water quality in the treatment facility and provided a natural range of turbidity for characterizing performance.

Table 3-3 provides a summary of the parameters tested in the on-line phase, the test solutions used, and the number of readings recorded for each parameter.

Table 3-3. Summary of Measurements for On-Line Testing

Parameter Tested	Test Solution	Number of Readings
Accuracy	Plant Water	2 per weekday for 4 weeks (40 total)
Drift	0.3 NTU Standard	5 for final linearity check
Drift	0.5 NTU Standard	5 each for eight calibration checks (40 total) and 5 for final linearity check
Drift	2 NTU Standard	5 for final linearity check
Drift	5 NTU Standard	5 for final linearity check

3.6.1 Accuracy

In the on-line testing, the accuracy of the Sigrist WTM500 turbidimeter relative to the ISO 7027 reference method was assessed on water samples from the plant stream. A sample stream was drawn from a flocculation settling basin at the Dublin Road Water Plant facility, containing unfiltered water that had been treated with lime, caustic, and alum. The sample stream was directed to the Sigrist WTM500 turbidimeter through the distribution manifold. Two grab samples of this stream were collected and analyzed by the reference turbidimeters each weekday (Monday through Friday) for the four weeks of testing. The reference measurements of these samples were compared with the simultaneous results from the Sigrist WTM500 turbidimeter. The observed range of turbidity in the sample stream was approximately 0.1 to 1.0 NTU.

3.6.2 Drift

Drift was determined in two ways: (1) through off-line calibration checks conducted regularly throughout the course of the verification test using formazin solutions, and (2) through a comparison of multi-point linearity checks performed initially during the off-line phase (described in Section 5.1) and subsequently after the completion of the on-line phase. The turbidimeter was calibrated by the vendor prior to shipment and installation at the water plant. **After that calibration, no further manual calibration or adjustment was performed for the duration of the verification test period.** However, during the course of the on-line testing, automatic calibration adjustments were performed daily by the WTM500 using its internal reference standard. Also, the housing of the Sigrist WTM500 turbidimeter was opened twice during the on-line testing, at which times the reservoir was cleaned to remove accumulated deposits.

The Sigrist WTM500 turbidimeter was taken off line briefly twice each week for routine calibration checks against a 0.5 NTU formazin solution. These intermediate calibration checks were performed twice weekly for four consecutive weeks. Freshly diluted StablCal solutions were used as the standards for these calibration checks.

Upon completion of the four-week period, calibration and linearity were checked again, through a comparison with the reference measurements using standard solutions of 0.3, 0.5, 2, and 5 NTU. A linear fit of these data was compared with the initial linearity check performed in the off-line phase to assess the degree of calibration drift.

Chapter 4
Quality Assurance/Quality Control

Quality control (QC) procedures were performed in accordance with the quality management plan (QMP) for the AMS pilot[5] and the test/QA plan[2] for this verification test.

4.1 Data Review and Validation

Test data were reviewed and approved according to the AMS pilot QMP,[5] the test/QA plan,[2] and Battelle's one-over-one policy. The Verification Test Coordinator, or the Verification Test Leader, reviewed the raw data and the data sheets that were generated each day and approved them by adding their signature and the date. Laboratory record notebook entries were also reviewed, signed, and dated.

4.2 Deviations from the Test/QA Plan

During the preparation and performance of the verification test, deviations from the test/QA plan were implemented to better accommodate differences in vendor equipment and other changes or improvements. Any deviation required the approval signature of Battelle's Verification Testing Leader. A planned deviation report form was used for documentation and approval of the following changes:

1. Commercial food coloring dye was used for the color test instead of diluted color standard owing to the strongly acidic nature of the cobalt-platinum standard solution.
2. Calibration of the pH meter was performed only once during the test, and the meter was not readjusted to account for variations in ambient temperature. Recalibration was to be performed under the conditions of the test. However, the pH measurements were used only to assess changes and not for absolute measurements.
3. Only one in-line filter was used in the recirculation system.
4. The schedule of tests was lengthened and the order of testing was changed to better group series of parameter evaluations and to respond to unexpected experimental results.

These deviations had no significant impact on the test results used to verify the performance of the on-line turbidimeters.

4.3 Calibration

4.3.1 Reference Turbidimeters

The reference turbidimeters were calibrated according to the procedures described in their respective instrument manuals. The calibrations were performed on August 23, 1999. Calibration was performed using a blank, and 20, 200, 2000, and 7500 NTU StablCal calibration standards (Hach Company, Loveland, Colorado). After calibration and before proceeding with the verification test, the calibration of each reference turbidimeter also was checked through a five-point linearity test using solutions with the following turbidities: < 0.1, 0.3, 0.5, 2, and 5 NTU. The < 0.1, 0.3, and 0.5 NTU solutions were purchased and used as is, whereas the 2 and 5 NTU solutions were prepared by diluting a purchased 20 NTU StablCal formazin standard solution. The results of the linearity check are summarized in Table 4-1, indicating that the two reference turbidimeters gave essentially identical results. For each reference turbidimeter, the slope of this linear fit was within the 0.90 and 1.10 limits prescribed in the test/QA plan,(2) and each fit had an $r^2 > 0.98$ as called for in the test/QA plan.(2)

Table 4-1. Results of Linearity Check of Reference Turbidimeters

Parameter	Hach 2100AN IS (ISO 7027)	Hach 2100AN (180.1)
Slope	1.086	1.086
Intercept	0.0038	0.0101
r^2	0.9991	0.9996

The calibration of each reference turbidimeter also was checked both before and after each series of test measurements, using a nominal 0.5 NTU StablCal standard solution. The reference turbidimeters were to be recalibrated if agreement between the turbidity reading and the certified 0.521 NTU turbidity value of this standard solution was not within ± 10% (i.e., 0.469 - 0.573 NTU). If this calibration check criterion was met before but not after a series of test measurements, those measurements were to be repeated after recalibration of the reference turbidimeters. Throughout the course of the verification test, neither reference turbidimeter was ever found to be out of calibration, and consequently no recalibration of the reference turbidimeters was performed.

Before the background readings were measured for the detection limit determination, an additional calibration check with < 0.1 NTU standard also was performed on the reference turbidimeters to ensure proper calibration at low levels. These calibration checks were performed on September 9, 1999, for the initial linearity test, and October 20, 1999, for the final linearity test. The results showed agreement within 0.02 NTU between the turbidity reading of the < 0.1 NTU standard and the value as reported on the certificate of analysis.

4.3.2 Temperature Sensors

A Fluke 52 thermocouple (Battelle Asset Number 570080) was used throughout the verification test to determine water temperature, and the ambient room temperature. This thermocouple was calibrated on June 30, 1999, against a calibrated temperature standard (Fluke 5500A, Battelle Asset Number SN-714755).

4.3.3 Flow Meters

The flow meter used in the verification test to measure the water flow through the Sigrist WTM500 turbidimeter was a panel-mounted, direct-reading meter purchased from Cole-Parmer (Catalog Number P-03248-56), capable of measuring up to 1 gpm. The flow meter was factory calibrated and was checked once during the verification test by measuring the time required to fill a container of known volume through the meter at a setting of 0.8 gpm. Table 4-2 summarizes the results of the flow rate checks.

Table 4-2. Summary of Flow Meter Calibration Check

Flow Meter Setting (gpm)	Volume (gallon)	Time (seconds)	Calculated Rate (gpm)
0.8	2	143	0.84
0.8	4	299	0.80

The calibration check was performed on August 26, 1999, and indicated agreement within the 10% criterion established in the test/QA plan[2] at this flow rate.

4.3.4 pH Meter

Calibration of the pH meter was performed once during the verification test with no further adjustment of the meter. Calibration included standardization at a pH of 7 and a pH of 10 using buffer solutions. Calibration checks performed during the color test indicated a bias of 0.1 to 0.3 pH units. Biases above 0.2 pH units fall outside of the acceptance criterion for the verification test and introduce an uncertainty to the absolute magnitude of the pH readings. However, the pH readings were recorded as a means of assessing if changes in the acidity of the solution occurred as a result of adding the color solution, rather than as an absolute measure of the pH itself. The pH readings recorded during the test indicated no evidence of pH change in the test solution as the result of adding dye to the test solution.

4.4 Data Collection

Electronic data were collected and stored by a PC-based data acquisition system using LabTech Notebook software (Version 8.0.1). Data were collected from the Sigrist WTM500 turbidimeter every 10 seconds over much of the course of verification testing. These data were saved in ASCII files along with the time of collection. Data files were stored electronically both on the hard drive of the data collection system and on floppy discs for backup purposes. Data collected manually included turbidity readings of the reference turbidimeters, flow rates, and water and ambient air temperature measurements. An example of the data recording sheet used to record these data is shown in Appendix A.

4.5 Assessments and Audits

4.5.1 Technical Systems Audit

Battelle's Quality Manager performed a technical systems audit once during the verification test. The purpose of this audit was to ensure that the verification test was performed in accordance with the test/QA plan(2) and that all QA/QC procedures were implemented. In this audit, the Quality Manager reviewed the calibration standards and reference methods used, compared actual test procedures with those specified in the test/QA plan, and reviewed data acquisition and handling procedures. A report on this audit is provided in Appendix B.

4.5.2 Performance Evaluation Audit

Performance evaluation audits were conducted to assess the quality of the measurements made in the verification test. These audits addressed only those measurements made by Battelle staff in conducting the verification test, i.e., the reference turbidimeter readings and temperature measurements. The audits were conducted by analyzing the standards or comparing them with references that were independent of those used in the verification test. Each audit was made at least once during the verification test.

The audit of the reference turbidimeters was performed by analyzing a reference solution that was independent of the formazin standards used for calibration of the reference turbidimeters during the verification test. The independent reference solution was an AMCO-AEPA-1 0.500 NTU standard solution obtained from APS Analytical Standards, Redwood City, California. This audit was conducted once daily throughout the verification test and served as an independent verification of the calibration of the reference turbidimeters. Agreement between the National Institute of Standards and Technology (NIST) traceable turbidity value of the AMCO-AEPA-1 solution and the turbidity readings from each reference turbidimeter was recorded and tracked graphically using a control chart. Furthermore, similar calibration assessments were performed daily using a purchased 0.521 NTU StablCal formazin standard (Hach Company, Loveland, Colorado), as described in Section 4.3.1. The results of these StablCal daily calibration assessments always showed agreement between the turbidity reading from each reference turbidimeter and the certified turbidity within ± 10%, as required in the test/QA plan.(2) The results of the daily calibration assessments are shown in Figures 4-1a and 4-1b for both the AMCO-AEPA-1 standard and the formazin standard, on the 2100AN IS (ISO 7027) and 2100AN (180.1) reference turbidimeters, respectively. (The dashed lines in the upper parts of Figures 4-1a and 4-1b are at intervals of 0.05 NTU, but are for visual reference only and are not exactly the ± 10% control limits of the calibration checks. The bottom portion of each figure shows the ± 10%

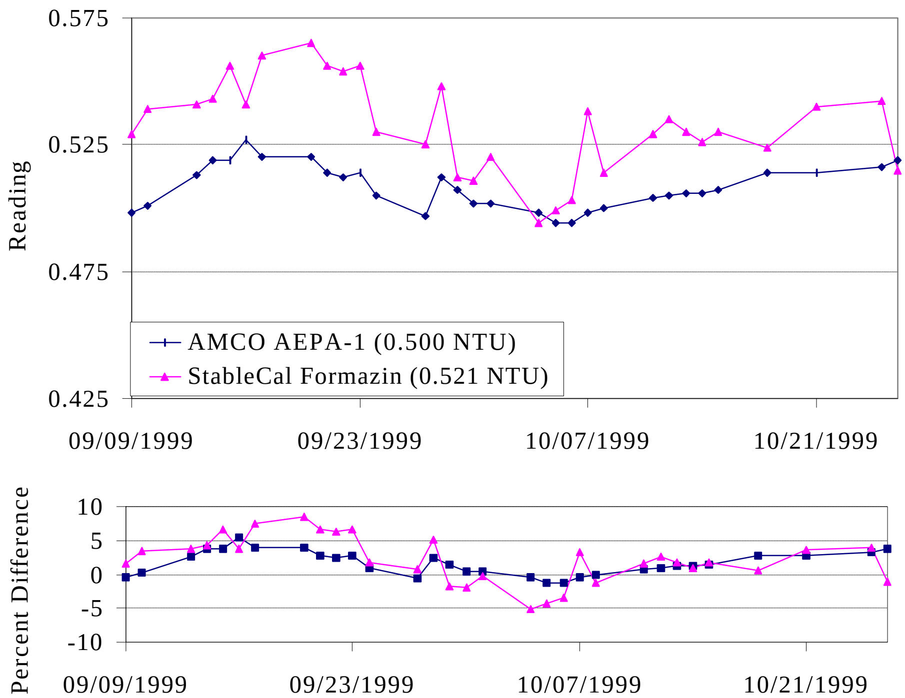

Figure 4-1a. Control Chart for Performance Evaluation Calibration Checks of ISO 7027 Reference Turbidimeter

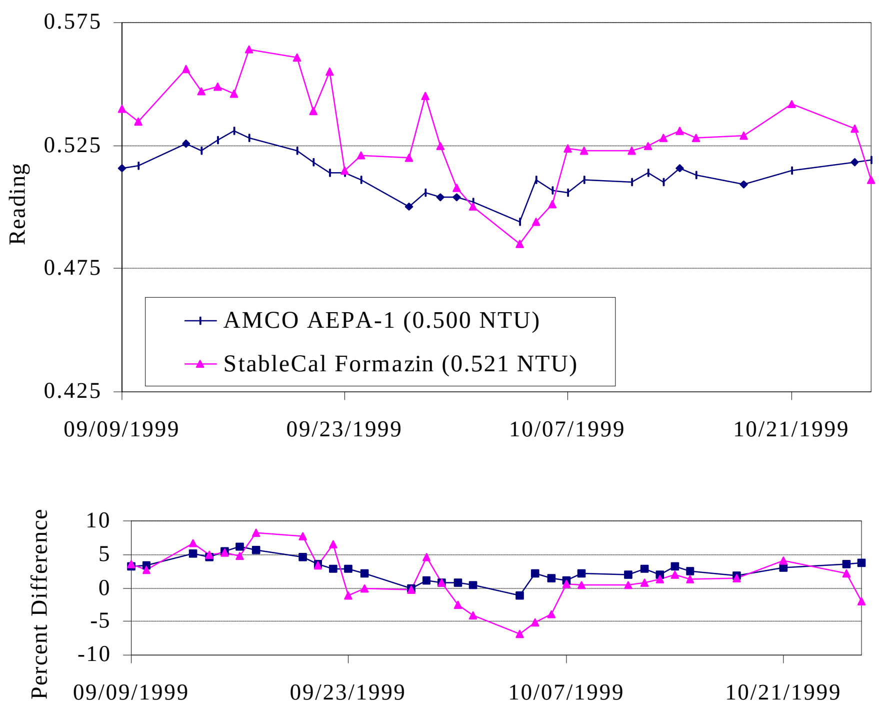

Figure 4-1b. Control Chart for Performance Evaluation Calibration Checks of Method 180.1 Reference Turbidimeter

control limits.) Throughout the course of the verification test, readings of the AMCO-AEPA-1 standard, as measured by the ISO 7027 reference turbidimeter, ranged from - 1.2% to + 6.2% relative to the certified turbidity value for that standard, and were on average ~ 2.7% higher. For the Method 180.1 turbidimeter, the range was - 1.2% to + 5.4% with an average reading that was 1.7% higher than the certified turbidity value. The daily fluctuations in these measurements resulted in standard deviations of ~ 1.7% for each reference turbidimeter. Similarly, readings of the formazin standard ranged from - 5.2% to + 8.4% for the ISO 7027 turbidimeter and from - 6.9% to + 8.3% for the Method 180.1. The average readings were higher than the certified turbidity value by ~ 2.2% when measured by the ISO 7027 turbidimeter, and by ~ 1.6% for the Method 180.1 turbidimeter, with standard deviations of 3.5% and 3.7%, respectively. Although the average deviations from the true turbidity values for these standards were approximately the same, the scatter in the readings was greater in the formazin readings.

The audit of the thermocouple used during the verification test consisted of a comparison of the temperature readings from the thermocouple with those of an independent temperature sensor. The thermocouple was checked for accuracy by comparison with an American Society for Testing and Materials mercury-in-glass thermometer in the Battelle Instrument Laboratory on October 13, 1999, and again on November 1, 1999. Those comparisons were done at ambient temperature, and the results are shown in Table 4-3.

Table 4-3. Results of Calibration Checks of Thermocouple Used in the Verification Test

	October 13, 1999	November 1, 1999
Fluke 52 Thermocouple	27.2°C	29.5°C
ASTM Mercury-in-Glass Thermometer	27.2°C	29.7°C

Agreement between the thermocouple used in the verification test and the mercury-in-glass thermometer was well within the two-degree specification established in the test/QA plan.[2]

4.5.3 Verification Test Data Audit

Battelle's Quality Manager audited at least 10% of the verification data acquired during the verification test. The Quality Manager traced the data from initial acquisition, through reduction and statistical comparisons, and to final reporting. All calculations performed on the data undergoing the audit were checked.

4.6 Audit Reporting

Each assessment and audit was documented in accordance with Section 2.9.7 of the Quality Management Plan for the AMS pilot.[5] The assessment report included the following:

- Identification of any adverse findings or potential problems
- Response to adverse findings or potential problems.

A copy of the Technical Systems Audit Report is included as Appendix B of this report.

Chapter 5
Statistical Methods

5.1 Off-Line Testing

The turbidimeter performance characteristics were quantified on the basis of statistical comparisons of the test data. This process began by converting the files that resulted from the data acquisition process into spreadsheet data files suitable for data analysis. The following statistical procedures were used to make the comparisons.

5.1.1 Linearity

Linearity was assessed by linear regression, with the reference turbidity reading (*R*) as an independent variable and the turbidimeter response (*T*) as a dependent variable. The regression model was

$$T = m_1 \times R + b$$

where μ_1 and β are the slope and intercept of the response curve, respectively. The turbidimeter performance was assessed in terms of the slope, intercept, and the square of the correlation coefficient of the regression analysis.

5.1.2 Accuracy

The accuracy of the turbidimeter with respect to the reference method was assessed in terms of the average relative bias (B), as follows:

$$B = \overline{\left(\frac{(R - T)}{R}\right)} \times 100$$

where *R* is the turbidity reading of the reference turbidimeter, and T is the corresponding turbidity reading of the Sigrist WTM500 turbidimeter.

Accuracy relative to the reference turbidimeter was assessed both for the prepared solutions and the samples from the plant water stream. The accuracy of the Sigrist WTM500 turbidimeter was assessed relative to the ISO 7027 reference method for verification purposes and relative to the 180.1 reference method as an additional illustration of performance.

5.1.3 Precision

Precision was reported in terms of the percent relative standard deviation (RSD) of a group of similar measurements. For a set of turbidity measurements given by T_1, T_2, ..., T_n, the standard deviation (*S*) of these measurements is

$$S = \left[\frac{1}{n-1} \sum_{k=1}^{n} (T_k - \overline{T})^2 \right]^{1/2}$$

where $\overline{T}$ is the average of the turbidity readings. The RSD is calculated as follows:

$$RSD = \frac{S}{\overline{T}} \times 100$$

and is a measure of the dispersion of the measurements relative to the average value of the measurements. This approach was applied to the groups of replicate measurements on each test solution. In some cases, the turbidity of the prepared solution changed approximately linearly with time, due to loss of particles in the recirculation system. In those cases, a linear regression of the data was performed to assess the slope of the turbidity change as a function of time. This slope was used to adjust the individual turbidity readings to approximately the initial concentration. The precision was then calculated on the adjusted values as described above.

5.1.4 Water Temperature Effects

The effect of water temperature on the response of the Sigrist WTM500 at 0.3 NTU and 5 NTU was assessed by trend analysis. The turbidity readings relative to the ISO 7027 reference turbidimeter were analyzed as a function of water temperature to identify trends in the relative turbidity at each of the two levels of turbidity. The calculations were performed using separate linear regression analyses for the data at each turbidity level. A similar calculation was done for illustrative purposes using the 180.1 reference data.

5.1.5 Flow Rate Sensitivity

Analysis of flow rate influence on turbidity readings was similar to that for water temperature effects. The turbidimeter response relative to the ISO 7027 reference turbidimeter was analyzed as a function of flow rate to assess trends in the response of the turbidimeter with changes in sample flow rate. The analyses were performed separately for the 0.3 NTU and 5 NTU data. A similar calculation was done for illustrative purposes using the 180.1 reference data.

5.1.6 Color Effects

The influence of color on turbidity was assessed through a linear regression analysis of the turbidity measured for each color relative to the ISO 7027 reference turbidimeter. Separate analyses were performed for the measurements recorded at 0.1 NTU and those recorded at 5 NTU. A similar calculation was done for illustrative purposes using the 180.1 reference data.

5.2 On-Line Testing

5.2.1 Accuracy

As described in Section 5.1.2, accuracy in the on-line measurements was determined as a bias relative to the ISO 7027 reference turbidimeter. Daily reference measurements of the sample stream from the water plant were used to assess accuracy. A similar calculation was done for illustrative purposes using the 180.1 reference data.

5.2.2 Drift

Drift was assessed in two ways. The drift in the calibration of the Sigrist WTM500 turbidimeter was assessed by a comparison of the regression analyses of the multi-point linearity tests performed at the beginning and end of the verification test. This comparison was used to establish any long-term drift in instrumental calibration during the verification test. Also, the reference and on-line turbidity results in monitoring the plant water stream were used to assess drift associated with the operation of the instrument (e.g., fouling of the optics, etc.). Trends in the intermediate calibration data toward a positive bias were used to identify when the turbidimeter needed cleaning.

Chapter 6
Test Results

The results of the verification test are presented in this section, based upon the statistical methods of comparison shown in Chapter 5. For all performance characteristics verified, two sets of results are shown. The primary verification results are based on comparisons with the ISO 7027 reference method; a secondary illustration of performance is based on comparisons with the 180.1 reference method.

6.1 Off-Line Testing

Off-line testing was performed to assess the performance of the Sigrist WTM500 turbidimeter when measuring known solutions under controlled conditions. The first of the off-line tests was performed to establish the linearity of the turbidimeter response in the range from < 0.1 to 5 NTU. Data from the linearity test also were used to assess the accuracy and precision of the WTM500 in this turbidity range. After the linearity test, the effects of sample temperature, sample flow rate, and sample color were evaluated. The results of these tests are described in this section.

6.1.1 Linearity

The verification data from the initial linearity test are shown in Figure 6-1a, relative to the ISO 7027 reference turbidimeter. A series of at least five data points was recorded at each of the five nominal turbidity levels (approximately 0.05, 0.3, 0.5, 2, and 5 NTU.) At the two highest NTU levels, a decrease in turbidity was observed in the readings of both the Sigrist WTM500 turbidimeter and the reference turbidimeter. This decrease can be seen graphically as a spread in the data along the slope of the linearity plots. Between the first and fifth readings at 2 NTU, the decrease in turbidity represented 4 to 5% of the initial turbidity as measured by the reference turbidimeter. This decrease in turbidity was likely the result of formazin being lost from the solution in the recirculation system. In an attempt to prevent the formazin loss, the solution was stirred magnetically. A second series of five measurements was recorded at the 2 NTU level after magnetic stirring of the formazin solution was introduced. After magnetic stirring was introduced, the decrease in turbidity was still observed, however, to a slightly lesser extent (approximately 2 to 4%).

The data from the linearity test were fit using a linear regression as described in Section 5.1.1, and the results of these fits are shown in Table 6-1. The secondary comparison with the Method 180.1 data is shown in Figure 6-1b, with the regression results shown in Table 6-1.

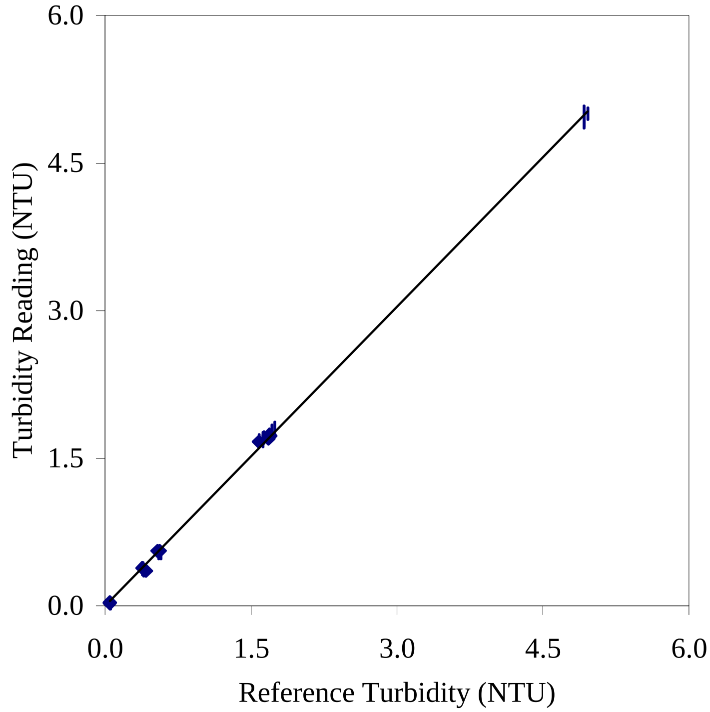

Figure 6-1a. Linearity Plot for Sigrist WTM500 Turbidimeter vs. ISO 7027 Reference Turbidimeter

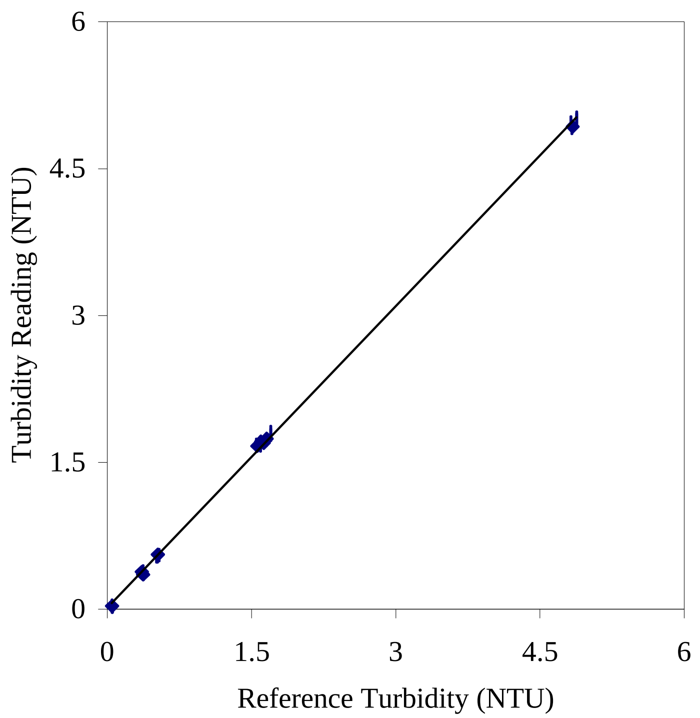

Figure 6-1b. Linearity Plot for Sigrist WTM500 Turbidimeter vs. Method 180.1 Reference Turbidimeter

Table 6-1. Statistical Results of Initial Linearity Test on the Sigrist WTM500 Turbidimeter

Linear Regression Parameter	Verification Results[a]	Secondary Comparison[b]
Slope (std. error)	1.013 (0.005)	1.026 (0.004)
Intercept (std. error)	0.001 (0.010)	0.014 (0.009)
r^2 (std. error)	0.9994 (0.0404)	0.9996 (0.0359)

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

The verification results of the linear regression indicate that the Sigrist WTM500 turbidimeter responded linearly to turbidity throughout the range of about 0.05 to 5 NTU. The slope of the response curve was 1.3% higher than unity with respect to the ISO 7027 reference method. Based on the uncertainty of the reference measurements, the 95% confidence interval of the slope relative to the reference method includes unity. A near zero intercept was determined for the linearity plot; the 95% confidence interval for the intercept includes zero.

The secondary comparison in Table 6-1 shows that the WTM500 also exhibited good linearity relative to Method 180.1.

6.1.2 Accuracy

Data obtained from the initial linearity test were used to assess accuracy for the off-line tests. The results of the accuracy verification are given in Table 6-2 and are presented as the average difference between the Sigrist WTM500 turbidimeter and the reference turbidimeter, as well as the relative bias of the Sigrist WTM500 turbidimeter with respect to the reference measurements. Negative values indicate a negative bias in the Sigrist WTM500 turbidimeter readings when compared with the reference turbidimeter, and positive numbers indicate a positive bias in the Sigrist WTM500 readings.

The verification results in Table 6-2 show a bias of about 1 to 5% over all turbidity levels from 0.3 to 5 NTU, resulting from average measured differences of 0.005 to 0.065 NTU. No trend of the average bias with NTU level is evident. The observed bias is comparable to the degree of fluctuations in the daily calibration checks of the reference turbidimeter.

The secondary comparison in Table 6-2 shows similar performance relative to Method 180.1, with average bias results of 1 to 7%.

Table 6-2. Bias of Sigrist WTM500 Turbidimeter Relative to Reference Measurements on Prepared Test Solutions

	Verification Results[a]		Secondary Comparison[b]	
Nominal Turbidity of Test Solution (NTU)	Average Difference (NTU)	Relative Bias (%)	Average Difference (NTU)	Relative Bias (%)
0.3	-0.0211	-5.2	0.0045	1.3
0.5	-0.0054	-0.9	0.0258	4.9
2	0.0650	5.1	0.0970	7.0
5	0.0390	0.8	0.1170	2.4

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

6.1.3 Precision

Data from the linearity test were used to calculate precision at 0.3, 0.5, 2, and 5 NTU. At both the 2 NTU and 5 NTU levels, a decrease in turbidity was observed as a function of time during the test procedure. To account for this variability in turbidity, the readings at these two levels were analyzed by linear regression against time and adjusted to approximately the initial turbidity value using correction factors based on the regression results. The adjusted values (T_i') were calculated using the following equation:

$$T_i' = T_i + c(t_i - t_0)$$

where T_i is the ith turbidity reading, t_i is the time at which the ith sample was collected, t_0 is the time of collection for the initial sample in the series, and c is the slope of the line determined from the linear regression results of turbidity versus time at 2 NTU or at 5 NTU. The results of the adjustment calculations are given in Table 6-3 for the Sigrist WTM500 turbidimeter. Similar corrections were applied to the reference readings since the reference readings showed the same trend of decreasing turbidity with time.

The precision was calculated from the raw data at the 0.3 and 0.5 NTU levels, and from the corrected data at the 2 NTU and the 5 NTU levels. The results of these calculations are shown in Table 6-4. For comparison, the calculated precision values for the two reference turbidimeters are also included in that table. The values presented in this table are based on five readings at each level, with the exception of the 2 NTU levels, which included ten readings.

Table 6-3. Adjusted Turbidity Readings for Precision Calculations on the Sigrist WTM500

Nominal Value (NTU)	Actual Reading (NTU)	Corrected Reading (NTU)	Nominal Value (NTU)	Actual Reading (NTU)	Corrected Reading (NTU)
2	1.8091	1.8091	5	5.0012	5.0012
2	1.7786	1.7929	5	5.0195	5.0360
2	1.7419	1.7705	5	4.9280	4.9610
2	1.7297	1.7725	5	4.9158	4.9653
2	1.6992	1.7563	5	4.9707	5.0367
2	1.7114	1.7828			
2	1.7053	1.7910			
2	1.6748	1.7748			
2	1.6809	1.7951			
2	1.6687	1.7972			

Table 6-4. Precision of Sigrist WTM500 Turbidimeter and of the Reference Turbidimeters

Nominal Turbidity	Sigrist WTM500		ISO 7027 (2100AN IS)		Method 180.1 (2100AN)	
	SD	RSD (%)	SD	RSD (%)	SD	RSD (%)
0.3 NTU	0.0127	3.4	0.0161	4.1	0.0051	1.4
0.5 NTU	0.0093	1.7	0.0118	2.1	0.0095	1.8
2 NTU	0.0157	0.88	0.0123	0.71	0.0108	0.64
5 NTU	0.0366	0.73	0.0126	0.26	0.0088	0.18

The results of these calculations indicate that the Sigrist WTM500 turbidimeter has approximately the same precision as the reference turbidimeter through the range of turbidity measured in this verification test. From 0.3 to 5 NTU, the WTM500 exhibited precision of 3.4 to 0.7% as RSD.

6.1.4 Water Temperature Effects

The verification data obtained for the temperature test are shown in Figure 6-2a. As a result of loss of formazin in the recirculation system during the temperature test, additional formazin solution was added between each set of temperature measurements to maintain turbidity levels at approximately 0.3 NTU and 5 NTU. Consequently, the absolute turbidity readings alone cannot be used as an indication of temperature effects. Therefore, the readings recorded for the Sigrist WTM500 turbidimeter were normalized to the corresponding reference readings to get a relative measure of turbidity. These relative values (i.e., ratios of WTM500 to ISO 7027 data) are shown in Figure 6-2a and were analyzed by linear regression to assess the effect of water temperature on turbidity reading. The results of the regression analysis are given in Table 6-5.

Table 6-5. Statistical Results of Temperature Test on the Sigrist WTM500 Turbidimeter

Linear Regression Parameter	Verification Results[a]		Secondary Comparison[b]	
	0.3 NTU	5 NTU	0.3 NTU	5 NTU
Slope (std. error)	-0.0009 (0.0018)	0.0011 (0.0014)	-0.0094 (0.0018)	0.0007 (0.0017)
Intercept (std. error)	0.8676 (0.0418)	1.025 (0.030)	0.9493 (0.0417)	1.024 (0.036)
r^2 (std. error)	0.0164 (0.0418)	0.046 (0.024)	0.6614 (0.0417)	0.012 (0.030)

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

These verification results indicate that, relative to the ISO 7027 reference turbidimeter, the Sigrist WTM500 shows no statistically significant relation between the turbidity readings and the water temperature at either 0.3 NTU or at 5 NTU, since the 95% confidence interval includes zero slope in both cases, i.e., water temperature has no effect on WTM500 readings within the tested temperature range.

The secondary results in Figure 6-2b and Table 6-5 suggest a slight negative dependence of turbidity reading on temperature at 0.3 NTU. However, the difference in measurement method

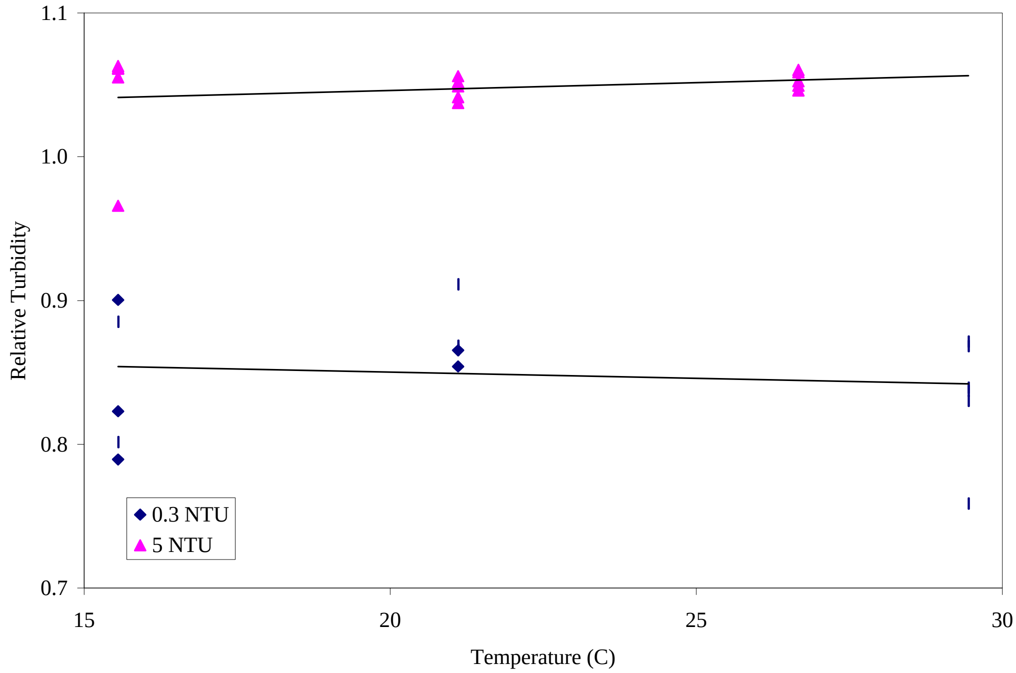

Figure 6-2a. Effect of Temperature on Sigrist WTM500 Turbidity Readings vs. ISO 7027 at Both 0.3 and 5 NTU

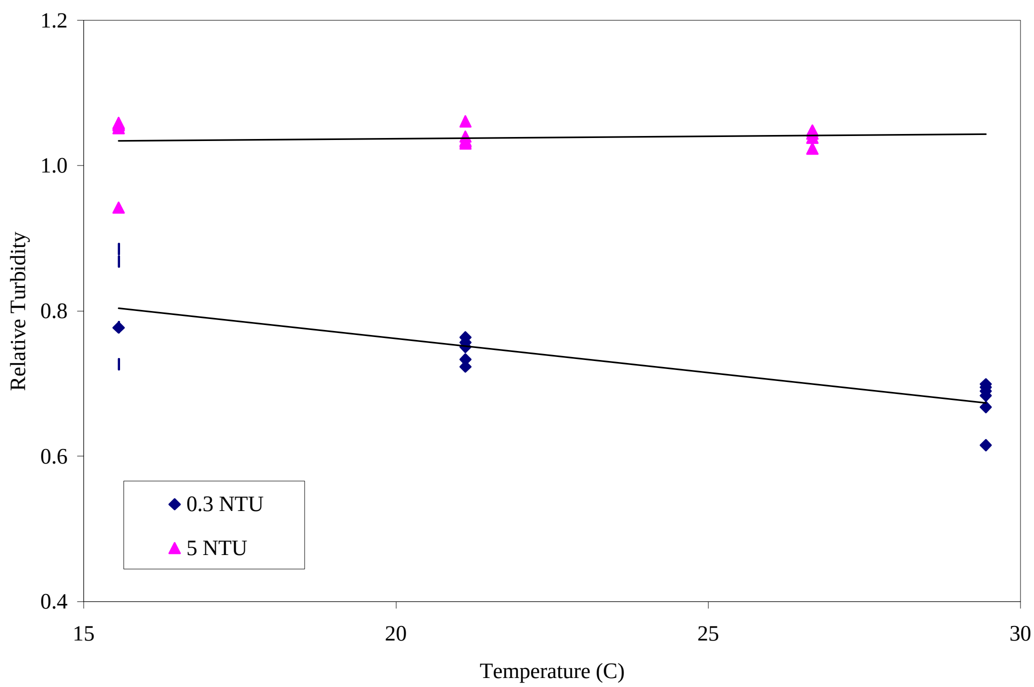

Figure 6-2b. Effect of Temperature on Sigrist WTM500 Turbidity Readings vs. Method 180.1 at Both 0.3 and 5 NTU

between the WTM500 and Method 180.1 may account for this result, rather than any actual temperature dependence of the WTM500.

6.1.5 Flow Rate

The results of the flow rate test are summarized in Figure 6-3. The data are again presented and analyzed as relative turbidity readings, rather than absolute turbidity readings, to account for loss of formazin during the testing. The results of the statistical analysis of the flow data are presented in Table 6-6.

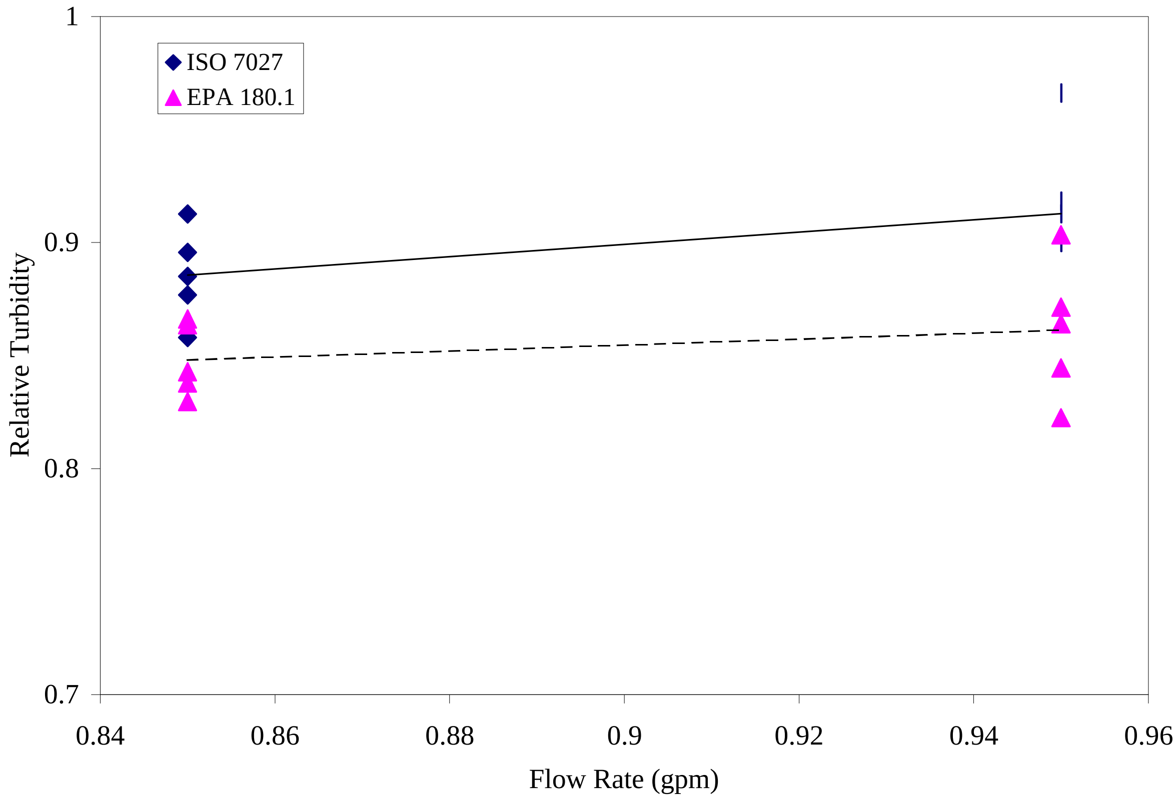

Figure 6-3. Effect of Sample Flow Rate on Sigrist WTM500 Turbidimeter Response

Table 6-6. Statistical Results of Flow Rate Test for the Sigrist WTM500 Turbidimeter

Parameter	Verification Results[a]	Secondary Comparison[b]
Slope (std. error)	0.271 (0.189)	0.131 (0.153)
Intercept (std. error)	0.655 (0.167)	0.736 (0.138)
r^2 (std. error)	0.211 (0.029)	0.084 (0.024)

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

The results show no statistically significant effect of sample flow rate on the response of the Sigrist WTM500 turbidimeter in the range of 0.85 to 0.95 gpm, since at the 95% confidence level the slope values are not significantly different from zero. It should be noted that the specifications of the Sigrist WTM500 turbidimeter require a small range of operational flow rates. It is reasonable that within the specified range no flow rate effects are present.

6.1.6 Color Effects

The verification data obtained from the color tests are shown in Figure 6-4a. In this figure, the data at each color level are plotted as relative values with respect to the reference turbidimeter readings, and the statistical analysis of these data involved a linear regression analysis of the relative data as a function of solution color. At 5 NTU, the background color reading of approximately 30 CU was subtracted, and only the effect of color added during the test is shown. The results of the statistical calculations are summarized in Table 6-7.

The verification results in Table 6-7 show that at the 0.1 NTU level color has no significant effect (95% confidence) on the response of the Sigrist WTM500 turbidimeter. At the 5 NTU level, color has a small but statistically significant effect on the response of the Sigrist WTM500 turbidimeter. This effect amounts to a decrease in turbidity determined by the Sigrist WTM500 turbidimeter on the order of 0.1% per CU increase relative to the reference turbidimeter. Very similar results also are shown in the secondary comparison in Table 6-7.

It is somewhat surprising that the magnitude of this effect is the same relative to both reference turbidimeters. Since the two reference turbidimeters use light sources with different peak wavelengths, the effect of color relative to the two reference turbidimeters would be expected to be different. However, it should be noted that both reference turbidimeters were used in the non-ratio mode in this test, and thus their readings were not compensated for color. Since the WTM500 readings are compensated, this difference may be the cause of the apparent color effect on WTM500 readings.

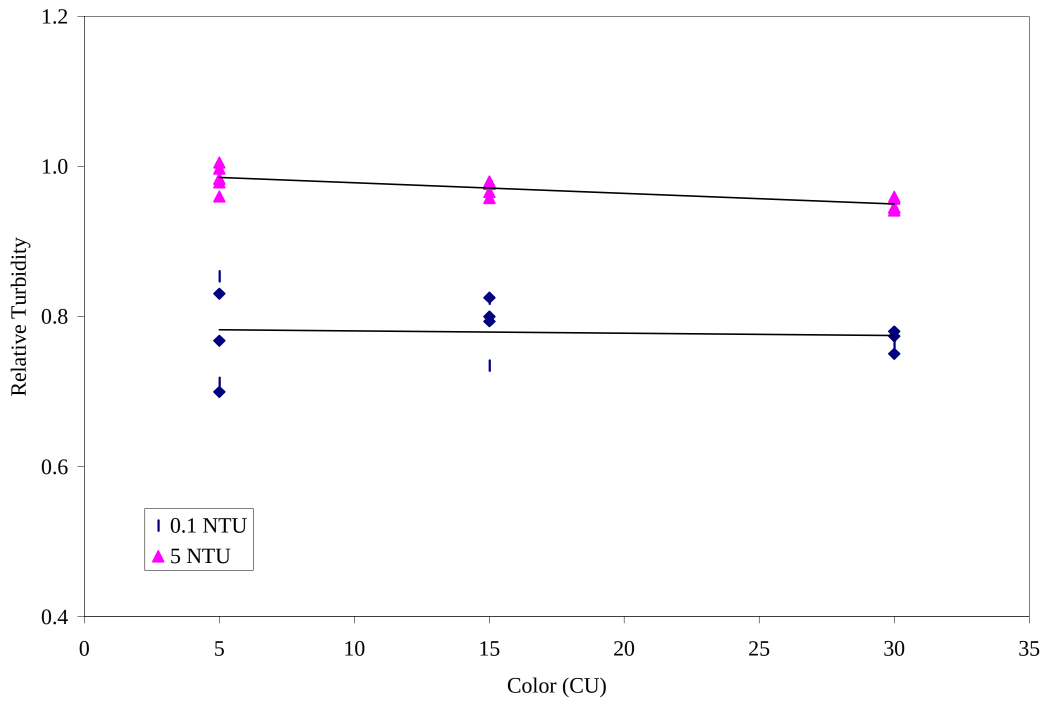

Figure 6-4a. Effect of Color on Relative Turbidity with the Sigrist WTM500 vs. the ISO 7027 at Both 0.1 and 5 NTU

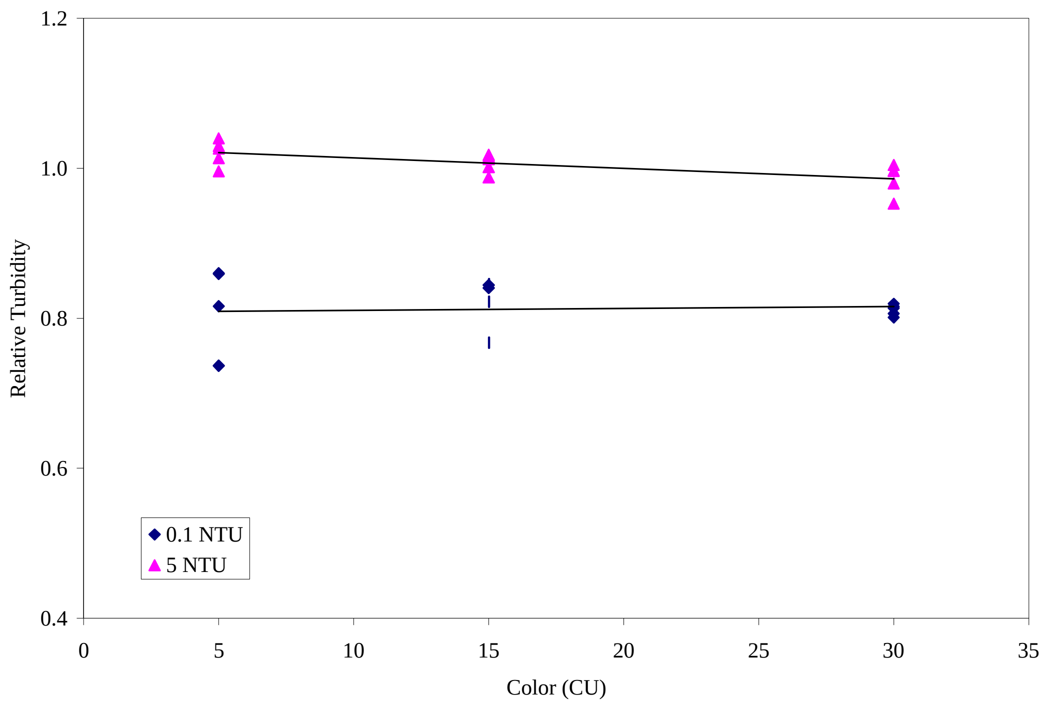

Figure 6-4b. Effect of Color on Relative Turbidity with the Sigrist WTM500 vs. Method 180.1 at Both 0.1 and 5 NTU

Table 6-7. Statistical Results of the Color Test with the Sigrist WTM500 Turbidimeter

Reference:	Verification Results[a]		Secondary Comparison[b]	
Parameter	**0.1 NTU**	**5 NTU**	**0.1 NTU**	**5 NTU**
Slope (std. error)	-0.0003 (0.0011)	-0.0014 (0.0003)	0.0003 (0.0010)	-0.0014 (0.0004)
Intercept (std. error)	0.7838 (0.0224)	0.9925 (0.0058)	0.8076 (0.0198)	1.028 (0.008)
r^2 (std. error)	0.0054 (0.0455)	0.634 (0.012)	0.0056 (0.0403)	0.471 (0.016)

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

6.2 On-Line Testing

Figure 6-5 shows the results from the four weeks of on-line testing. In this figure, data from the Sigrist WTM500 and the reference turbidimeters are shown, along with additional data supplied by the Dublin Road Water Plant (DRWP). Data from the DRWP are from a turbidimeter in the plant sampling the same water stream at a different location, for plant operational purposes. These DRWP data are shown to illustrate the trends in turbidity of the water stream sampled for this test. No quantitative comparisons with the DRWP data should be made, since these data were not collected at the same location as samples for this verification test. For convenience, only one data point per hour is shown for the Sigrist WTM500, although data were recorded at intervals of 10 seconds throughout the on-line testing. Breaks in the data from the Sigrist turbidimeter indicate periods during which the turbidimeter was taken off-line for calibration checks, or for cleaning.

In general, Figure 6-5 illustrates correlation and sometimes close quantitative agreement between the WTM500 and the reference measurements. Also, the varying turbidity levels shown by the WTM500 indicate a temporal pattern similar to that of the DRWP data. Two episodes near the end of the four-week period show large deviations in the Sigrist data from the benchtop measurements. These episodes occurred after adjustments to the recirculation system and are likely to be associated with these modifications. Consequently, data recorded between 10/8 to 10/10, and after 10/12, will not be included in the following discussions of accuracy.

6.2.1 Accuracy

The results from the four weeks of on-line accuracy testing are given in Table 6-8. The results shown in the table are given as the average of the two readings taken each day on water stream samples for the Sigrist WTM500 turbidimeter and the reference turbidimeter. In cases where more than the prescribed two readings were recorded, all the values are included in the reported

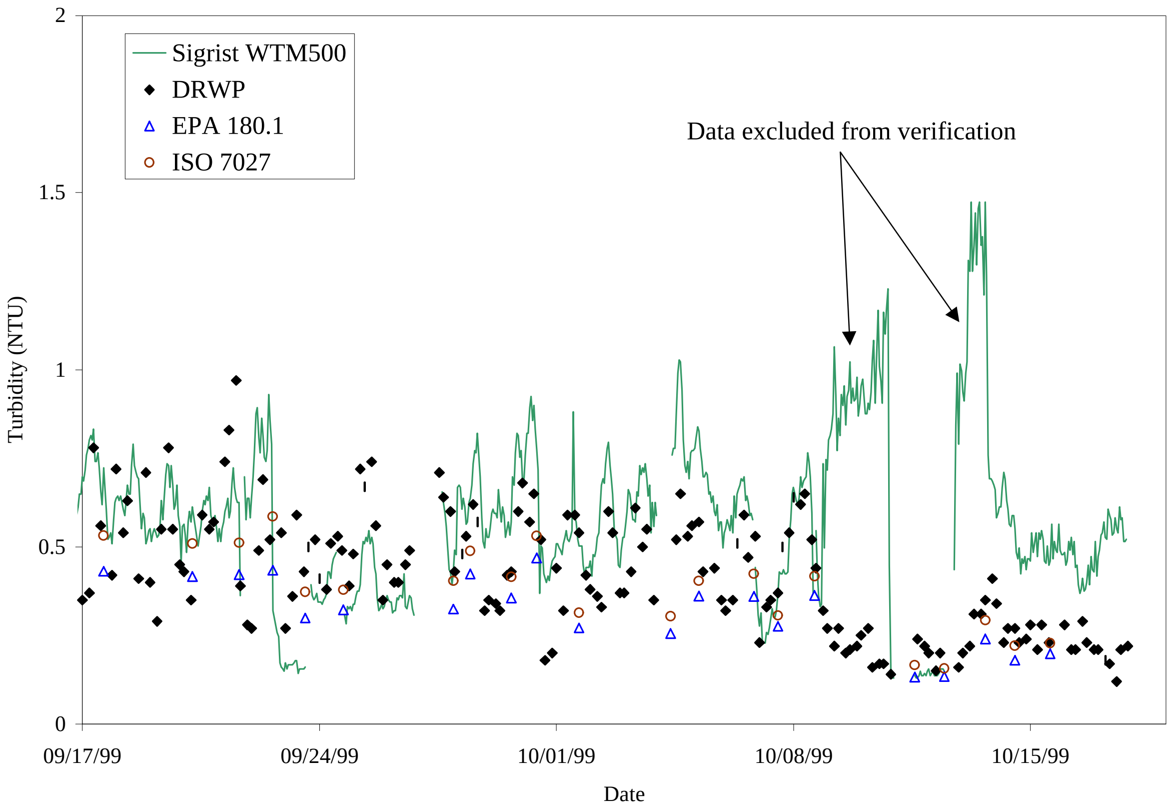

Figure 6-5. Summary of Stream Turbidity Data from On-Line Testing of Sigrist WTM500

average. Additionally, the bias in the Sigrist readings relative to the reference turbidimeter is reported.

The verification results in Table 6-8 show that the WTM500 generally read about 0.05 to 0.2 NTU higher than the ISO 7027 reference turbidimeter within a reference turbidity range of about 0.16 to 0.6 NTU. Positive biases of about 15 to 40% characterize most of this data range. However, near the end of the on-line test the lowest turbidities and best accuracy were observed (i.e., biases of about 0 to -20%). The WTM500 and reference data exhibited a linear regression of the form WTM500 = 1.288 (ISO 7027) + 0.025 NTU, with r^2 = 0.513.

The secondary comparison in Table 6-8 shows somewhat lower accuracy of the WTM500 relative to Method 180.1, as expected, but the same degree of correlation (r^2 = 0.513).

A similar positive bias was observed for all of the on-line turbidimeters tested in this verification test, suggesting a systematic bias in the reference data. It should be noted that, since visible granular deposits accumulated in the test apparatus during the on-line testing, it is possible that a systematic negative bias may have existed as a result of large particles settling in the grab sample vial between sample collection and reference analysis.

Table 6-8. On-Line Daily Accuracy Check Results from Water Stream Samples

Date	Sigrist WTM500 NTU	Verification Results[a] (Relative bias %)	Secondary Comparison[b] (Relative bias %)
9/17/99	0.7044	0.5320 (32.4)	0.4315 (63.2)
9/20/99	0.6067	0.5090 (19.2)	0.4165 (45.7)
9/21/99	0.6250	0.5115 (22.2)	0.4215 (48.3)
9/22/99	0.7944	0.5855 (35.7)	0.4338 (83.1)
9/23/99	0.4389	0.3725 (17.8)	0.2990 (46.8)
9/24/99	0.4755	0.3790 (25.4)	0.3220 (47.7)
9/27/99	0.4755	0.4040 (17.7)	0.3245 (46.5)
9/28/99	0.8814	0.4885 (80.4)	0.4230 (108.4)
9/29/99	0.6006	0.4155 (44.5)	0.3560 (68.7)
9/30/99	0.7593	0.5310 (43.0)	0.4690 (61.9)
10/1/99	0.5151	0.3140 (64.0)	0.2710 (90.1)
10/4/99	0.8661	0.3040 (184.9)	0.2550 (239.6)
10/5/99	0.5803	0.4043 (43.5)	0.3607 (60.9)
10/6/99	0.4023	0.4240 (-5.1)	0.3605 (11.6)
10/7/99	0.3901	0.3065 (27.3)	0.2755 (41.6)
10/8/99	0.3320	0.4173 (-20.4)	0.3627 (-8.5)
10/11/99	0.1459	0.1660 (-12.1)	0.1320 (10.5)
10/12/99	0.1581	0.1570 (0.7)	0.1340 (17.9)

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

6.2.2 Drift

6.2.2.1 Calibration Checks

The results from the twice weekly calibration checks at 0.5 NTU with formazin standards are shown in Figure 6-6 and summarized in Table 6-9.

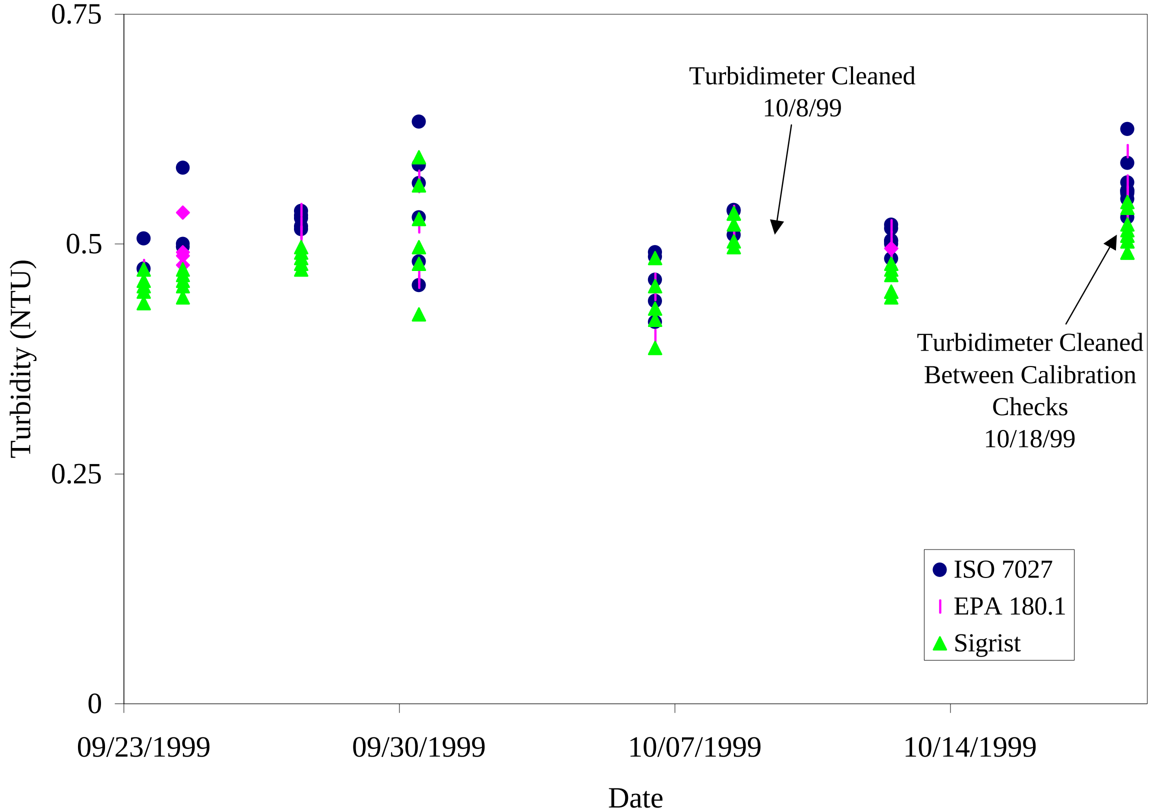

Figure 6-6. Twice-Weekly Calibration Checks During On-Line Testing of the Sigrist WTM500

Table 6-9. Results of Calibration Checks Performed During On-Line Testing

Date	Sigrist WTM500 (NTU)	Verification Results[a] (Relative Bias %)	Secondary Comparison[b] (Relative Bias %)
09/23/99	0.454	0.473 (-4.1)	0.461 (-1.6)
09/24/99	0.459	0.512 (-10.4)	0.492 (-6.8)
09/27/99	0.485	0.526 (-7.9)	0.518 (-6.4)
09/30/99	0.514	0.542 (-5.1)	0.524 (-1.9)
10/06/99	0.435	0.458 (-5.2)	0.432 (0.6)
10/08/99	0.518	0.530 (-2.3)	0.514 (0.6)
10/12/99	0.459	0.505 (-9.0)	0.498 (-7.7)
10/18/99	0.520	0.556 (-6.5)	0.544 (-4.4)
10/18/99	0.505	0.569 (-11.3)	0.544 (-7.2)

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

The verification results in Table 6-9 show that the WTM500 read about 2 to 11% lower than the ISO 7027 reference turbidimeter on the twice-weekly calibration solutions, with an average negative bias of 6.8% (and an average uncertainty of ± 4.6%).

During the initial linearity check (Section 6.1.2), data from the WTM500 showed an average bias of -0.9% ± 3.0% relative to the ISO 7027 reference turbidimeter. No significant drift can be inferred from the results of the initial linearity check and the on-line calibration checks because the uncertainties in these measurements overlap.

Drift associated with optics fouling was not a concern since the Sigrist WTM500 turbidimeter measures turbidity on a falling stream of water, and at no point does the sample stream contact the optics of the turbidimeter.

The secondary comparison data in Table 6-9 show slightly better agreement of the WTM500 with the EPA Method 180.1 results than with the ISO 7027 results (i.e., -3.9% average bias compared to -6.8% relative to ISO 7027).

6.2.2.2 Final Linearity Check

Data from the final linearity check are shown in Figure 6-7a. These data were recorded after completion of the four weeks of on-line testing and after the Sigrist WTM500 turbidimeter had been cleaned. As with the data from the initial linearity test, these data were analyzed by linear regression. The results are summarized in Table 6-10. In Table 6-11, the results of the final linearity test are compared with those from the initial linearity check conducted at the start of the verification as part of the off-line phase.

The verification results of the regression analysis show a high degree of linearity, with a slight negative bias in the slope with respect to the reference turbidimeter and a small negative intercept of less than 0.05 NTU.

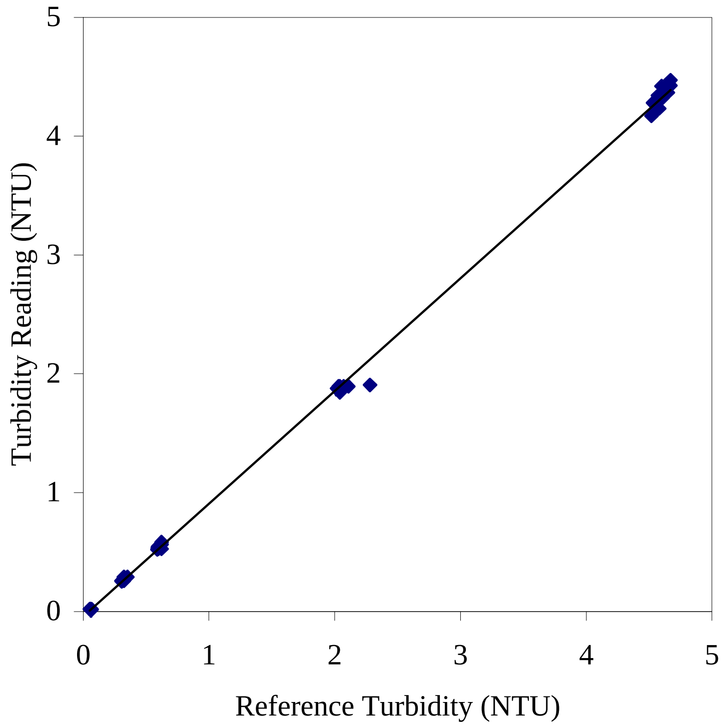

Figure 6-7a. Final Linearity Plot for Sigrist WTM500 vs. ISO 7027 Reference Turbidimeter

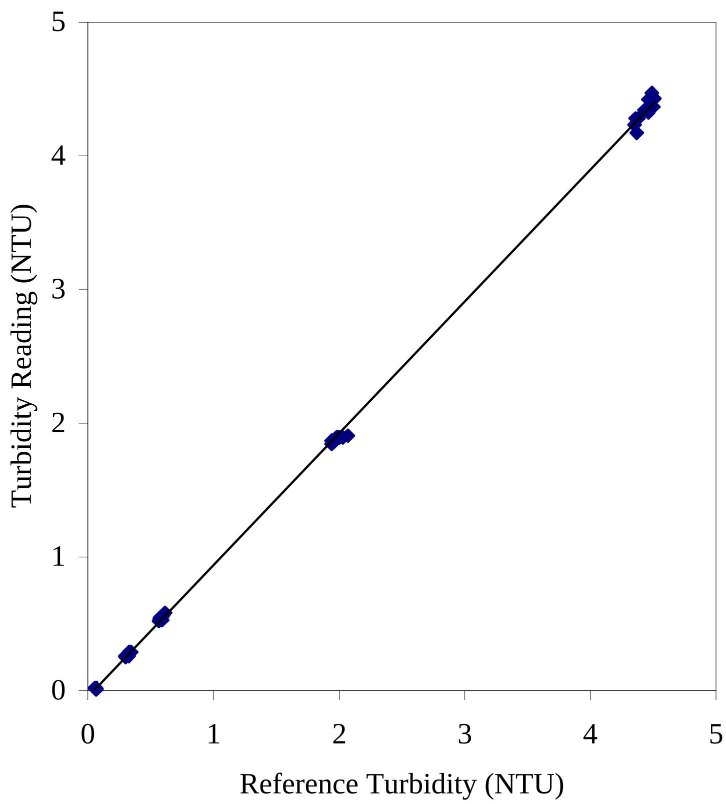

Figure 6-7b. Final Linearity Plot for Sigrist WTM500 vs. Method 180.1 Reference Turbidimeter

Table 6-10. Statistical Results of Final Linearity Test

	Reference Turbidimeter	
Linear Regression	**Verification Results[a]**	**Secondary Comparison[b]**
Slope (std error)	0.949 (0.004)	0.985 (0.003)
Intercept (std error)	-0.042 (0.008)	-0.045 (0.006)
r^2 (std. error)	0.9993 (0.0436)	0.9997 (0.0302)

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

Table 6-11. Comparison of Results from Linearity Tests at Beginning and End of Verification

	Verification Results[a]		Secondary Comparison[b]	
	Slope	**Intercept**	**Slope**	**Intercept**
Initial Linearity Test	1.013	0.001	1.026	0.014
Final Linearity Test	0.949	-0.042	0.985	-0.045
Difference	-0.064	-0.043	-0.041	-0.059
% Difference	6.3	-	4.0	-

[a] Comparison with ISO 7027 reference method (2100AN IS reference turbidimeter).
[b] Comparison with EPA Method 180.1 (2100AN reference turbidimeter).

The verification results in Table 6-11 show a change of 6.3% in the slope of the WTM500 response relative to the ISO 7027 reference method between the initial and final linearity tests. Based on the results of the daily calibration checks, the average difference between the reference turbidimeter readings and the stated turbidity value of the formazin standard used for the checks was 3.2%, with a standard deviation of 2.4%. With these uncertainties, at the 95% confidence level, the initial and final slopes are not significantly different from unity and no drift can be inferred from the difference between the slopes. A very slight change in intercept (0.04 NTU) also was observed. Again, these changes are within the total estimated uncertainty of the reference method, and thus do not definitively indicate significant drift in the WTM500 calibration.

The secondary comparison shown in Table 6-11 leads to a similar conclusion, as a difference of only 4% in slope was observed, relative to the Method 180.1.

6.3 Other Performance Parameters

6.3.1 Cost

As tested, the cost of the Sigrist WTM500 was approximately $4,000.

6.3.2 Maintenance/Operational Factors

Time requirements for installation were not assessed in this test, as temporary installation in the test apparatus did not simulate permanent installation in a water treatment facility. However, the primary time-consuming activities in the installation procedure were securing the “L” bracket to the panel and leveling of the turbidimeter housing. After installation, the Sigrist WTM500 turbidimeter required no operator input and provided data continuously throughout the verification test.

The only maintenance of the Sigrist WTM500 turbidimeter involved occasional cleaning of the sample reservoir. The reservoir was cleaned twice during the on-line testing to remove residues and material deposits that had accumulated. Since the optics in the Sigrist WTM500 turbidimeter never contact the water sample, the optics remained clean throughout the verification test and required no maintenance.

The primary concern with the Sigrist WTM500 turbidimeter is ensuring that the flow through the system remains within the specified narrow limits. On at least one occasion during the test, the housing of the Sigrist WTM500 turbidimeter was flooded as a result of a flow rate above the specified limit. However, flooding caused no damage to the turbidimeter or the housing. After the flooding occurred, the turbidimeter housing was opened and the inside of the housing was dried with paper towels. Proper control of the flow must be maintained to eliminate this potential problem. However, design changes in the WTM500 are being considered to prevent overflow.

Chapter 7
Performance Summary

The Sigrist WTM500 is an on-line turbidimeter designed to provide continuous, real-time measurement of turbidity of aqueous solutions. The Sigrist WTM500 turbidimeter provided linear response over the tested range of < 0.1 to 5 NTU. The slope of the response curve from <0.1 to 5 NTU for the Sigrist WTM500 turbidimeter relative to the ISO 7027 reference turbidimeter was 1.013 at the beginning of this test, with an intercept of 0.001 NTU and r^2 > 0.999.

In measuring standard formazin solutions in the range of 0.3 to 5 NTU, the Sigrist WTM500 and the ISO 7027 reference turbidimeter agreed within 5%, which was comparable to the fluctuations in the daily calibration checks of the reference turbidimeter. The precision in the measurements of the Sigrist WTM500 ranged from 3.4% to 0.7% RSD at turbidities of 0.3 to 5 NTU. These results were approximately the same as for the reference turbidimeter throughout this range of turbidity.

Water temperature had no effect on the response of the Sigrist WTM500 turbidimeter relative to the ISO 7027 method at low turbidity (0.3 NTU) or at higher turbidity (5 NTU). In contrast, there was an effect of color on readings at high turbidity (5 NTU), but none at low turbidity (~ 0.1 NTU). The color effect at 5 NTU resulted in a decrease in the observed turbidity of ~ 0.1% per each CU increase relative to the reference turbidimeters. In the narrow range of flow rates tested for the Sigrist WTM500 turbidimeter (0.85 to 0.95 gpm), there was no statistically significant effect on the turbidity readings as a function of sample flow rate.

In reading the turbidity of treated, unfiltered water from a municipal drinking water plant with a turbidity range of ~ 0.1 to 0.6 NTU, the Sigrist WTM500 turbidimeter usually showed a positive bias of typically ~ 0.05 to 0.2 NTU relative to the reference turbidimeter. Similar results were seen with other on-line turbidimeters verified in this same test. On the other hand, calibration checks of the WTM500 turbidimeter using a nominal 0.5 NTU formazin solution showed a negative bias of 4 to 7% with respect to the reference turbidimeter, indicating a difference in response between the formazin and plant water streams. A systematic bias in the reference readings may have been present in the on-line test phase and may have contributed to the observed differences between the Sigrist WTM500 and reference readings on the water stream samples.

A change of approximately 6% in the slopes of the response curves between the beginning and end of the verification test was observed; however, this change is within the combined experimental uncertainty of the reference measurements over this time period, and does not definitively indicate a calibration drift. A change of approximately 0.04 NTU was observed in the values of the intercepts calculated from the initial and final linearity checks. This degree of change is within the experimental uncertainty of the reference measurements. No apparent drift was observed in the Sigrist WTM500 calibration throughout the on-line testing on the plant water stream.

The Sigrist WTM500 turbidimeter is easy to use and provides continuous on-line turbidity readings. The turbidimeter was cleaned during the test to remove residues and material deposits from inside the system reservoir. However, cleaning the optics was not required since the optics are never in contact with the sample. The flow rate of the sample solution through the turbidimeter must be closely controlled to avoid producing an uneven column of falling water or internal flooding of the turbidimeter housing.

Chapter 8
References

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3. "Determination of Turbidity by Nephelometry," *Methods for the Determination of Inorganic Substances in Environmental Samples*, Method 180.1, EPA/600/R-93/100, U. S. Environmental Protection Agency, Cincinnati, Ohio, August 1993.

4. "Color in Water by Visual Comparison to Standards," *Standard Methods for the Examination of Water and Wastewater*, 18th Edition, Method 2120-B, American Public Health Association, 1992.

5. *Quality Management Plan (QMP) for the ETV Advanced Monitoring Systems Pilot*, U.S. EPA Environmental Technology Verification Program, Battelle, Columbus, Ohio, September 1998.

Appendix A
Example Data Recording Sheet

Appendix B
Technical Systems Audit Report