

Coal Combustion Waste Impoundment Round 7 - Dam Assessment Report

Sibley Generating Station

Fly Ash Pond KCP&L Greater Missouri Operations Company Sibley, Missouri

Prepared for:

United States Environmental Protection Agency Office of Resource Conservation and Recovery

Prepared by:

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INTRODUCTION, SUMMARY CONCLUSIONS AND RECOMMENDATIONS

The release of over five million cubic yards of coal combustion waste from the Tennessee Valley Authority's Kingston, Tennessee facility in December 2008 flooded more than 300 acres of land, damaging homes and property. In response the U.S. EPA is assessing the stability and functionality of the coal combustion ash impoundments and other management units across the country and, as necessary, identifying any needed corrective measures.

This assessment of the stability and functionality of the Sibley Generating Station Fly Ash Pond management unit is based on a review of available documents and on the site assessment conducted by Dewberry personnel on Wednesday, September 22, 2010. We found the supporting technical documentation adequate (Section 1.1.3). As detailed in Section 1.2.5, there are three recommendations based on field observations that may help to maintain a safe and trouble-free operation. A second pond was also observed on site that was used for slag settling; since the pond was incised no dike assessment was required.

In summary, the Sibley Generating Station Fly Ash Pond is SATISFACTORY for continued safe and reliable operation, with no recognized existing or potential management unit safety deficiencies.

PURPOSE AND SCOPE

The U.S. Environmental Protection Agency (EPA) is embarking on an initiative to investigate the potential for catastrophic failure of Coal Combustion Surface Impoundments (i.e., management units) from occurring at electric utilities in an effort to protect lives and property from the consequences of a dam failure or the improper release of impounded slurry. The EPA initiative is intended to identify conditions that may adversely affect the structural stability and functionality of a management unit and its appurtenant structures (if present); to note the extent of deterioration (if present), status of maintenance and/or a need for immediate repair; to evaluate conformity with current design and construction practices; and to determine the hazard potential classification for units not currently classified by the management unit owner or by a state or federal agency. The initiative will address management units that are classified as having a Less-than-Low, Low, Significant or High Hazard Potential ranking. (For Classification, see pp. 3-8 of the 2004 Federal Guidelines for Dam Safety).

In early 2009, the EPA sent its first wave of letters to coal-fired electric utilities seeking information on the safety of surface impoundments and similar facilities that receive liquid-borne material that store or dispose of coal combustion waste. This letter was issued under the authority of the Comprehensive Environmental Response, Compensation, and Liability Act

(CERCLA) Section 104(e), to assist the Agency in assessing the structural stability and functionality of such management units, including which facilities should be visited to perform a safety assessment of the berms, dikes, and dams used in the construction of these impoundments.

EPA requested that utility companies identify all management units including surface impoundments or similar diked or bermed management units or management units designated as landfills that receive liquid-borne material used for the storage or disposal of residuals or by-products from the combustion of coal, including, but not limited to, fly ash, bottom ash, boiler slag, or flue gas emission control residuals. Utility companies provided information on the size, design, age and the amount of material placed in the units. The EPA used the information received from the utilities to determine preliminarily which management units had or potentially could have High Hazard Potential ranking.

The purpose of this report is to evaluate the condition and potential of waste release from management units that have or have not been rated for hazard potential classification. This evaluation included a site visit. Prior to conducting the site visit, a two-person team reviewed the information submitted to EPA, reviewed any relevant publicly available information from state or federal agencies regarding the unit hazard potential classification (if any) and accepted information provided via telephone communication with the management unit owner. After the field visit additional information was received by Dewberry & Davis LLC about the Sibley Generating Station Fly Ash Pond that was reviewed and used in preparation of this report.

Factors considered in determining the hazard potential classification of the management units(s) included the age and size of the impoundment, the quantity of coal combustion residuals or by-products that were stored or disposed of in these impoundments, its past operating history, and its geographic location relative to down gradient population centers and/or sensitive environmental systems.

This report presents the opinion of the assessment team as to the potential of catastrophic failure and reports on the condition of the management unit(s).

LIMITATIONS

The assessment of dam safety reported herein is based on field observations and review of readily available information provided by the owner/operator of the subject coal combustion waste management unit(s). Qualified Dewberry engineering personnel performed the field observations and review and made the assessment in conformance with the required scope of work and in accordance with reasonable and acceptable engineering practices. No other warranty, either written or implied, is made with regard to our assessment of dam safety.

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Doc 01:	Aerial Map
Doc 02:	Site Plan
Doc 03:	Steam Electric Questionnaire
Doc 03a:	Kansas City Power & Light Response to EPA RFI
Doc 04:	Grading Plan Area II, Drawing Y3 dated December 29, 1976
Doc 05:	Grading Plan Area III, Drawing Y4 dated December 29, 1976
Doc 06:	Inspection Report, dated March 5, 2009
Doc 07:	Missouri Operating Permit
Doc 08:	Fly Ash Grading and Drainage Plan Drawing S103 dated August 8, 1992
Doc 09:	Construction permit for fly ash pond modification
Doc 10:	Outfall Structure, Drawing Y13 dated December 29, 1976
Doc 11:	Inflow design flood analysis
Doc 12:	Slope stability analysis
Doc 13	Dam breach analysis
Doc. 14:	Soil Boring Logs

Appendix B

Doc. 16:	Dam Inspection Check List Form- Fly ash pond
Doc. 17:	Dam Inspection Check List Form- Slag settling pond



1.0 CONCLUSIONS AND RECOMMENDATIONS

1.1 CONCLUSIONS

Conclusions are based on visual observations from a one-day site visit and review of technical documentation provided by Kansas City Power and Light (KCP&L) Greater Missouri Operations (GMO).

1.1.1 Conclusions Regarding the Structural Soundness of the Management Unit(s)

The dike embankments and spillway appear to be structurally sound based on a review of the engineering data provided by the owner's technical staff and Dewberry engineers' observations during the site visit. However the slope stability analysis was limited, and did not include long term static or seismic events.

1.1.2 Conclusions Regarding the Hydrologic/Hydraulic Safety of the Management Unit(s)

Hydrologic and hydraulic data performed by Dewberry indicate adequate impoundment capacity to contain the 1 percent probability design storm without overtopping the dikes.

1.1.3 Conclusions Regarding the Adequacy of Supporting Technical Documentation

The supporting technical documentation is adequate. Engineering documentation reviewed is referenced in Appendix A.

1.1.4 Conclusions Regarding the Description of the Management Unit(s)

The description of the management unit provided by KCP&L GMO was an accurate representation of what Dewberry observed in the field.

1.1.5 Conclusions Regarding the Field Observations

Dewberry staff was provided access to all areas in the vicinity of the management units required to conduct a thorough field observation. The visible parts of the dike embankments and outlet structure were observed to have no signs of overstress, significant settlement, shear failure, or other signs of instability, although visual observations were hampered by the presence of thick vegetation in some areas. Embankments visually appear

structurally sound. There are no indications of unsafe conditions or conditions needing remedial action.

1.1.6 Conclusions Regarding the Adequacy of Maintenance and Methods of Operation

The current maintenance and methods of operation appear to be adequate for the fly ash management unit. There was no evidence of repaired embankments or prior releases observed during the field inspection. Dewberry identified the need for brush clearing and re-sodding on the North dike; a geotechnical engineering firm should be consulted to develop a plan to properly remove brush and re-sod the slope.

1.1.7 Conclusions Regarding the Adequacy of the Surveillance and Monitoring Program

The surveillance program appears to be adequate. The management unit dikes are not instrumented. Based on the size of the dikes, the history of satisfactory performance and the current inspection program, installation of a dike monitoring system is not needed at this time.

1.1.8 Classification Regarding Suitability for Continued Safe and Reliable Operation

The facility is SATISFACTORY for continued safe and reliable operation. No existing or potential management unit safety deficiencies are recognized. Acceptable performance is expected under all applicable loading conditions (static, hydrologic) in accordance with the applicable criteria.

1.2 RECOMMENDATIONS

1.2.1 Recommendations Regarding the Structural Stability

Recommend performing a stability analysis for seismic loading applied to the steady state loading and a static analysis under rapid draw down condition.



1.2.2 Recommendations Regarding the Maintenance and Methods of Operation

The following recommendations may help maintain safe and trouble-free operation:

- Monitor encroachment of vegetation.
- Employ a Geotechnical Engineer to develop a program to safely remove large trees and woody brush and replace with grasses.
- Dewberry recommends that an operations and maintenance (O&M) procedures document be created that includes a Record of Maintenance.

1.3 PARTICIPANTS AND ACKNOWLEDGEMENT

1.3.1 List of Participants

Paul Ling, Kansas City Power & Light Steve Brooks, Kansas City Power & Light Bob Beck, Kansas City Power & Light Michael McLaren, S.E., P.E., PSA-Dewberry Andrew Cueto, P.E., Dewberry

1.3.2 Acknowledgement and Signature

We acknowledge that the management unit referenced herein has been assessed on September 22, 2010. Andrew Cueto, PE, PMP McLaren, PE (MO

2.0 DESCRIPTION OF THE COAL COMBUSTION WASTE MANAGEMENT UNIT(S)

2.1 LOCATION AND GENERAL DESCRIPTION

The Sibley Generating Station is located by the Missouri River bank near Sibley, MO. The plant is operated by KCP&L GMO. The Fly Ash Pond is adjacent to the plant. A project location map is provided in Appendix A – Doc. 02. An aerial photograph of the impoundment is provided in Appendix A – Doc. 01.

The Sibley Generating Station Fly Ash Pond is a continuous native clayey fill embankment that impounds fly ash and pond water. It was constructed in 1977.

The maximum height of the dike is 18 feet. The impoundment area is approximately 15.0 acres and has a storage capacity of 361,000 cubic yards (223.8 acre-feet) (See Appendix A – Doc. 3). Construction began on the dike in 1977, and the plant opened for operation in 1977. Between 1993 and 1994, the west end of the pond was filled (75 x 125 feet) for placement of a new silo.

2.2 SIZE AND HAZARD CLASSIFICATION

The classification for size, based on the height of the dam is "Small" and based on the storage capacity is "Small" in accordance with the USACE Recommended Guidelines for Safety Inspection of Dams ER 1110-2-106 criteria summarized in Table 2.2a.

Table 2.2a: USACE ER 1110-2-106Size Classification			
Impoundment			
Category	Storage (Ac-ft)	Height (ft)	
Small	50 and < 1,000	25 and < 40	
Intermediate	1,000 and < 50,000	40 and < 100	
Large	> 50,000	> 100	

Missouri does not have a dam safety program, and the Sibley Generating Station Fly Ash Pond is not in the National Inventory of Dams, therefore the dike does not have an established hazard classification. Dewberry conducted a qualitative hazard classification based on the 2004 Federal Guidelines for Dam Safety classification system (shown in Table 2.2b).

Table 2.2b: FEMA Federal Guidelines for Dam SafetyHazard Classification					
	Loss of Human Life Economic, Environmental,				
	Lifeline Losses				
Low	None Expected	Low and generally limited to owner			
Significant	None Expected	Yes			
High	Probable. One or more	Yes (but not necessary for			
	expected	classification)			

Loss of human life is not probable in the event of a catastrophic failure of the dikes and a failure of the dikes is expected to have a low economic and environmental impact. Therefore, Dewberry evaluated the fly ash pond as "**low hazard potential**."

2.3 AMOUNT AND TYPE OF RESIDUALS CURRENTLY CONTAINED IN THE UNIT(S) AND MAXIMUM CAPACITY

The data reviewed by Dewberry did include the volume of residuals stored in the fly ash pond at the time of inspection. The pool elevation is approximately 722 feet, and the surface area of the pond is approximately 15.0 acres.

Table 2.3: Amount of Residuals and Maximum Capacity of Unit		
Greene County Fly Ash Pond		
Surface Area (acre) ¹	15.0	
Current Storage Capacity (cubic yards) ¹	9,747,000	
Current Storage Capacity (acre-feet)	223.8	
Total Storage Capacity (cubic yards) ¹	10,260,000	
Total Storage Capacity (acre-feet)	235.5	
Crest Elevation (feet)	725	
Normal Pond Level (feet) 722		

¹ See Appendix A – Doc. 03



2.4 PRINCIPAL PROJECT STRUCTURES

2.4.1 Earth Embankment

The dike is an earthen embankment. The crest width is approximately 20 feet. The perimeter of the dike is approximately 5250 feet. The inside slope of the dike embankment is approximately 2:1 on each dike. The outside slopes of the dike embankment range from approximately 2:1 to 3:1 on the east, west dikes. The outside slope embankment is approximately 3:1 on the north dike and 2:1 on the south dike (See Appendix A – Doc. 04, 05). Much of the south embankment is covered in various species of grasses. The outside slope of the east and north and portions of south embankment are covered in dense vegetation (various species of tall grass. trees and other plants). A small portion of the north embankment is also covered in rip-rap.

Table 2.4.1: Summary of Dike Dimensions and Size				
	East Dike	South Dike	West Dike	North Dike
Dam Height	18'	18'	18'	18'
Crest Width	20'	20'	20'	20'
Length	500'	2350'	150'	2250
Side Slopes (inside)	2:1	2:1	2:1	2:1
Side Slopes (outside)	2:1 to 3:1	2:1	3:1	3:1
Hazard Classification	low	low	low	low

2.4.2 Outlet Structures

The impoundment has a 48" sharp crested weir inlet elevation at 716.0' which discharges through a spillway into the Missouri River.

The impoundment has no emergency spillway.

2.5 CRITICAL INFRASTRUCTURE WITHIN FIVE MILES DOWN GRADIENT

Critical infrastructure inventory data was not provided to Dewberry for review.

Based on available area topographic maps, surface drainage in the area of the Fly Ash Pond is to the northeast. A bend in the Missouri river intercepts surface runoff at the east of the Fly Ash Pond (See Appendix A Doc. 04, 05). Releases from the east side of the impoundment will discharge into the Missouri River. Based on available area aerial photographs and a brief driving tour of the area Dewberry did not identify critical infrastructure assets down gradient of the Fly Ash Pond.

The nearest town, Napoleon, is approximately 7 miles down gradient from the impoundment.



3.0 SUMMARY OF RELEVANT REPORTS, PERMITS, AND INCIDENTS

3.1 SUMMARY OF REPORTS ON THE SAFETY OF THE MANAGEMENT UNIT

KCP&L GMO provided one dam safety report of inspections conducted by State of Missouri Department of Natural Resources. The report provided included:

• Utilicorp-Sibley Generating Station, routine inspection, March 5, 2009,(See Appendix A – Doc. 06)

The 2009 report concluded that the structures appeared to be performing adequately and no conditions were observed that would affect the continued safe operation of the impoundment.

3.2 SUMMARY OF LOCAL, STATE, AND FEDERAL ENVIRONMENTAL PERMITS.

The State of Missouri has not implemented a dam safety program; therefore there is no local or state permit. However, discharge from the impoundment is regulated by the Missouri Department of Natural Resources.

The impoundment has been issued a Missouri State Operating Permit No. MO 0004871 issued November 3, 2000, and expires November 02, 2005 (See Appendix A – Doc 07). KCP&L GMO filed for a renewal of the permit in 2005, MDNR continues to review the permit for reissuance.

3.3 SUMMARY OF SPILL/RELEASE INCIDENTS

Data reviewed by Dewberry did not indicate any spills, unpermitted release, or other performance related problems with the dam.



4.0 SUMMARY OF HISTORY OF CONSTRUCTION AND OPERATION

4.1 SUMMARY OF CONSTRUCTION HISTORY

4.1.1 Original Construction

The Sibley Generating Station Fly Ash Pond was constructed beginning in 1977, and was completed in 1977. The original design crest elevation was 725 feet (See Appendix A – Doc. 04, 05).

4.1.2 Significant Changes/Modifications in Design since Original Construction

Between 1993 and 1994, the west end of the pond was filled (75 x 125 feet) for placement of a new silo also added was a dewatering dike (See Appendix A- Doc. 8).

4.2 SUMMARY OF OPERATIONAL PROCEDURES

4.2.1 Original Operational Procedures

The impoundment was designed and operated for fly ash sedimentation and control. The pond receives plant process waste water, coal combustion waste slurry. Treated (via sedimentation) process water is discharged through an overflow outlet structure.

4.2.2 Significant Changes in Operational Procedures and Original Startup

No documents were provided to indicate any operational procedures have changed.

4.2.3 Current Operational Procedures

Modification in 1994 which added a fly ash silo redirected precipitator ash pneumatically to the new silo. (See Appendix A- Doc. 9).

4.2.4 Other Notable Events since Original Startup

No additional information was provided to Dewberry of other notable events impacting the operation of the impoundment.

5.0 FIELD OBSERVATIONS

5.1 PROJECT OVERVIEW AND SIGNIFICANT FINDINGS

Dewberry personnel Michael McLaren, P.E. and Andrew Cueto, P.E. performed a site visit on Wednesday, September 22, 2010 in company with the participants.

The site visit began at 9:00 AM. The weather was warm and cloudy. Photographs were taken of conditions observed. Selected photographs are included here for ease of visual reference. All pictures were taken by Dewberry personnel during the site visit.

The Dam Inspection Checklist is provided in Appendix B. The overall assessment of the dam was that it was in satisfactory condition and no significant findings were noted.

5.2 SOUTH DIKE

5.2.1 Crest

The crest of the south dike had no signs of depressions, tension cracks, or other indications of settlement or shear failure, and appeared to be in satisfactory conditions. Figure 5.2.1-1 shows the conditions of the crest of the east dike.



Figure 5.2.1-1. Photo Showing Crest/ inside slope of South Dike.

5.2.2 Inside Slope

The inside dike embankments include areas of bare earth. Figure 5.2.1-1 shows the general condition of the unprotected bare earth interior slope of the east dike. Photographs 2 and 6, Appendix B provide additional views of the crest and inside slope of the south dike.

5.3 EAST DIKE

5.3.1 Crest

The crest of the east dike had no signs of any depressions, tension cracks, or other indications of settlement or shear failure, some minor signs of tire rutting, and appeared to be in satisfactory condition. Figure 5.3.1-1 shows the conditions of the dike crest.



Figure 5.3.1-1. East Dike Crest

5.3.2 Upstream/Inside Slope

The inside slope of the east dike is covered with limited vegetation. There were no observed scarps, sloughs, bulging, cracks, or depressions or other indications of slope instability or signs of erosion. Figure 5.3.1-1 shows the general condition of the inside slope of the east dike.

5.3.3 Downstream/Outside Slope and Toe

There were no observed scarps, sloughs, bulging, cracks, or depressions or other indications of slope instability or signs of erosion. The outside slope borders areas of dense vegetation including trees. Figure 5.3.3-1 shows the general condition of the outside slope. Appendix B provides additional views of the outside slopes of the east dike.



Figure 5.3.3-1. Photo Showing Typical Condition of Outside Slope of East Dike

5.4 NORTH DIKE

5.4.1 Crest

The crest of the north dike had no signs of depressions, tension cracks, or other indications of settlement or shear failure, and appeared to be in satisfactory condition. Figure 5.4.1-1 shows the conditions of the dike crest. Photographs 15 - 22, Appendix B provide additional views of the crest of the north dike.



Figure 5.4.1-1. Crest of North Dike

5.4.2 Upstream/Inside Slope

Most of the inside slope of the north dike embankment is covered with limited vegetation. There were no observed scarps, sloughs, bulging, cracks, or depressions or other indications of slope instability or signs of erosion. Figure 5.4.1-1 shows the general condition of the inside slope of the north dike.

5.4.3 Outside Slope and Toe

The outside slope is covered in various species of tall grass, trees and rip rap. There were no observed scarps, sloughs, bulging, cracks, or depressions or other indications of slope instability some limited signs of erosion. The outside slope borders the Missouri River.



Figure 5.4.3-1. Outside Slope of North Dike.



Figure 5.4.3-2. Outside Slope of North Dike Erosion.

5.5 WEST DIKE

5.5.1 Crest

The crest of the west dike had no signs of any depressions, tension cracks, or other indications of settlement or shear failure, and appeared to be in satisfactory conditions. Figure 5.5.1-1 shows the conditions of the dike crest.



Figure 5.5.1-1. Crest of West Dike

5.5.2 Outside Slope

Most of the outside slope is covered in various species of tall grass, and trees. In one area, the outside slope is covered in riprap. There were no observed scarps, sloughs, bulging, cracks, scarps, or depressions or other indications of slope instability or signs of erosion. Figure 5.5.1-1 shows the general condition of the outside dike.

5.6 OUTLET STRUCTURES

5.6.1 Overflow Structure

As described on the discharge stream assembly drawings (See Appendix A- Doc. 10), the impoundment has an 8'-0" x 9'-4" concrete inlet structure with an invert elevation at 722.0' and a steel pipe 12-in diameter which discharges through a spillway into the Missouri River.

The primary overflow structure was observed to be working properly, discharging flow from the pond, and visually appeared to be in satisfactory condition. There was no sign of clogging of the spillway and the water exiting the outlet was flowing clear. Figure 5.6.1-1 shows the main outlet structure. Photographs 12 and 13, Appendix B provide additional views of the spillway riser.



Figure 5.6.1-1. Main Outlet Structure.

5.6.2 Outlet Conduit

The outlet weir appeared to be in good shape and operating normally with no sign of clogging and the water exiting the outlet was flowing clear. Figure 5.6.2-1 shows the water discharging from the main spillway tunnel outfall. Photographs 12 and 13, Appendix B provide additional views of the spillway outfall conduit and channel.



Figure 5.6.2-1. Main Spillway Outfall.

5.6.3 Emergency Spillway

No emergency spillway is present.

5.6.4 Low Level Outlet

No low level outlet is present.



6.0 HYDROLOGIC/HYDRAULIC SAFETY

6.1 SUPPORTING TECHNICAL DOCUMENTATION

6.1.1 Flood of Record

No documentation has been provided about the flood of record.

6.1.2 Inflow Design Flood

Dewberry conducted a hydrologic and hydraulic analysis of the capacity of the Fly Ash Pond to store water from the design storm event (See Appendix A – Doc. 11). The design storm was a 100-year (1 percent probability in a given year), 24-hour event with an estimated intensity of 11.32-inches. The report estimates that the 1 percent probability storm can be retained in the Fly Ash Pond, raising the spillway pond water elevation to about 723 feet, leaving a freeboard of at least 2.0 feet.

6.1.3 Spillway Rating

No spillway hydraulic data was provided for review.

6.1.4 Downstream Flood Analysis

No downstream flood analysis data was provided for review Breach Analysis?

6.2 ADEQUACY OF SUPPORTING TECHNICAL DOCUMENTATION

Supporting documentation reviewed by Dewberry is adequate.

6.3 ASSESSMENT OF HYDROLOGIC/HYDRAULIC SAFETY

Based on the calculations provided in the hydrologic and hydraulic study (See Appendix A – Doc 11) the Fly Ash Pond can retain the 1 percent design storm event with a freeboard safety of at least 2.0 feet. Hence dike failure by overtopping seems improbable.

7.0 STRUCTURAL STABILITY

7.1 SUPPORTING TECHNICAL DOCUMENTATION

7.1.1 Stability Analyses and Load Cases Analyzed

The January 26, 1977 Memorandum Subsurface Recommendation for Fly Ash Pond Missouri Public Service - Sibley, This document (See Appendix A – Doc. 12) includes the original stability analysis for the pond.

The stability analyses included the results of a single loading condition:

• Steady state conditions based on ground water levels measured at the time of the borings.

The stability analyses did not address:

- Seismic loading applied to the steady state loading
- A static analysis under rapid draw down conditions.

Based on the results of the analyses it was concluded that the embankments have stability safety factors at or above the minimum recommended values.

7.1.2 Design Parameters and Parameters of Materials

Documentation provided to Dewberry for review was the January 26, 1977 Memorandum Subsurface Recommendation for Fly Ash Pond Missouri Public Service - Sibley (See Appendix A – Doc. 12).

7.1.3 Uplift and/or Phreatic Surface Assumptions

No documentation of uplift calculations was provided to Dewberry for review. Based on the Geotechnical Findings (See Appendix A – Doc. 14) the initial phreatic surface was assumed to be at the elevation measured in the borings.

7.1.4 Factors of Safety and Base Stresses

The safety factors computed in the Slope Stability Analysis report (See Appendix A - Doc. 12) are listed in Table 7.1.4.

Table 7.1.4 Factor of Safety Sibley Fly Ash Pond					
Location	Loading Condition	US Corps of Engineers Recommended Minimum Safety Factors	Inside Slope	Outside Slope	
North Dike	Steady State	1.5	1.9	1.77	
	Sta 31+00				
North	Steady State	1.5	1.36*	1.21*	
Dike	Sta 46+00				
North	Steady State				
Dike	Sta 34+50	1.5	2.23	1.6	

15 foot bench was added to increase slope stability factor of safety.

Based on Dewberry's observations at the site, the overflow weir discussed in the slope stability analysis report is the only discharge location provided for the impoundment. As the weir outlet is uncontrolled, it does not provide the capability to conduct a rapid drawdown. Therefore Dewberry concurs with the conclusion that the probability of a catastrophic failure due to a rapid drawdown event is low.

7.1.5 Liquefaction Potential

The documentation reviewed by Dewberry did not include an evaluation of liquefaction potential. Foundation soil conditions do not appear to be susceptible to liquefaction.

7.1.6 Critical Geological Conditions

There was no documentation provided to Dewberry that included an evaluation of Critical Geological Conditions.

7.2 ADEQUACY OF SUPPORTING TECHNICAL DOCUMENTATION

Structural stability documentation is not adequate. The slope stability analysis was too limited, and did not include long-term static or seismic events.



7.3 ASSESSMENT OF STRUCTURAL STABILITY

Overall, the structural stability of the dikes appears to be satisfactory based on the following observations during the September 22, 2010 filed visit and dam inspection by Dewberry, available dam inspection report (See Appendix A - Doc. 12):

- The crest appeared free of depressions and no significant vertical or horizontal alignment variations were observed,
- There were no indication of major scarps, sloughs or bulging along the dikes,
- Boils, sinks or uncontrolled seepage was not observed along the slopes, groins or toe of the dikes,
- The computed factors of safety comply with accepted criteria for the condition assessed.

Additional analyses are recommended to address long-term static conditions and seismic events.



8.0 ADEQUACY OF MAINTENANCE AND METHODS OF OPERATION

8.1 OPERATIONAL PROCEDURES

The facility is operated for settling pond and storage of fly ash deposits. Treated coal combustion process waste water is discharged through an overflow outlet structure.

8.2 MAINTENANCE OF THE DAM AND PROJECT FACILITIES

No maintenance plan was supplied to Dewberry for review. Through dam maintenance discussions during the site visit, it appears that the procedures are adequate.

8.3 ASSESSMENT OF MAINTENANCE AND METHODS OF OPERATIONS

8.3.1 Adequacy of Operational Procedures

No operational procedures were supplied to Dewberry for review. Based upon the site visit, however, the current methods of operation appear to be adequate for the fly ash management unit. There was no evidence of prior releases observed during the field inspection. Dewberry recommends that an operations and maintenance (O&M) procedures document be created to formalize onsite activities.

8.3.2 Adequacy of Maintenance

No Record of Maintenance was supplied to Dewberry for review. The current maintenance activities appear to be adequate for the fly ash management unit, based upon discussions during the site visit. There was no evidence of repaired embankments or prior releases observed during the field inspection. Dewberry identified the need for brush clearing and re-sodding on the North dike. Dewberry recommends development of an operations and maintenance (O&M) procedures document that includes creation of a Record of Maintenance.



9.0 ADEQUACY OF SURVEILLANCE AND MONITORING PROGRAM

9.1 SURVEILLANCE PROCEDURES

Weekly Inspections

Weekly inspections are conducted by plant personnel. Inspection reports are submitted to the plant manager for review and appropriate corrective actions are supplied in form of work order if required.

Annual Inspections

Annual inspections are conducted by the Missouri Department of Natural Resources. The 2009 inspection report was submitted June 16, 2009 (See Appendix A – Doc. 13).

Special Inspections

No special inspections have been conducted at the Sibley fly ash pond.

9.2 INSTRUMENTATION MONITORING

The Sibley Generating Station fly ash impoundment dikes do not have an instrumentation monitoring system.

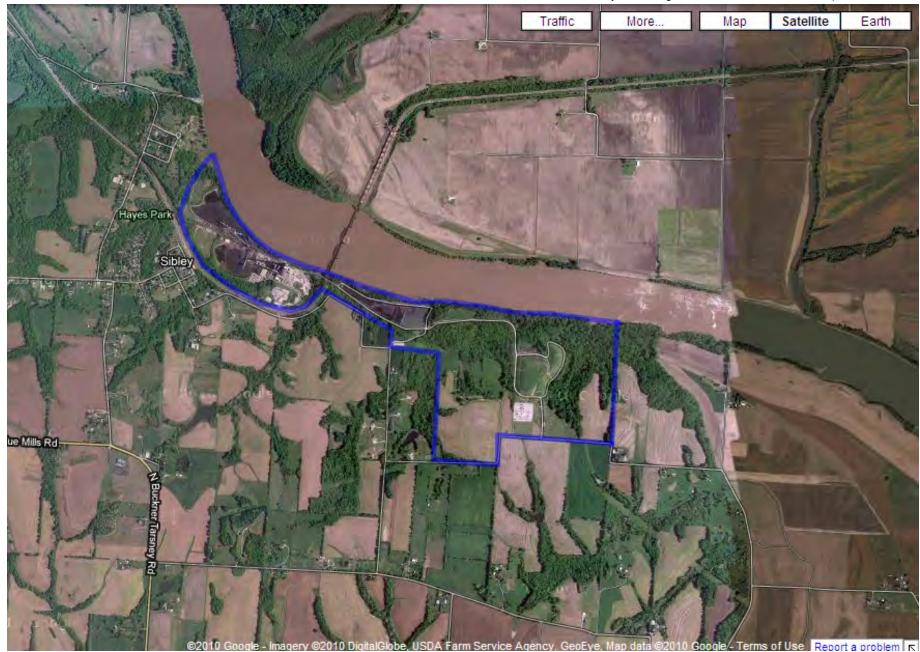
9.3 ASSESSMENT OF SURVEILLANCE AND MONITORING PROGRAM

9.3.1 Adequacy of Inspection Program

Based on the data reviewed by Dewberry, including observations during the site visit, the inspection program is adequate, but should be documented.

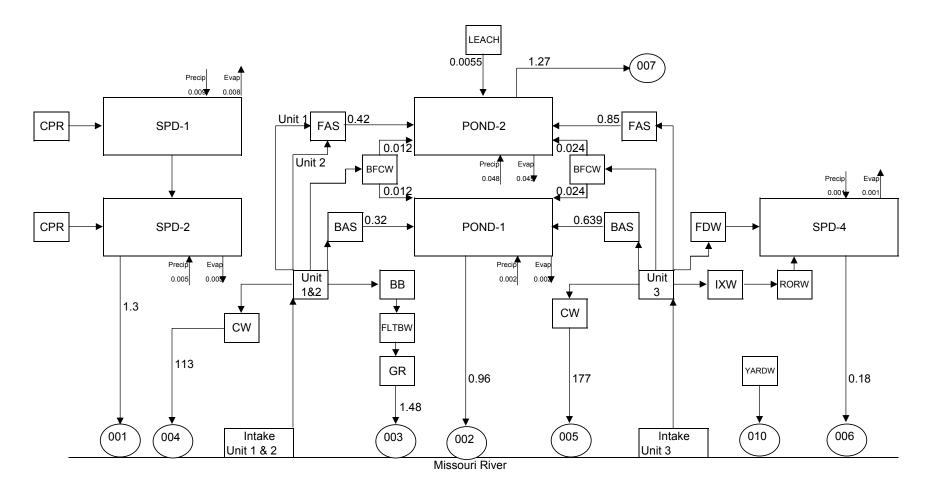
9.3.2 Adequacy of Instrumentation Monitoring Program

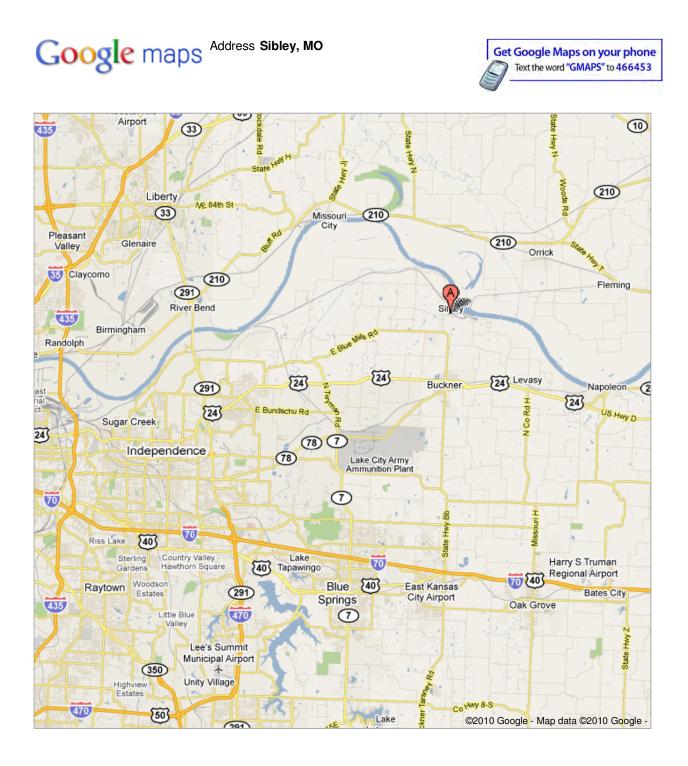
The Sibley fly ash dikes are not instrumented. Based on the size of the dikes, the portion of the impoundment currently used to store wet fly ash and stormwater, the history of satisfactory performance and the current inspection program, installation of a dike monitoring system is not needed at this time.



All flows are in MGD

Plant Name: Sibley Generating Station Plant ID: 06984 WB-1





OMB Control Number: 2040-0281 Approval Expires: 05/31/2013



Steam Electric Questionnaire

PART D - POND/IMPOUNDMENT SYSTEMS AND OTHER WASTEWATER TREATMENT OPERATIONS

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Plant ID: 6984 Plant Name: Sibley Generating St

PART D. POND/IMPOUNDMENT SYSTEMS AND OTHER WASTEWATER TREATMENT OPERATIONS

INSTRUCTIONS

Part D requests information about all ponds/impoundments used (or planned to be used or under construction/installation by December 31, 2020) for the storage, treatment, and/or disposal of process wastewater, residues, or by-products (or sludges or water streams containing the residues or by-products) from the combustion of <u>coal</u>, <u>petroleum</u> <u>coke</u>, or <u>oil</u>, including but not limited to fly ash, bottom ash, boiler slag, or flue gas emission control residues. Additionally, Part D requests information about wastewater treatment systems, other than pond/impoundment systems, for the treatment of wastewaters from ash handling or FGD operations that are located at the plant or are planned to be located at the plant. Complete Part D if you operate one or more systems, or if you are currently constructing/installing, or planning to construct/install one or more systems by December 31, 2020.

Refer to the following definitions throughout Part D.

A "**pond/impoundment**" is defined as a natural topographic depression, man-made excavation, or diked area formed from earthen materials or man-made materials or a combination of them, which is designed to hold an accumulation of liquid process wastes or process wastes containing free liquids, and which is not an injection well. Examples of ponds/impoundments include holding, storage, settling, and aeration pits, ponds, and lagoons. It does not include building sumps and outdoor collection/transfer concrete basins.

A "*pond/impoundment system*" is defined as a system consisting of one or more ponds/impoundments.

A "*wastewater treatment unit*" is defined as a unit operation used to remove pollutants from process wastewater. Wastewater treatment units include, but are not limited to: ponds/impoundments, chemical precipitation, pH adjustment, clarification, biological reactor, thickeners, filters, and constructed wetlands.

A "*wastewater treatment system*" is defined as a combination of one or more "wastewater treatment units", other than ponds/impoundments, designed to achieve wastewater treatment.

NOTE: If a pond/impoundment unit (as defined in Section 4.1) is part of a broader "wastewater treatment system" containing non-pond units (e.g., a pond/impoundment unit in a biological wastewater treatment system), it is not considered part of a pond/impoundment system. Throughout Part D, information is requested for pond/impoundment and wastewater treatment units and systems that are under construction/installation, or planned to be under construction/installation by December 31, 2020. Provide design information, or best engineering estimates as necessary, for these planned systems/units. Additionally, indicate "NA" if the information requested is not applicable for planned systems/units (e.g., a question that requests flow rate data for year 2009).

As you are completing the electronic form, note the following: When you enter your plant name and plant ID on the Part D Table of Contents tab, all name and ID fields throughout Part D will automatically populate. Refer to the overall questionnaire instructions, the glossary, and the acronym list for assistance with completing Part D.

Please provide all free response answers in the highlighted yellow areas. Throughout Part D, you may need to make copies of certain sections/questions. Instructions are provided throughout Part D regarding making copies. Note that pond/impoundment system (and unit) and wastewater treatment system ID's must be populated on the copied tab or section, located in the upper right corner under "Plant ID" and "Plant Name", in order to correlate the requested information with the pond/impoundment or wastewater treatment system.

Use the Part D Comments tab to do the following: provide additional information as requested in certain questions within Part D; indicate atypical data (e.g., if 2009 information is not representative of normal operations); and note methods used to make best engineering estimates in the event that exact data are not available.

Steam Electric Questionnaire

			Plant ID: 698 Plant Name: Sibley Generatin
Γ	Part: Section Title:		/Impoundment System and Wastewater Treatment System Identification
	Instructions	(or begir	te Section 2 (Questions D2-1 through D2-7) for <i>pond/impoundment systems</i> and/or <i>wastewater treatment systems</i> that the plant operates and/or plans to opera n construction/installation of) by December 31, 2020, including those located on non-adjoining property, for the treatment of <i>process wastewaters</i> from ash g or FGD operations. Please provide all free response answers in the highlighted yellow areas.
CBI? Ves	D2-1.	. Has the	plant been involved with any ash or FGD wastewater treatment studies (pilot- or full-scale), including studies on pond/impoundment systems, since 2000?
		O Yes	(Continue)
		• No	(Skip to Question D2-4)
CBI? Ves	D2-2.	Are any	of these studies ongoing?
		O Yes	
		No No	
CBI?	D2-3.	Was a s	ummary and/or report describing/documenting the pilot- or full-scale study prepared (including internal and published reports)?
		O Yes	(Provide a copy of the summary/report)
		No No	(Continue)
			a description of the pilot- or full-scale study. Note the types of treatment technologies studied and the analytes measured in influent to and/or effluents from the ater treatment system.

CBI? D2-4. List any ash or FGD wastewater treatment technologies that have been studied by the plant that are not covered by Questions D2-1 through D2-3 (e.g., those that have been studied in bench-scale studies).

None

D2-5. Do you operate OR plan to operate (or begin construction/installation of) by December 31, 2020 any systems, including those located on non-adjoining property, for the treatment of process wastewaters from ash handling or FGD operations?

O Yes (Continue)
 ○ No (Skip to Section 4.1)

D2-6. Do you operate OR plan to operate (or begin construction/installation of) by December 31, 2020 any <u>pond/impoundment systems</u>, including those located on nonadjoining property, for the treatment of process wastewaters from ash handling or FGD operations?

O Yes (Continue)

O No (Skip to Question D2-7)

List these pond/impoundment systems in Table D-1. For each pond/impoundment system, EPA assigned a number (e.g., POND-1, POND-2) in Table D-1, which will be used throughout the remainder of the survey. In the "Plant Designation" column, provide the plant's name for each pond/impoundment system. In the "Individual Ponds/Impoundments Included in the Pond System" column, identify all pond/impoundment units from Table A-4 that are included in the pond system.

NOTE: Do NOT include a pond/impoundment unit in Table D-1 if the pond/impoundment unit is or is planned to be part of a broader wastewater treatment system containing *non-pond wastewater treatment units* (e.g., pond/impoundment unit in a biological wastewater treatment system).

DOCUMENT

EPA ARCHIVE

CBI?

CBI?

Pond/ Impoundment System ID	Year Initially Brought Online	Plant Designation			Pond	•	itified in Tal ment Syster	•	cluded in the
	ſ	Active/Inactive/Open							
POND-1	1986	Slag Settling Pond	SPD - 1	SPD - 3		SPD - 7	SPD - 9	SPD - 11	SPD - 13
POND-2	1979	Ely Ach Dond	SPD - 1	SPD - 3	SPD - 5	SPD - 7	SPD - 9	SPD - 11	SPD - 13
		Fly Ash Pond	SPD - 2	SPD - 4		SPD - 8	SPD - 10	SPD - 12	SPD - 14
POND-3			SPD - 2	SPD - 4	SPD - 6	SPD - 8	SPD - 10	SPD - 12	SPD - 14
POND-4			SPD - 1	SPD - 3		SPD - 7	SPD - 9	SPD - 11	SPD - 13
POND-5			SPD - 2	SPD - 4		SPD - 7	SPD - 9	SPD - 12	SPD - 13
			SPD - 2	SPD - 4		SPD - 8	SPD - 10	SPD - 12	SPD - 14
POND-6			SPD - 1	SPD - 3	_	SPD - 7	SPD - 9	SPD - 11	SPD - 13
POND-7			SPD - 1	SPD - 3		SPD - 7	SPD - 9	SPD - 11	SPD - 13
			SPD - 2	SPD - 4		SPD - 8	SPD - 10	SPD - 12	SPD - 14
POND-8			SPD - 2	SPD - 4		SPD - 8	SPD - 10	SPD - 12	
POND-9			SPD - 1	SPD - 3	_	SPD - 7	SPD - 9	SPD - 11	SPD - 13
			SPD - 2	SPD - 4		SPD - 8	SPD - 10	SPD - 12	SPD - 14
POND-10			SPD - 2	SPD - 4	SPD - 6	SPD - 8	SPD - 10	SPD - 12	SPD - 14

Table D-1. Plant Pond/Impoundment Systems

		Retired/Clo	osed Pond/Impoundment Systems
RET-POND-1	4000		RET SPD - 1 RET SPD - 3
	<u>1988</u>	Sedimentation Pond	RET SPD - 2 RET SPD - 4
RET-POND-2			RET SPD - 1 RET SPD - 3
RET-FOND-2			RET SPD - 2 RET SPD - 4
DET DOND A			RET SPD - 1 RET SPD - 3
RET-POND-3			RET SPD - 2 RET SPD - 4
			RET SPD - 1 RET SPD - 3
RET-POND-4			RET SPD - 2 RET SPD - 4
			RET SPD - 1 RET SPD - 3
RET-POND-5			🔲 RET SPD - 2 🛛 🗌 RET SPD - 4
		Plannec	d Pond/Impoundment Systems
POND-A			SPD - A SPD - C SPD - E
FOND-A	2010	Leachate Pond	SPD - B SPD - D
			SPD - A SPD - C SPD - E
POND-B			SPD - B SPD - D
			SPD - A SPD - C SPD - E
POND-C			SPD - B SPD - D

D2-7. Do you operate OR plan to operate (or begin construction/installation of) by December 31, 2020 any wastewater treatment systems, including those located on nonadjoining property, other than pond/impoundment systems for the treatment of process wastewaters from ash handling or FGD operations?

O Yes (Continue)

O No (Skip to Section 3.1)

List these wastewater treatment systems in Table D-2. For each wastewater treatment system, EPA assigned a number (e.g., WWT-1, WWT-2) in Table D-2, which will be used throughout the remainder of the survey. In the "Plant Designation" column, provide the plant's name for each wastewater treatment system. As an example, if a plant operates a *chemical precipitation* FGD wastewater treatment system that discharges to an ash pond/impoundment system (as shown in EPA example diagrams EPA_D-1 and EPA_D-2 located at the bottom of Part D Section 3.1) the FGD wastewater treatment system should be identified in Table D-2 (e.g., as WWT-1) and the ash pond/impoundment system should have been previously identified in Table D-1 (e.g., as POND-1).

Note that "Approximate Length of Piping from FGD Scrubber System" refers to the length of piping from the FGD solids separation overflow storage tank (or FGD scrubber absorber if no FGD solids separation) to the beginning of the FGD wastewater treatment system. "Approximate Length of Piping to Subsequent Treatment or Discharge" refers to the length of piping from the end of the FGD wastewater treatment system to either the beginning of the subsequent treatment system or the wastewater discharge point, as appropriate.

CBI?

Yes

Table D-2. Plant Wastewater Treatment Systems

				FGD Wastewater Treatment	
Wastewater Treatment System ID	Plant Designation	Treatment System Footprint (ft ²)	Year Initially Brought On Line	Approximate Length of Piping from FGD Scrubber System (ft)	Approximate Length of Piping to Subsequent Treatment or Discharge (ft)
	200.9.1.101	Operating Wastewater Tree		()	
WWT-1					
WWT-2					
WWT-3					
WWT-4					
WWT-5					
WWT-6					
		Planned Wastewater Trea	tment Systems		
WWT-A					
WWT-B					
WWT-C					

Plant ID: <u>6984</u> Plant Name: <u>Sibley Generating</u> Pond/Impoundment Unit ID: <u>SPD-3</u>

Part: D

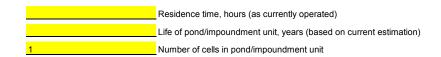
Section Title: 4.1. Active/Inactive/Open and Planned Pond/Impoundment Unit Information

Instructions: Complete Section 4.1 (Questions D4-1 through D4-12) for each active/inactive/open *pond/impoundment* unit used OR planned to be used (or constructed/installed), including those located on non-adjoining property, by December 31, 2020 for the storage, treatment, and/or disposal of process wastewater, *residues*, or by-products (or *sludges* or water streams containing the residues or by-products) from the combustion of coal, petroleum coke, or oil, including but not limited to fly ash, bottom ash, boiler slag, or flue gas emission control residues. Use the pond/impoundment unit IDs assigned in Table A-4.

Make a copy of Section 4.1 for each active/inactive/open and planned pond/impoundment units used (or planned to be used) for the storage, treatment, and/or disposal of process wastewater, residues, or by-products (or sludges or water streams containing the residues or by-products) from the combustion of coal, petroleum coke, or oil, including but not limited to fly ash, bottom ash, boiler slag, or flue gas emission control residues using the "Copy Section 4.1" button below.

NOTE: If a pond/impoundment unit is part of a broader wastewater treatment system containing non-pond wastewater treatment units (e.g., a pond/impoundment unit in a biological wastewater treatment system), complete questions in this section for the pond/impoundment unit.

D4-2. Provide the residence time of the process wastewater in the pond/impoundment unit, the life of the pond/impoundment unit (based on the current estimation), and the number of cells in the pond/impoundment unit.



CBI?

CBI?

D4-3. Complete Table D-5. Provide the pond/impoundment unit's volume, surface area, bottom and top elevation, freeboard height, maximum height of berms and dams above the surrounding grade, and the total quantity of solids placed in the pond/impoundment when it was originally built or planned/designed, at its current status, and at its expected end of life. Additionally, provide the expected year of closure/retirement in the "Expected End of Life" column. Volume should reflect the free water volume, including the stored solids. For planned pond/impoundment units, enter "NA" in all fields in the "Current" column. Figure D-1 presents an illustration of pond/impoundment dimensions.

Note: Respondents are not required to take new measurements to provide this data; however, best available information should be used to complete Table D-5.

Below Grade

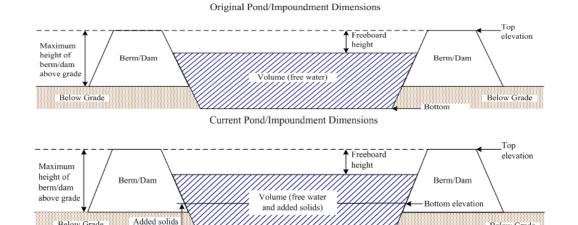


Figure D-1. Pond/Impoundment Dimensions

Table D-5. Active/Inactive/Open and Planned Pond/Impoundment Information

	Originally Built or Planned/Designed	Current	Expected End of Life
Volume, ft ³	102000	102000	102000
Surface area, ft ²	27000	27000	27000
Bottom elevation, ft	713	713	713
Top elevation, ft	724	724	724
Freeboard height, ft	5	5	5
Maximum height of berms/dams above grade, ft	0	0	0
Total solids placed in the pond/impoundment, tons			
Expected year of closure/retirement			

Below Grade

D4-4. Does the pond/impoundment unit have a liner?

- Yes
 (Complete Table D-6)
- O No (Skip to Question D4-5)
- O NA (Pond/Impoundment is planned to be constructed. Information is currently unavailable. Skip to Question D4-10).

Table D-6. Pond/Impoundment Unit Liner

Liner Layer Number (number from inner to outer layer)	Type of Liner	Thickness of Liner Layer (cm)	Permeability of Liner Layer (cm/sec)
	O Compacted clay		
	O Geosynthetic clay		
	O High density polyethylene (HDPE)		
1	Other (provide below:)	15.4	
	Roller Compacted concrete		
	O Compacted clay		
	O Geosynthetic clay		
	O High density polyethylene (HDPE)		
	O Other (provide below:)		
	O Compacted clay		
	O Geosynthetic clay		
	O High density polyethylene (HDPE)		
	O Other (provide below:)		
	O Compacted clay		
	O Geosynthetic clay		
	O High density polyethylene (HDPE)		
	O Other (provide below:)		

D4-5. Has the pond/impoundment unit ever been dredged?

Yes (Provide following information)

2009	Year of last dredging
365	Frequency of dredging that year, dpy
64154	Amount of material removed that year, tons
1825	Number of times dredged in the last five years
1825	Number of days dredged in the last five years
269980	Amount of material removed in the last five years, tons

O No (Skip to Question D4-7)

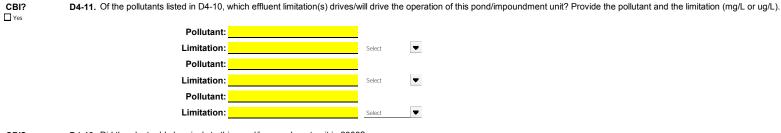
O_{NA} (Pond/Impoundment is planned to be constructed. Skip to Question D4-10)

Steam Electric Questionnaire

CBI?

CBI?	D4-6. Indicate	D4-6. Indicate where the dredged solids are transferred or are planned to be transferred.						
	O Dredged	I solids used in embankment const	truction.					
		i solids transferred to landfill.						
	O Dredgeo							
	• Other (f	xplain):	marketed or landfilled					
CBI?	D4-7. Has the	pond/impoundment ur	nit been expanded since the date it was built?					
	O Yes	(Continue)						
	• No	(Skip to Question	ו D4-10)					
	O NA	(Pond/Impoundm	nent is planned to be constructed. Skip to Question D4-10)					
CBI?	D4-8. Identify	the type of expansion.						
	O Lateral	expansion						
	O Vertica	l expansion						
	O Both Ia	iteral and vertical expansion						
CBI? Yes	D4-9. Describ	e any expansion(s), sin	nce January 1, 2000, to the pond/impoundment unit, including the starting and ending dimensions.					
			ed with the expansion(s). Total costs should include labor, materials, energy, hazardous and nonhazardous waste disposal, purchased equipment, installation, buildings, site preparation, ruction expenses, and any other costs available.					
			\$Total cost of expansion					
CBI?	D4-10. Indicate	the pollutants targeted	d for removal by this pond/impoundment unit using techniques other than solely settling (e.g., adding chemicals to remove certain metals). [Check all boxes that apply.]					
	Metals (specify):						
	TSS							
		n compounds (ammonia, nitrate, n	nitrite)					
	Organic							
	Chlorine	or other oxidizing agents						
	Oil and	grease						
	Other:							
	□ NA		(Skip to Question D4-12)					

Steam Electric Questionnaire



D4-12. Did the plant add chemicals to this pond/impoundment unit in 2009?

O Yes (Complete Table D-7)

No (Skip to Section 4.2)

O NA (Pond/impoundment is planned to be constructed. Provide information in Table D-7 to the extent possible based on plans.)

Note that "Chemical Type" refers to the generic name of the chemical added to the pond/impoundment (e.g., lime, sodium hydroxide, alum, polymer). "Average Dose Concentration" refers to the average concentration of the chemical within the pond/impoundment unit just after it is added to the unit. In the "Location of Chemical Addition" column, indicate where within or near the pond/impoundment the chemical is added (e.g., within the pond/impoundment near the process wastewater influent point, within the pond/impoundment near the effluent, in the effluent/discharge canal). If chemical addition is known only on a yearly basis, divide the yearly value by the approximate number of days the plant added chemicals (which should be the same estimate for the "Frequency of Addition" column).

Table D-7. Chemicals Used in Pond/Impoundment Unit Operations

Chemical Type	Trade Name	Manufacturer	Purpose	Location of Chemical Addition	Average Dose Concentration (g/L)	Average Addition Ra Ib/day)	te (gpd or	Frequency of Addition (dpy)
						O gpd O lb/day	O Solid O Liquid	
						O gpd O lb/day	O Solid O Liquid	
						O gpd O lb/day	O Solid O Liquid	
						O gpd O lb/day	O Solid O Liquid	
						O gpd O lb/day	O Solid O Liquid	

Plant ID: <u>6984</u> Plant Name: <u>Sibley Generating</u> Pond/Impoundment Unit ID: <u>SPD-5</u>

Part: D

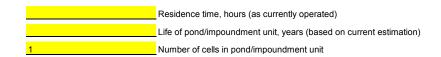
Section Title: 4.1. Active/Inactive/Open and Planned Pond/Impoundment Unit Information

Instructions: Complete Section 4.1 (Questions D4-1 through D4-12) for each active/inactive/open *pond/impoundment* unit used OR planned to be used (or constructed/installed), including those located on non-adjoining property, by December 31, 2020 for the storage, treatment, and/or disposal of process wastewater, *residues*, or by-products (or *sludges* or water streams containing the residues or by-products) from the combustion of coal, petroleum coke, or oil, including but not limited to fly ash, bottom ash, boiler slag, or flue gas emission control residues. Use the pond/impoundment unit IDs assigned in Table A-4.

Make a copy of Section 4.1 for each active/inactive/open and planned pond/impoundment units used (or planned to be used) for the storage, treatment, and/or disposal of process wastewater, residues, or by-products (or sludges or water streams containing the residues or by-products) from the combustion of coal, petroleum coke, or oil, including but not limited to fly ash, bottom ash, boiler slag, or flue gas emission control residues using the "Copy Section 4.1" button below.

NOTE: If a pond/impoundment unit is part of a broader wastewater treatment system containing non-pond wastewater treatment units (e.g., a pond/impoundment unit in a biological wastewater treatment system), complete questions in this section for the pond/impoundment unit.

D4-2. Provide the residence time of the process wastewater in the pond/impoundment unit, the life of the pond/impoundment unit (based on the current estimation), and the number of cells in the pond/impoundment unit.



CBI?

CBI?

D4-3. Complete Table D-5. Provide the pond/impoundment unit's volume, surface area, bottom and top elevation, freeboard height, maximum height of berms and dams above the surrounding grade, and the total quantity of solids placed in the pond/impoundment when it was originally built or planned/designed, at its current status, and at its expected end of life. Additionally, provide the expected year of closure/retirement in the "Expected End of Life" column. Volume should reflect the free water volume, including the stored solids. For planned pond/impoundment units, enter "NA" in all fields in the "Current" column. Figure D-1 presents an illustration of pond/impoundment dimensions.

Note: Respondents are not required to take new measurements to provide this data; however, best available information should be used to complete Table D-5.

Below Grade

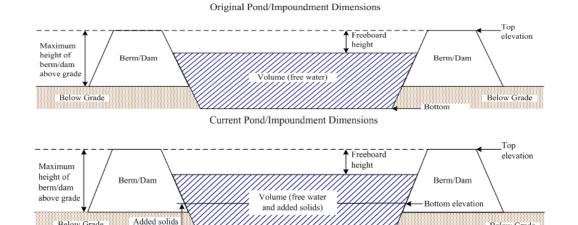


Figure D-1. Pond/Impoundment Dimensions

Table D-5. Active/Inactive/Open and Planned Pond/Impoundment Information

	Originally Built or Planned/Designed	Current	Expected End of Life
Volume, ft ³	10260000	9747000	9747000
Surface area, ft ²	687789	653400	653400
Bottom elevation, ft	703	703	703
Top elevation, ft	725	725	725
Freeboard height, ft	3	3	3
Maximum height of berms/dams above grade, ft	18	18	18
Total solids placed in the pond/impoundment, tons			
Expected year of closure/retirement			

Below Grade

D4-4. Does the pond/impoundment unit have a liner?

- Yes
 (Complete Table D-6)
- O No (Skip to Question D4-5)
- O NA (Pond/Impoundment is planned to be constructed. Information is currently unavailable. Skip to Question D4-10).

Table D-6. Pond/Impoundment Unit Liner

Type of Liner	Thickness of Liner Layer (cm)	Permeability of Liner Layer (cm/sec)
Compacted clay		
O High density polyethylene (HDPE)		
O Other (provide below:)	61.5	
O Compacted clay		
O Geosynthetic clay		
O High density polyethylene (HDPE)		
O Other (provide below:)		
O Compacted clay		
O Geosynthetic clay		
O High density polyethylene (HDPE)		
O Other (provide below:)		
O Compacted clay		
O Geosynthetic clay		
O High density polyethylene (HDPE)		
O Other (provide below:)		
	Compacted clay Geosynthetic clay High density polyethylene (HDPE) Other (provide below:) Geosynthetic clay High density polyethylene (HDPE) Other (provide below:) Other (provide below:)	Type of Liner Layer (cm) © Compacted clay © Geosynthetic clay © Other (provide below:) © Compacted clay © Other (provide below:) © Compacted clay © Compacted clay © Compacted clay © Compacted clay © Other (provide below:) © Other (provide below:) © Compacted clay © Compacted clay

D4-5. Has the pond/impoundment unit ever been dredged?

Yes (Provide following information)

2007	Year of last dredging
1	Frequency of dredging that year, dpy
110000	Amount of material removed that year, tons
1	_Number of times dredged in the last five years
120	Number of days dredged in the last five years
110000	Amount of material removed in the last five years, tons

O No (Skip to Question D4-7)

O_{NA} (Pond/Impoundment is planned to be constructed. Skip to Question D4-10)

Steam Electric Questionnaire

CBI?

DOCUMENT

ARCHIVE

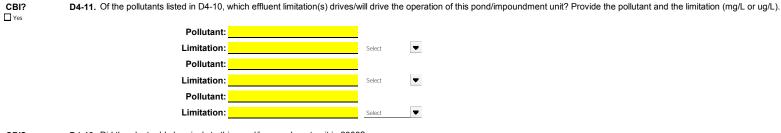
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CBI?	D4-6. Indicate where the dredged solids are transferred or are planned to be transferred.
	O Dredged solids used in embankment construction.
	Dredged solids transferred to landfill.
	O Dredged solids marketed/sold for reuse.
	O Other (Explain):
CBI?	D4-7. Has the pond/impoundment unit been expanded since the date it was built?
	O Yes (Continue)
	O NA (Pond/Impoundment is planned to be constructed. Skip to Question D4-10)
CBI? □ Yes	D4-8. Identify the type of expansion.
	O Lateral expansion
	O Vertical expansion
	O Both lateral and vertical expansion
CBI?	D4-9. Describe any expansion(s), since January 1, 2000, to the pond/impoundment unit, including the starting and ending dimensions.
	Provide the total cost associated with the expansion(s). Total costs should include labor, materials, energy, hazardous and nonhazardous waste disposal, purchased equipment, installation, buildings, site preparation, land, engineering costs, construction expenses, and any other costs available.
	\$Total cost of expansion
CBI?	D4-10. Indicate the pollutants targeted for removal by this pond/impoundment unit using techniques other than solely settling (e.g., adding chemicals to remove certain metals). [Check all boxes that apply.]
	Metals (specify):
	□ Nitrogen compounds (ammonia, nitrate, nitrite) □ Organic Acids
	□ NA (Skip to Question D4-12)

Approved: May 20, 2010

Steam Electric Questionnaire



D4-12. Did the plant add chemicals to this pond/impoundment unit in 2009?

Yes
 (Complete Table D-7)

O No (Skip to Section 4.2)

O NA (Pond/impoundment is planned to be constructed. Provide information in Table D-7 to the extent possible based on plans.)

Note that "Chemical Type" refers to the generic name of the chemical added to the pond/impoundment (e.g., lime, sodium hydroxide, alum, polymer). "Average Dose Concentration" refers to the average concentration of the chemical within the pond/impoundment unit just after it is added to the unit. In the "Location of Chemical Addition" column, indicate where within or near the pond/impoundment the chemical is added (e.g., within the pond/impoundment near the process wastewater influent point, within the pond/impoundment near the effluent, in the effluent/discharge canal). If chemical addition is known only on a yearly basis, divide the yearly value by the approximate number of days the plant added chemicals (which should be the same estimate for the "Frequency of Addition" column).

Table D-7. Chemicals Used in Pond/Impoundment Unit Operations

Chemical Type	Trade Name	Manufacturer	Purpose	Location of Chemical Addition	Average Dose Concentration (g/L)	Average Ad	dition Rate	e (gpd or	Frequency of Addition (dpy)
<mark>CO2</mark>	Compressed CO2	NA	pH control	Within the pond		300	O gpd Ib/day	O Solid Liquid	365
							O gpd O lb/day	O Solid O Liquid	
							O gpd O lb/day	O Solid O Liquid	
							O gpd O lb/day	O Solid O Liquid	
							O gpd O lb/day	O Solid O Liquid	

Plant ID: 6984 Plant Name: Sibley Generating Statio

Part: D Section Title: Part D Comments

Instructions: Cross reference your comments by question number and indicate the confidential status of your comment by checking the box next to "Yes" under "CBI?" (Confidential Business Information).

	Question Number	Comments
CBI?		For SPD-3 and SPD-5 residence time varies with flow rate and amount of material present in the pond. The expected life of pond is the life of the plant which has not been determined. The expected life of SPD-A is the life of the landfill which is not known.
CBI?	D4-3 copy 2 and	Amount of solids is unknown, the pond will close at the end of the plant life.
CBI?	Table D-7	Dose is unknown.
-	D4-15	Max height of berms/dams above grade is NA
-	D5-13	Was accidently answered. It is meant to be blank.
	D4-5	For SPD-3 the last full year of dredging was 2009. The pond has been dredged daily in 2010.
_	Section 6.1 & 6.2	Capital and operating costs and other information have not been provided for SPD-A because it is still under construction.
	Table D-3 and D- 4, all PONDs	Influent and Effluent flows are estimates
	Table D-5, all PONDs	All values vary.
	D4-5 all PONDs	These values are estimates.
CBI? □Yes		
CBI? Ves		

CBI?	
CBI? Ves	
CBI? Ves	
CBI?	
CBI? Ves	
CBI?	
CBI?	

DOCUMENT

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Process Wastewaters			
For Use in Tables and Questions throughout Parts A, B, C, D, and F.			
Air heater cleaning water	AHCW		
Ash pile runoff	APR		
Boiler blowdown	BB		
Boiler fireside cleaning water	BFCW		
Boiler tube cleaning water	BTCW		
Bottom ash sluice	BAS		
Carbon capture wastewater	CCAPW		
Coal pile runoff	CPR		
Combined ash sluice	CAS		
Combustion turbine cleaning (combustion gas portion of	COMBCW		
turbine) water			
Combustion turbine cleaning (compressor portion of the	COMPRCW		
turbine) water			
Combustion turbine evaporative coolers blowdown	TECB		
Cooling tower blowdown	CTB		
FGD scrubber purge	SCRBP		
FGD slurry blowdown	FGDB		
Filter Backwash	FLTBW		
Floor drain wastewater	FDW		
Flue gas mercury control system wastewater	FGMCW		
Fly ash sluice	FAS		
General runoff	GR		
Gypsum pile runoff	GPR		
Gypsum wash water	GYPWW		
Ion exchange wastewater	IXW		
Landfill runoff - capped landfill	LRC		
Landfill runoff - uncapped landfill	LRUC		
Leachate	LEACH		
Limestone pile runoff	LPR		
Mill reject sluice	MRS		

Treated Wastewaters			
For Use as Effluents from Pond/Impoundment Systems			
and/or Wastewater Treatment Systems in Part D, Table D-4.			
Effluent - 1	EFF-1		
Effluent - 2	EFF-2		
Effluent - 3	EFF-3		
Effluent - 4	EFF-4		
Effluent - 5	EFF-5		
Effluent - 6	EFF-6		
Filter backwash	FItBW		
Sludge	SLDG		
For Use as Influents to Por			
and/or Wastewater Treatment			
AND Recycled Waters Th			
POND-1 Effluent	POND-1-EFF		
POND-2 Effluent	POND-2-EFF		
POND-3 Effluent	POND-3-EFF		
POND-4 Effluent	POND-4-EFF		
POND-5 Effluent	POND-5-EFF		
POND-6 Effluent	POND-6-EFF		
POND-7 Effluent	POND-7-EFF		
POND-8 Effluent	POND-8-EFF		
POND-9 Effluent	POND-9-EFF		
POND-10 Effluent	POND-10-EFF		
POND-A Effluent	POND-A-EFF		
POND-B Effluent	POND-B-EFF		
POND-C Effluent	POND-C-EFF		
WWT-1 Effluent	WWT-1-EFF		
WWT-2 Effluent	WWT-2-EFF		
WWT-3 Effluent	WWT-3-EFF		
WWT-4 Effluent	WWT-4-EFF		
WWT-5 Effluent	WWT-5-EFF		

Process Wastewaters			
For Use in Tables and Questions throughout Parts A, B, C, D, and F.			
Once -through cooling water	CW		
Reverse osmosis reject water	RORW		
SCR catalyst regeneration wastewater	SCRRW		
SCR catalyst washing wastewater	SCRWW		
Soot blowing wash water	SOOTW		
Steam turbine cleaning water	STCW		
Yard drain wastewater	YARDW		

Treated Wastewaters

For Use as Influents to Pond/Impoundment Systems and/or Wastewater Treatment Systems in Part D, Table D-3, AND Recycled Waters Throughout Questionnaire.

WWT-6 Effluent	WWT-6-EFF
WWT-A Effluent	WWT-A-EFF
WWT-B Effluent	WWT-B-EFF
WWT-C Effluent	WWT-C-EFF

Wastewater Treatment Units			
For Use in Tables and Questions Throughout Parts D and F.			
Adsorptive media	ADSORB		
Aerobic Biological Reactor	AERBIO		
Anaerobic Biological Reactor	ANBIO		
Aerobic/Anaerobic Biological Reactor	AER/ANBIO		
Chemical Precipitation Reaction Tank 1 - 1	CP-1-1		
Chemical Precipitation Reaction Tank 1 - 2	CP-1-2		
Chemical Precipitation Reaction Tank 2 - 1	CP-2-1		
Chemical Precipitation Reaction Tank 2 - 2	CP-2-2		
Chemical Precipitation Reaction Tank 3 - 1	CP-3-1		
Chemical Precipitation Reaction Tank 3 - 2	CP-3-2		
Clarification, Primary - 1	CL-P-1		
Clarification, Primary - 2	CL-P-2		
Clarification, Secondary - 1	CL-S-1		
Clarification, Secondary - 2	CL-S-2		
Clarification, Tertiary - 1	CL-T-1		
Clarification, Tertiary - 2	CL-T-2		
Constructed wetland - Cell 1	CWL -1		
Constructed wetland - Cell 2	CWL -2		
Constructed wetland - Cell 3	CWL -3		
Constructed wetland - Cell 4	CWL -4		
Constructed wetland - Cell 5	CWL -5		
Constructed wetland - Cell 6	CWL -6		
Constructed wetland system	CWTS		
Equalization, Primary	EQ-P		
Equalization, Secondary	EQ-S		
Filter, Microfiltration - 1	FLT-M-1		
Filter, Microfiltration - 2	FLT-M-2		

Destinations			
For Use in Tables and Questions Throughout Parts A, C, D,			
and F.			
Burned on site	BURN		
Deep-well injection	DWELL		
Discharge to POTW	POTW		
Discharge to PrOTW	PrOTW		
Discharge to surface water	SW		
Evaporation	EVAP		
Hauled off site for reuse	HAULR - RF		
(removal fee)			
Hauled off site for reuse (given	HAULR - GA		
away)			
Hauled off site for reuse	SOLD		
(marketed and sold)			
Hauled off site for disposal	HAUL		
Mixed with fly ash for disposal	MFA		
On-site landfill (as reported in	LANDF		
Table A-6)			
POND-1	POND-1		
POND-2	POND-2		
POND-3	POND-3		
POND-4	POND-4		
POND-5	POND-5		
POND-6	POND-6		
POND-7	POND-7		
POND-8	POND-8		
POND-9	POND-9		
POND-10	POND-10		
POND-A	POND-A		
POND-B	POND-B		
POND-C	POND-C		
WWT-1	WWT-1		
WWT-2	WWT-2		

Wastewater Treatment Units For Use in Tables and Questions Throughout Parts D and F. Filter, Microfiltration - 3 FLT-M-3 Filter, Microfiltration - 4 FLT-M-4 FLT-S-1 Filter, Sand/Gravity - 1 Filter, Sand/Gravity - 2 FLT-S-2 Filter, Sand/Gravity - 3 FLT-S-3 FLT-S-4 Filter, Sand/Gravity - 4 Filter, Ultrafiltration - 1 FLT-U-1 Filter, Ultrafiltration - 2 FLT-U-2 Filter, Ultrafiltration - 3 FLT-U-3 Filter, Ultrafiltration - 4 FLT-U-4 FP-1 Filter press - 1 Filter press - 2 FP-2 Holding tank HT Ion exchange IX Natural wetlands NW PH-1 pH adjustment - 1 PH-2 pH adjustment - 2 PH-3 pH adjustment - 3 **Reverse osmosis** ROS SPD-1 Pond Unit - 1 SPD-2 Pond Unit - 2 SPD-3 Pond Unit - 3 Pond Unit - 4 SPD-4 SPD-5 Pond Unit - 5 SPD-6 Pond Unit - 6 SPD-7 Pond Unit - 7 SPD-8 Pond Unit - 8 Pond Unit - 9 SPD-9

Destinations			
For Use in Tables and Questions Throughout Parts A, C, D, and F.			
WWT-3	WWT-3		
WWT-4	WWT-4		
WWT-5	WWT-5		
WWT-6	WWT-6		
WWT-A	WWT-A		
WWT-B	WWT-B		
WWT-C	WWT-C		
Reuse as boiler water	RECYC - BW		
Reuse as bottom ash sluice	RECYC - BAS		
Reuse as combined ash sluice	RECYC - CAS		
Reuse as FGD slurry	RECYC - FGDP		
preparation water			
Reuse as FGD absorber	RECYC - FGDAB		
makeup			
Reuse as fly ash sluice	RECYC - FAS		
Reuse as mill reject sluice	RECYC - MRS		
Reuse in cooling towers	RECYC - CW		

Wastewater Treatment Units		
For Use in Tables and Questions Throughout Parts D and F.		
Pond Unit - 10	SPD-10	
Pond Unit - 11	SPD-11	
Pond Unit - 12	SPD-12	
Pond Unit - 13	SPD-13	
Pond Unit - 14	SPD-14	
Settling tank - 1	ST-1	
Settling tank - 2	ST-2	
Settling tank - 3	ST-3	
Settling tank - 4	ST-4	
Settling tank - 5	ST-5	
Thickener - 1	TH-1	
Thickener - 2	TH-2	
Vacuum drum filter - 1	VF-1	
Vacuum drum filter - 2 VF-2		
Vacuum filter belt - 1 VFB-1		
Vacuum filter belt - 2	VFB-2	

Solids Handling For Use as Planned Solids Handling for the FGD Slurry Blowdown in Part B Table B-2.				
Centrifuge - 2	CENT-2			
Centrifuge - 3	CENT-3			
Centrifuge - 4	CENT-4			
Hydrocyclones - 1	HYC-1			
Hydrocyclones - 2	HYC-2			
Hydrocyclones - 3	HYC-3			
Hydrocyclones - 4	HYC-4			
Filter press - 1	FP-1			
Filter press - 2	FP-2			
Thickener - 1	TH-1			
Thickener - 2	TH-2			
Vacuum drum filter - 1	VF-1			
Vacuum drum filter - 2	VF-2			
Vacuum filter belt - 1	VFB-1			
Vacuum filter belt - 2	VFB-2			



Daniel F. Rembold Sibley Generating Station 33200 East Johnson Road Sibley, MO 64088

May 15, 2009

Mr. Richard Kinch US Environmental Protection Agency Two Potomac Yard 2733 S. Crystal Dr. 5th Floor; N-5738 Arlington, VA 22202-2733

Re: Request for Information Under Section 104(e) of the Comprehensive Environmental Response, Compensation, and Liability Act, 42 U.S.C. 9604(e)

Dear Mr. Kinch:

Enclosed is the response of KCP&L Greater Missouri Operations Company (KCP&L GMO) to EPA's Section 104 (e) request for information not dated that was received May 4, 2009 regarding an ash settling pond and slag settling pond at KCP&L GMO's Sibley Generating Station. Both ponds are currently being operated for settling and not disposal. Slag is removed from the slag settling pond and beneficially used off-site. Fly ash is removed from the fly ash settling pond and deposited in an on-site permitted landfill.

I certify that the information contained in this response to EPA's request for information and the accompanying documents is true, accurate, and complete. As to the identified portions of this response for which I cannot personally verify their accuracy, I certify under penalty of law that this response and all attachments were prepared in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fines and imprisonment for knowing violations.

If you have any questions regarding this response, please contact me at 816-650-2900.

Sincerely,

Daniel F. Rembold Plant Manager Sibley Generating Station

Enclosure A

Enclosure A

KCP&L Greater Missouri Operations Company Sibley Generating Station Management Unit: Slag Settling Pond

May 15, 2009

Please provide the information requested below for each surface impoundment or similar diked or bermed management unit(s) or management units designated as landfills which receive liquidborne material for the storage or disposal of residuals or by-products from the combustion of coal, including, but not limited to, fly ash, bottom ash, boiler slag, or flue gas emission control residuals. This includes units that no longer receive coal combustion residues or by-products, but still contain free liquids.

1. Relative to the National Inventory of Dams criteria for High, Significant, Low, or Less-than-Low, please provide the potential hazard rating for each management unit and indicate who established the rating, what the basis of the rating is, and what federal or state agency regulates the unit(s). If the unit(s) does not have a rating, please note that fact.

The Management Unit does not have a known rating. The Missouri Department of Natural Resources - Solid Waste Management Program regulates solid waste facilities in Missouri.

2. What year was each management unit commissioned and expanded?

The Management Unit was commissioned approximately in 1986 and has not been expanded. Slag is removed from the Management Unit and beneficially used off-site.

3. What materials are temporarily or permanently contained in the unit? Use the following categories to respond to this question: (1) fly ash; (2) bottom ash: (3) boiler slag; (4) flue gas emission control residuals; (5) other. If the management unit contains more than one type of material, please identify all that apply. Also, if you identify "other," please specify the other types of materials that are temporarily or permanently contained in the unit(s).

Slag.

L,

4. Was the management unit(s) designed by a Professional Engineer? Is or was the construction of the waste management unit(s) under the supervision of a Professional Engineer? Is inspection and monitoring of the safety of the waste management unit(s) under the supervision of a Professional Engineer?

The Management Unit is in ground without dikes or berms. The Management Unit was designed by a Professional Engineer. The construction drawings for the Management Unit were sealed by a Professional Engineer. Inspection and monitoring of the safety of the Management Unit is not completed under the supervision of a Professional Engineer.

5. When did the company last assess or evaluate the safety (i.e., structural integrity) of the management unit(s)? Briefly describe the credentials of those conducting the structural integrity

assessments/evaluations. Identify actions taken or planned by facility personnel as a result of these assessments or evaluations. If corrective actions were taken, briefly describe the credentials of those performing the corrective actions, whether they were company employees or contractors. If the company plans an assessment or evaluation in the future, when is it expected to occur?

The Management Unit is visually inspected on approximately a weekly basis by operational or security personnel. There has been no known assessment or evaluation of the safety (i.e., structural integrity) of the Management Unit beyond the visual inspection. There have been no known actions taken or planned by facility personnel as a result of the visual inspections of the Management Unit. There are no planned assessments or evaluation of this Management Unit in the future beyond the visual inspections.

6. When did a State or a Federal regulatory official last inspect or evaluate the safety (structural integrity) of the management unit(s)? If you are aware of a planned state or federal inspection or evaluation in the future, when is it expected to occur? Please identify the Federal or State regulatory agency or department which conducted or is planning the inspection or evaluation. Please provide a copy of the most recent official inspection report or evaluation.

There have been no known State or Federal regulatory official inspection or evaluation of the safety (structural integrity) the Management Unit. We are not aware of a planned state or federal inspection or evaluation in the future.

7. Have assessments or evaluations, or inspections conducted by State or Federal regulatory officials conducted within the past year uncovered a safety issue(s) with the management unit(s), and, if so, describe the actions that have been or are being taken to deal with the issue or issues. Please provide any documentation that you have for these actions.

There have been no known assessments or evaluations, or inspections conducted by State or Federal regulatory officials conducted within the past year that uncovered a safety issue(s) with the Management Unit.

8. What is the surface area (acres) and total storage capacity of each of the management units? What is the volume of material currently stored in each of the management unit(s)? Please provide the date that the volume measurement(s) was taken. Please provide the maximum height of the management units(s). The basis for determining the maximum height is explained later in this Enclosure.

The Management Unit's surface area is less than one acre and the total storage capacity is approximately 500 cubic yards. The capacity measurements were made as of 1986. The volume of material currently stored in the Management Unit is estimated today to be approximately 300 cubic yards. The Management Unit is in ground without dikes or berms and therefore has no Dam Height.

9. Please provide a brief history of known spills or unpermitted releases from the unit within the last ten years, whether or not these were reported to State or federal regulatory agencies. For

purposes of this question, please include only releases to surface water or to the land (do not include releases to groundwater).

There have been no known spills or unpermitted releases from the Management Unit within the last ten years.

10. Please identify all current legal owner(s) and operator(s) at the facility.

The current legal owner of the Sibley Generating Station is KCP&L Greater Missouri Operations Company. The current operator of Sibley Generating Station is KCP&L Greater Missouri Operations.

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Enclosure A

KCP&L Greater Missouri Operations Company Sibley Generating Station Management Unit: Fly Ash Settling Pond

May 15, 2009

Please provide the information requested below for each surface impoundment or similar diked or bermed management unit(s) or management units designated as landfills which receive liquidborne material for the storage or disposal of residuals or by-products from the combustion of coal, including, but not limited to, fly ash, bottom ash, boiler slag, or flue gas emission control residuals. This includes units that no longer receive coal combustion residues or by-products, but still contain free liquids.

1. Relative to the National Inventory of Dams criteria for High, Significant, Low, or Less-than-Low, please provide the potential hazard rating for each management unit and indicate who established the rating, what the basis of the rating is, and what federal or state agency regulates the unit(s). If the unit(s) does not have a rating, please note that fact.

The Management Unit does not have a known rating. The Missouri Department of Natural Resources - Solid Waste Management Program regulates solid waste facilities in Missouri.

2. What year was each management unit commissioned and expanded?

The Management Unit was commissioned approximately in 1979 and has not been expanded. Fly ash is periodically removed from the Management Unit and deposited into an on-site permitted landfill.

3. What materials are temporarily or permanently contained in the unit? Use the following categories to respond to this question: (1) fly ash; (2) bottom ash: (3) boiler slag; (4) flue gas emission control residuals; (5) other. If the management unit contains more than one type of material, please identify all that apply. Also, if you identify "other," please specify the other types of materials that are temporarily or permanently contained in the unit(s).

Fly ash.

4. Was the management unit(s) designed by a Professional Engineer? Is or was the construction of the waste management unit(s) under the supervision of a Professional Engineer? Is inspection and monitoring of the safety of the waste management unit(s) under the supervision of a Professional Engineer?

The Management Unit was designed by a Professional Engineer. The construction drawings for the Management Unit were sealed by a Professional Engineer. Inspection and monitoring of the safety of the Management Unit is not completed under the supervision of a Professional Engineer.

5. When did the company last assess or evaluate the safety (i.e., structural integrity) of the

management unit(s)? Briefly describe the credentials of those conducting the structural integrity assessments/evaluations. Identify actions taken or planned by facility personnel as a result of these assessments or evaluations. If corrective actions were taken, briefly describe the credentials of those performing the corrective actions, whether they were company employees or contractors. If the company plans an assessment or evaluation in the future, when is it expected to occur?

The Management Unit is visually inspected on approximately a weekly basis by operational or security personnel. There has been no known assessment or evaluation of the safety (i.e., structural integrity) of the Management Unit beyond the visual inspection. There have been no known actions taken or planned by facility personnel as a result of the visual inspections of the Management Unit. There are no planned assessments or evaluation of this Management Unit in the future beyond the visual inspections.

6. When did a State or a Federal regulatory official last inspect or evaluate the safety (structural integrity) of the management unit(s)? If you are aware of a planned state or federal inspection or evaluation in the future, when is it expected to occur? Please identify the Federal or State regulatory agency or department which conducted or is planning the inspection or evaluation. Please provide a copy of the most recent official inspection report or evaluation.

There have been no known State or Federal regulatory official inspection or evaluation of the safety (structural integrity) the Management Unit. We are not aware of a planned state or federal inspection or evaluation in the future.

7. Have assessments or evaluations, or inspections conducted by State or Federal regulatory officials conducted within the past year uncovered a safety issue(s) with the management unit(s), and, if so, describe the actions that have been or are being taken to deal with the issue or issues. Please provide any documentation that you have for these actions.

There have been no known assessments or evaluations, or inspections conducted by State or Federal regulatory officials conducted within the past year that uncovered a safety issue(s) with the Management Unit.

8. What is the surface area (acres) and total storage capacity of each of the management units? What is the volume of material currently stored in each of the management unit(s)? Please provide the date that the volume measurement(s) was taken. Please provide the maximum height of the management units(s). The basis for determining the maximum height is explained later in this Enclosure.

The Management Unit's surface area is approximately 15 acres and the total storage capacity is approximately 361,000 cubic yards. The volume measurement was taken approximately January 1987. The volume of material currently stored in the Management Unit is estimated today to be approximately 220,000 cubic yards. The Management Unit's Dam Height, pursuant to Enclosure A, is approximately 18 feet.

9. Please provide a brief history of known spills or unpermitted releases from the unit within the

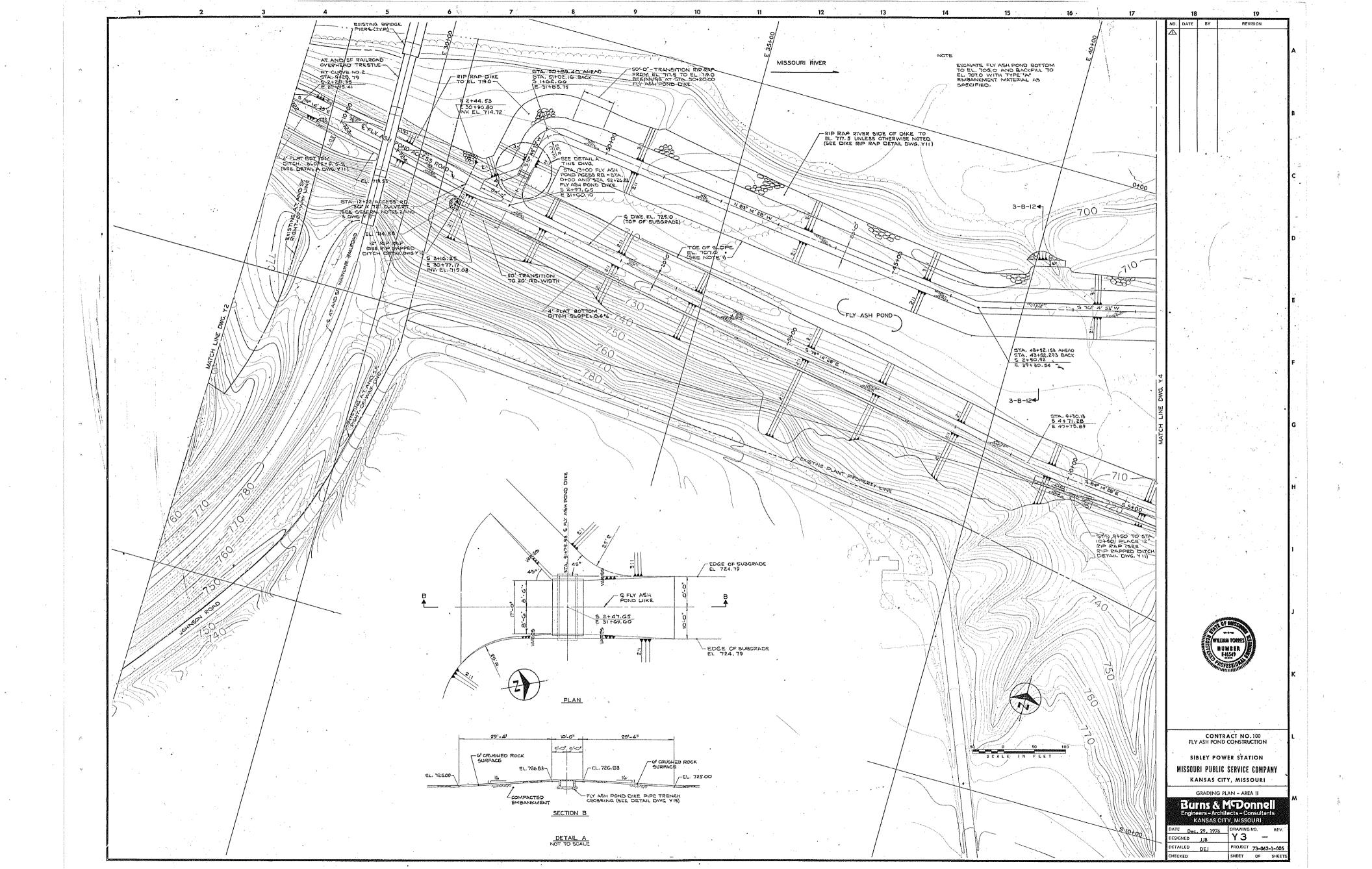
last ten years, whether or not these were reported to State or federal regulatory agencies. For purposes of this question, please include only releases to surface water or to the land (do not include releases to groundwater).

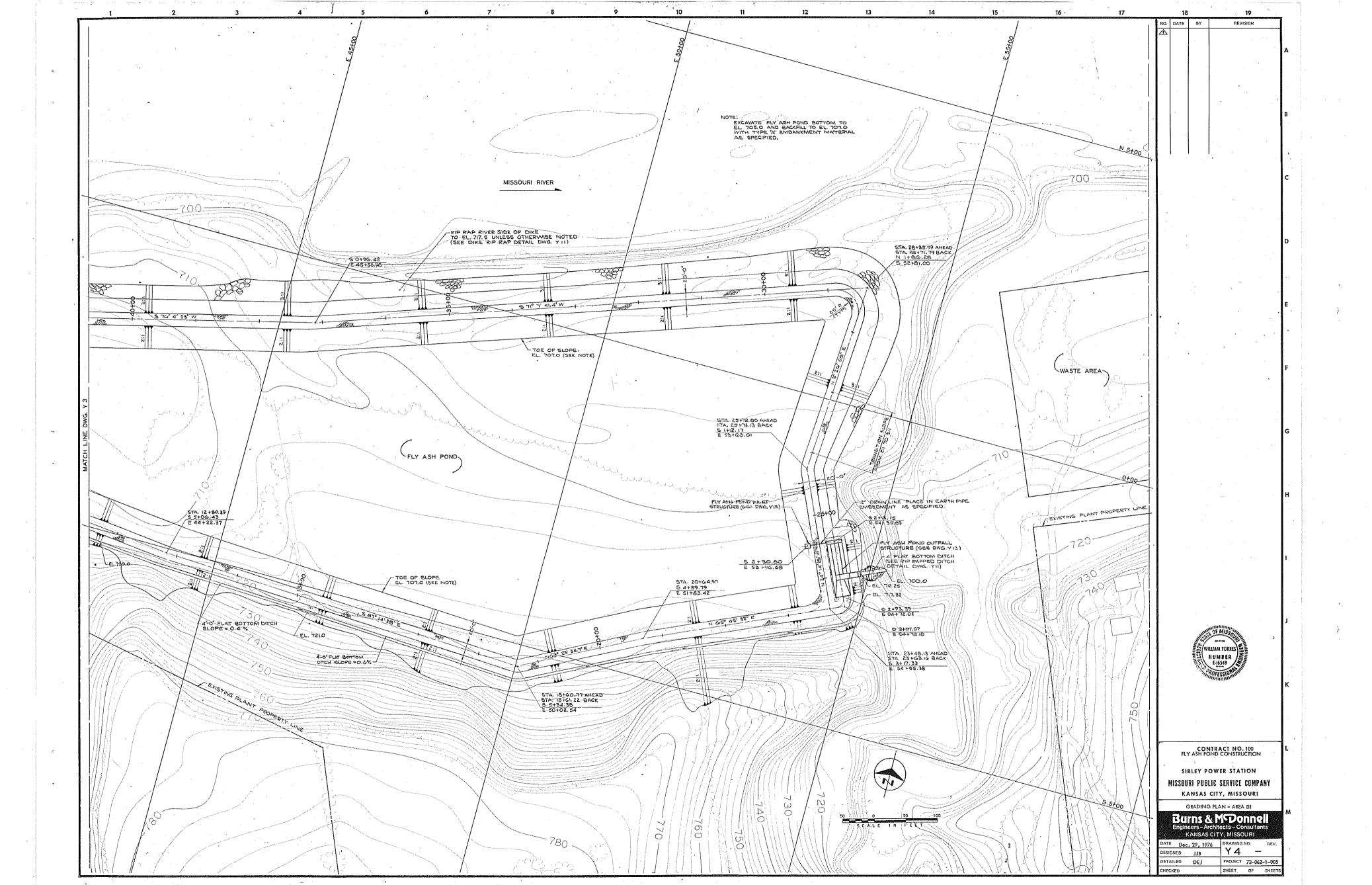
There have been no known spills or unpermitted releases from the Management Unit within the last ten years.

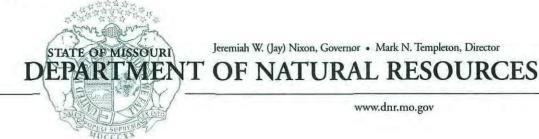
10. Please identify all current legal owner(s) and operator(s) at the facility.

The current legal owner of the Sibley Generating Station is KCP&L Greater Missouri Operations Company. The current operator of Sibley Generating Station is KCP&L Greater Missouri Operations.

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www.dnr.mo.gov

JUN 1 6 2009

Mr. Bob Beck Utilicorp-Sibley Generating Station 33200 East Johnson Road Sibley, MO 64088

Dear Mr. Beck:

On March 5, 2009, Patrick Peltz and Ryan Kivett from the Missouri Department of Natural Resources, Kansas City Regional Office (the department), conducted a routine inspection of Utilicorp-Sibley Generating. Station #2. The purpose of the inspection was to assess compliance with the Missouri Clean Water Law, Missouri Clean Water Commission regulations, and the facility's Missouri State Operating Permit.

The inspector's report is enclosed for your review. The facility was found to be in compliance. If you have any questions or comments regarding this report, please feel free to contact Patrick Peltz at the Kansas City Regional Office, 500 Northeast Colbern Road, Lee's Summit, Road, 64086 at (816) 622-7013 or Richard Sanders at the same address, (816) 622-7000. Thank you.

> 3 Recycled Paper

Sincerely

KANSAS CITY REGIONAL OFFICE

Douathy manhlis

Dorothy E. Franklin **Environmental Manager**

DEF/pkp

Enclosures

Water Pollution Control Program C:

M:\WPC\Clay\Clay County\utilicorp-sibley generating station 080305\0004871_INS.doc

Missouri Department of Natural Resources Kansas City Regional Office/Water Pollution Program Utilicorp-Sibley Generating Station Report of Inspection 33200 E Johnson Road Sibley, MO 64088 MO-0004871

INTRODUCTION

On March 5, 2009, Patrick Peltz and Ryan Kivett of the Missouri Department of Natural Resources Kansas City Regional Office (the department), conducted a routine inspection of Utilicorp-Sibley Generating Station. The purpose of the inspection was to assess compliance with the Missouri Clean Water Law (MCWL), Missouri Clean Water Commission (MCWC) regulations, and the facility's Missouri State Operating Permit (MSOP); and conducted with the authority granted to the department by the Missouri Clean Water Commission [644.026.1 (21) RSMo]. The inspection also served to promote proper operation and to provide technical assistance where necessary. At the time of the inspection the facility was found to be in compliance.

PARTICIPANTS

Missouri Department of Natural Resources, Kansas City Regional Office Patrick Peltz, Environmental Specialist Ryan Kivett, Environmental Specialist

Independence Power and Light Bob Beck, Engineer Steve Brooks, Engineer

FACILITY DESCRIPTION

Utilicorp-Sibley is a Coal Fired Steam Electricity Generating Plant. The back-up energy source is fuel oil. This facility is owned by Utilicorp United, Inc. in Kansas City Missouri. The Standard Industrial Codes for this Utilicorp-Sibley Electrical Generating Plant is 4911.

Utilicorp Sibley has three electrical power generators at the Sibley location. The first generator was placed on line in 1960. In 1962 Utilicorp-Sibley placed the second generator on line. In 1963 generator number three was brought into service.

Utilicorp-Sibley has a total of ten outfalls in its Missouri State Operating Permit. Eight outfalls are being utilized as listed below. Outfalls 008 and 009 have been closed.

- 1. Outfall 001 serves the settling ponds for coal solids from the coal pile runoff/.settling pond.
- 2. Outfall 002 serves the slag settling pond for Generator 1, 2, and 3 slag sluice.
- 3. Outfall 003 serves various sources including boiler number one and number two, boiler blowdown, slag tank overflow, manhole stormwater drains, aerator basin overflow, roof stormwater and slag tank seals.

- 4. Outfall 004 discharges, once-through, non-contact cooling water for boiler number one and number two.
- 5. Outfall 005 discharges, once-through, non-contact cooling water for boiler number three, slag tank overflow.
- 6. Outfall 006 accepts the effluent from multiple sources. The bulk of the effluent comes from the machinery maintenance and plant effluent, carbon filter backwash, chemical cleaning wastes. The effluent is stabilized in a lagoon prior to discharge in a manner to extract the liquid and leave the oil and grease on the lagoon.
- 7. Outfall 007 serves the fly ash pond and the landfill leachate effluent.
- 8. Outfall 008 has been eliminated.
- 9. Outfall 009 has been eliminated.
- 10. Outfall 010 discharges stormwater from the plant area.

On June 13, 1997, Utilicorp-Sibley constructed a 24 inch thick base-pad from 22,000 tons of fly ash. This flexible, six acre fly ash pad is being used to support the coal stockpile. Constructing the fly ash base gave Utilicorp a place to use fly ash as well as create a coal storage base pad that would resist cracking and material leaching.

Utilicorp-Sibley maintains a fly ash landfill. This closed landfill is at capacity, and is not accepting fly ash. The facility has been capped with an impervious layer of clay, stabilized with top soil and heavy grasses. The spillways are profoundly engineered to stabilize erosion created by stormwater runoff from the massive landfill.

Utilicorp Sibley no longer treats its own domestic wastewater but pumps it to the main. Waste disposal for used oil and hazardous wastes are handled by licensed haulers.

COMPLIANCE HISTORY

The DNR issued Missouri State Operating Permit, MO0004588, to Utilicorp-Sibley on November 1, 2002. This permit expired on October 31, 2007. Utilicorp is presently operating on the expired permit while the department is processing the new permit. Clean Water Commission regulations at 10 CSR 20-6.010(5)(C) require that an application for renewal be submitted within 180 days prior to expiration of the permit. Utilicorp-Sibley submitted the application within proper time frames.

In the January 26, 2001, inspection, the department detected an oily ring and sheen on the lagoon berm serving outfall #006. Because the design of the outfall and catch lagoon was to retain oily wastes, the department found outfall #006 to be in compliance. During the March 9, 2009 inspection, the department detected a similar ring around the lagoon and a minute sheen on the lagoon surface of about 3 square feet. The department found outfall #006 to be in compliance. In April 30, 2006 outfall #006 showed a TSS exceedence level of 31 mg/L.

Utilicorp-Sibley is presently engineering a landfill expansion. On April 17, 2009, the department's solid waste management program acknowledged Sibley's request for a construction permit for the expansion.

A review of the facility's Discharge Monitoring Reports (DMR) in the WQIS database was conducted. The monthly Discharge Monitoring Reports are submitted to the Kansas City Regional Office on a Quarterly Basis. Utilicorp's MSOP requires that the Discharge Monitoring Reports be submitted to the department no later than the 28th of each month. The review covered the previous sixty months. The DMRs were analyzed for the permitted parameters and effluent limitations. Each outfall has different monitoring requirements, parameters, final effluent limits, units and frequencies because of the conditions, requirements, and the location of the outfall. These conditions are outlined in the Missouri State Operating Permit. The table below lists the measured values that exceeded the permitted effluent limits.

REPORT PERIOD	PARAMETER	OUTFALL	PERMIT LIMIT	REPORTED VALUE
20050831	TSS	001	30 mg/l	63 mg/l
20070430	TSS	001	30 mg/L	126 mg/L
20060430	TSS	002	30 mg/L	64 mg/L
20070831	SO4	002	30 mg/L	01 mg/L
20070930	TSS	002	30 mg/L	39 mg/L
20071031	WET Violation	002	30 mg/L	55 mg/L/
20080731	TSS	002	30 mg/L	40 mg/L
20050131	WET Violation	003	50 mg/L	10 mg/L
20060131	WET Violation	003		
20060531	TSS	003	30 mg/L	34 mg/L
20060630	WET Violation	003	30 mg/L	mg/L
20070131	WET Violation	003	30 mg/L	mg/L
20080131	TSS	003	30 mg/L	96 mg/L
20070131	WET Violation	004		
20060630	TSS	006	30mg/L	31mg/L
20070131	WET Violation	006		0
20040930	pH	007	6.0-9.0	9.05
20060430	pH	007	6.0-9.0	9.1
20060731	pH	007	6.0-9.0	9.1
20061031	pH	007	6.0-9.0	9.29
20070131	pH	007	6.0-9.0	9.5
20070831	pH	007	6.0-9.0	9.2
20070930	pH	007	6.0-9.0	9.1
20070930	WET Violation	007		
20071130	pH	007	6.0-9.0	9.1
20080131	pH	007	6.0-9.0	9.1
20080430	pH	007	6.0-9.0	9.2
20080531	pH	007	6.0-9.0	9.2
20080630	pH	007	6.0-9.0	9.5
20080831	pH	007	6.0-9.0	9.3
20080930	TSS	007	30 mg/L	62

OBSERVATIONS

Utilicorp-Sibley Generating Plant has 10 Outfalls, all outfalls were inspected.

- 1. Outfall 002 serves the slag settling pond for Generator 1, 2, and 3 slag sluice. At the time of the inspection, the pond had ample storage space available.
- 2. Outfall 007 serves the fly ash pond and the landfill leachate effluent. At the time of the inspection, effluent was not discharging from the landfill. The landfill is in good shape and well maintained. The black fly ash is stored in patterns in the pond. The pond is not stressed but nearing optimal storage capacity Utilicorp-Sibley uses low sulphur coal which creates high pH in this wet storage area. This is a contributing factor for multiple exceedences on the pH parameter.
- Utilicorp-Sibley maintains a closed fly ash landfill. Leachate from the landfill is collected in the fly ash, wet storage pond and discharged through outfall #007.
- 4. Clean, dry fly ash is stored in a silo and sold for commercial purposes.
- 5. The coal stock piles are maintained on top of a fly ash structure. This provides a flexible, crack resistant, protective cap, and a stabile base to store the coal on. It also provides a place to use the fly ash.
- 6. Fly ash is stored in a heavily constructed, uniformly built, wet pond. The storage is approaching capacity. Presently, the fly ash remains at a level that is below berm tops. There is adequate freeboard. There appears to be room for further safe storage. Utilicorp-Sibley annually performs a TCLP on the fly ash stored in the pond. Recently the pH has demonstrated a trend of being over the permitted limit of 9.0. Sibley reports that its engineers are continuing to work towards a solution to the high pH.
- On March 5, 2009 the department inspected the inside of the facility and examined the floor drains, contents, materials and work performed in the shed of each drain. The drains were found to be protected from contaminants.
- 8. Materials and liquids display the supplier's label, showing material type, characteristics, and manufacture contact information in case of a spill. Utilicorp-Sibley utilizes booms and spill prevention practices to protect the floor drains. The power plant has a spill team. It is the practice of Utilicorp to refrain from using drains to catch liquid. All material is recovered as opposed to being disposed of in the drains. The wastes and sludge are handled through a licensed hauler. As a final protection, the drains terminate into a lagoon supporting outfall #006.

UNSATISFACTORY FEATURES

Some of the outfall markers were not acceptable. One was held down to a culvert with rocks.

REQUIRED ACTIONS

Continue to monitor pH levels and progress toward maintaining a pH no higher than 9.0 for outfall 007. Utilicorp-Sibley has attempted to adjust the pH by metering acid into the discharge. Success was limited therefore Utilicorp-Sibley should seek a solution for maintaining the pH limitation within the permitted limit.

Monitor the capacity of fly ash pond. The pond was engineered for a limited amount of fly ash and water. Disallow the structure to become stressed, putting it at risk for a release or failure.

Position and display outfall markers so that they can be seen from both directions and make them permanent.

COMMENTS

Utilicorp-Sibley is a large complicated facility. It maintains a diverse series of outfalls with many environmental exposures and varied parameters. Commonly, the parameter limits are being met.

DMRs for outfall #007 exhibit consistent exceedences with the pH limits since September 2004. The managers expressed that the pH has risen with the switch to low sulfur coal and that the limit of 9.0 is difficult to maintain. They have endeavored to implement new methods to seek solutions. In a Utilicorp-Sibley report, the Missouri River consistently displays a pH of 8.44 in the intake water. The permitted effluent limit is 9.0. Continued attention should be given to lowering the pH and stabilizing outfall #007 effluent limitations.

Overall, Utilicorp-Sibley Power Generating Station is well managed environmentally. The managers have a good knowledge of all issues and management of these issues.

CONCLUSION

The overall operation and appearance of the facility is satisfactory, and the facility was determined to be in compliance with the Missouri Clean Water Law and the Missouri Clean Water Commission Regulations.

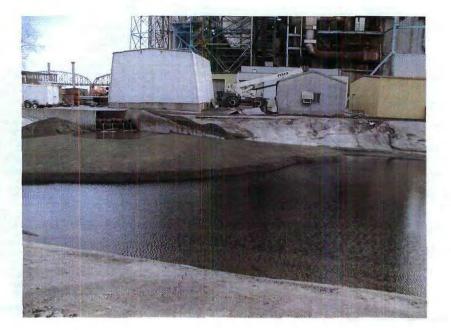
If you have any questions or comments regarding this report, please feel free to contact Patrick Peltz or Richard Sanders at the Kansas City Regional Office, 500 NE Colbern Road, Lee's Summit, MO 64086 or by telephone at (816) 622-7013 or (816) 622-7000. Thank you.

Reported By

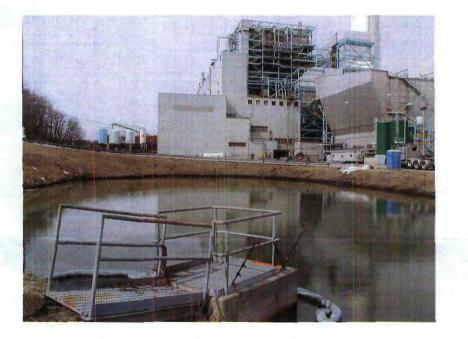
Patrick Peltz Environmental Specialist Water Pollution Program Kansas City Regional Office

Approved By:

Richard W Sanders II Unit Chief Water Pollution Program Kansas City Regional Office



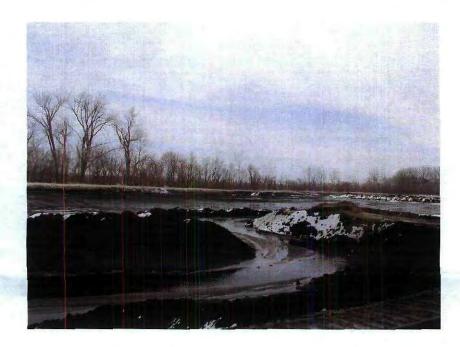
Photograph 001, Ryan Kivett. March 5, 2009. Ash sluice and boiler slag. The Missouri River is protected from products and by-products of the plant operations.



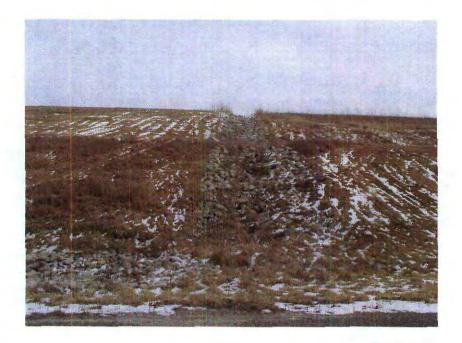
Photograph 002, Ryan Kivett. March 5, 2009. Outfall 006. This pond catches oil and grease from the floor drains in the building and service areas, inside and outside. It serves to settle solids and to trap oil and grease before water is discharged through outfall 006.



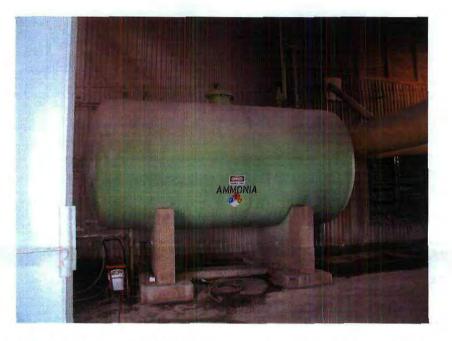
Photograph 003, Ryan Kivett. March 5, 2009. Coal runoff settling pond. Utilicorp monitors its settling ponds and maintains its outfalls.



Photograph 004, Ryan Kivett. March 5, 2009. Fly ash storage pond. The outfall serving the flyash pond has consistently been a challenge for Utilicorp to maintain the pH levels. They have continued to research and implement methods to control levels.



Photograph 005, Ryan Kivett. March 5, 2009. Closed fly ash landfill. Leachate is discharged to the fly ash storage pond. This landfill is well maintained.



Photograph 006, Ryan Kivett. March 5, 2009. Chemicals are stored inside the generating plant. Utilicorp has spill emergency plan with trained personnel. The plant floor drains terminate into the storage lagoon at the outfall 006. Utilicorp is careful to monitor all agents and chemicals stored within the building to keep them from spilling or tracking into the environment. Utilicorp captures all agents before discharging from outfall 006.



Photograph 007, Ryan Kivett. March 5, 2009. This outfall marking designates that this is certainly outfall 002, however it is less than the department requires. Utilicorp's Missouri State Operating Permit does not specifically tell Utilicorp, exactly how to place and make the outfall sign but the method of attempting to adhere tape to a structure obviously may be improved upon. Outfalls must be marked so that they can be seen from both sides in letters that are legible at a distance. The department recommends to elevate the sign at least two feet from the ground and to use letters at least two inches tall. It is a good idea to make certain that signage is fastened more permanently.

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STATE OF MISSOURI

DEPARTMENT OF NATURAL RESOURCES

MUSSOURI CLEAN WATER COMMISSION



MISSOURI STATE OPERATING PERMIT

In compliance with the Missouri Clean Water Law. (Chapter 644 R.S. Mo. as amended, hereinafter, the Law), and the Federal Water Pollation Control Act (Public Law 92-500, 92^{an} Congress) as amended, ...

Faran Bo.	MO-0004871
Qwaer.	Otilicorp United, Inc.
Address	10700 east 350 Highway, Kansas City, MO 64138
Commany Authority:	Same as above
Address:	Same as above
Euclay Name:	Utilicorp - Sibley Station
Faulity Address.	33200 East Johnson Road, Sibley, MO 64088
Legal Description:	SW %, NW %, Sec. 2, T50N, R30W, Jackson County
L'initude/Longitude:	See Page 2
Receiving Stream	Missouri River (P)
First Classified Stream and ID:	Missouri River (P)(00356)
USUS Bann & Sub-watershed No	(10300101-080002)
	cility described herein, in accordance with the effluent limitations and monitoring requirements
as set torth herein:	at the
а цонация бухобы а добя пострују после в	ing Pond - SIC #4911
November 3, 2000	
Provide Date	Stuphen Mendunford, Obrande Repairman of Source Construction Executive Secretary, Clean Wieter Computingen
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Page 2 of 11 Permit No. MO-0004871,

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#002 +3910463/-09411079
#003 +3910475/-09411066
#004 +3910443/-09411020
#005 +3910418/-09411276
#006 +3910400/-09410591
#007 +3910293/-09410211
#008 & #009 eliminated
#010 +3910447/-09411261

FACILITY DESCRIPTION (continued)

<u>Outfall #003</u> - Various Sources - SIC #4911 Units 1 and 2 slag tank overflow/boiler blowdown/roof stormwater drains/aerator basin overflow/electric manhole stormwater drains/slag tank seals. Design flow is 1.844 MGD. Actual flow is 0.677 MGD.

<u>Outfall #004</u> - Non-contract Cooling Water - SIC #4911 Units 1 and 2 once-through cooling water. Design flow is 174.65 MGD. Actual flow is 96.923 MGD.

<u>Outfall #005</u> - Non-contact Cooling Water - SIC #4911 Unit 3 once-through cooling/unit 3 slag tank overflow/slag tank seals. Design flow is 266.40 mad. Actual flow is 164.05 mad.

<u>Outfall #006</u> - Various Sources - SIC #4911, including: Overflow, including carbon filter backwash/demineralizer - effluent samples/chemical cleaning wastes/units 1 and 2 control room treated sanitary waste/unit 3 control room treated sanitary waste/laboratory drain/units 1 and 2 floor drains/units 3 floor drain/all non-PCB oil filled transformer containment drains/condensate polishers backwash /neutralization tank overflow. Design flow is 0.313 MGD. Actual flow is 0.159 MGD.

Outfall #007 Units 1 and 2 fly ash sluice/units 3 fly ash sluice/filter backwash/clarifier sluice/chemical feed area floor drains/neutralization tank discharge/fly ash landfill sedimentation pond. q Design flow is 5.6 MGD. Actual flow is 1.32 MGD.

Outfall #008 - Bliminated.

Outfall #009 - Bliminated.

Outfall #010 Stormwater from various plant areas. Design flow is 0.007 MGD. Actual flow is 0.003 MGD.

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	•				PAGE NUMBER 3 of	F11
A. EFFLUENT LIMITATIONS AND MONI					PERMIT NUMBER MO	
The permittee is authorized to discharge fror final effluent limitations shall become effecti shall be controlled, limited and monitored by	ve upon iss	uance and re	emain in effe			
OUTFALL NUMBER AND EFFLUENT PARAMETER(S)	UNITS	DAILY	FLUENT LI	MITATIONS MONTHLY AVERAGE	MONITOBING REOL MEASUREMENT FREQUENCY	JIREMENTS SAMPLE TYPE
Outfall #001 - Coal Pile Runoff		1	1			
low	MGD	+		•	once/month 24 h	r. total
fotal Suspended Solids	mg/L	50	l	50	once/month	grab
ok - Units	ຣບ	***		***	once/month	grab
il and Grease	mg/L	20		15	once/quarter****	• grab
Outfall #002-Slag Settling Pond						
10W 3214" 1 925	MGD	•		•	once/month 24 h	r. total
ntake Suspended Solids	mg/L	•		•	once/month	grab
olids	mg/L	•		•	once/month	grab
et Total Suspended Solids****	mg/L	100		30	once/month	grab
H - Onits 7, 19	, so	***		***	once/month	grab
11 and Grease	mg/L	20	· .	15	once/quarter****	grab
	mg/L	•		+	once/quarter****	grab
ONITORING REPORTS SHALL BE SUBMITTE		RLY; THE FI	RST REPOR			
Nole Effluent Toxicity & Su VET) Test	rvival		ee Specia mditions		once/year	grab
ONITORING REPORTS SHALL BE SUBMITTE	D ANNUAL	LY: THE FIR	ST REPORT	IS DUE OC	tober 28, 2001.	
tfall # 003-Various Sources				T		
ow	MGD	•		•	once/month 24 hr.	total
take Suspended Solids	mg/L	•		•	once/month	grab
fluent Total Suspended lids	mg/L	••	- 1	•	once/month	grab
t Total Suspended Solids****	mg/L	100		30	once/month	grab
- Units	BU	***		***	once/month	grab
1 and Grease	mg/L	20		15	once/quarter****	grab
NITORING REPORTS SHALL BE SUBMITTED NO DISCHARGE OF FLOATING SOLIDS OR						SHALL
STANDARD CONDITIONS						
ADDITION TO SPECIFIED CONDITIONS STA						
ANDARD CONDITIONS DATED <u>October 1,</u> LLY SET FORTH HEREIN.	1980 and	August 1	5 <u>, 1994</u> , A	ND HEREBY	INCORPORATED AS THO	UGH (

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UNITS	FINAL F	ELLIENT LIM WEEKLY AVERAGE	MONTHLY	MONITORING P	FOUREMENTS SAMPLE TYPE
MGD	-		•	once/week	24 hr. tota
۰F	+	ſ	+	once/week	grab
40				ODCA (NDO)	grab
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AIT TED QUAR	TERLY; TH	E FIRST REPO	ORT IS DUE	January 28, 2001	, <u> </u>
Survival	(See Spe	cial Cond	litions)	once/year	grab
ITTED ANNU	ALLY: THE	FIRST REPOR	TIS DUE	October 28, 2001.	
[· ·
MGD	*		+	once/week	24 hr. total
۰Ŧ	*		*	once/waek	grab
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of river	flow ove	er 5°F (No	te 1)	once/week	calculated
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A. EFFLUENT LIMITATIONS AND		NITORING I	REQUIREME	NTS		PERMIT NUMBER MO-	0004871
The permittee is authorized to diach final fifuent limitations shall becom shall be controlled, limited and mon	e effec	ctive upon is	suance and re	main in effe	oct until exp		
		7	FINAL EFF	LUENT LIM	ITATIONS	MONITORING REQU	IREMENTS
OUTFALL NUMBER AND EFFLUE PARAMETER(S)	NT	UNITS	DAILY	WEEKLY AVERAGE	MONTHLY AVERAGE	MEASUREMENT FREQUENCY	SAMPLE TYPE
Outfall #007 - Fly Ash Por	nd		1				
Flow		MGD	+		•	once/month 24 hr	. total
Intake Total Suspended Sol	Liđe	mg/L	•		+	once/month	grab
Rffluent Total Suspended Solids		mg/L	100		30	once/month	drøp
Net Total Suspended Bolids****		_ mg/L	•		•	once/month	grab
Oil and Grease		ng/L	20		15	once/quarter****	grab
pH - Units		BU	**•		***	once/month	grab
Sulfate		mg/L	i•		*	once/ quarter****	* grab
MONITORING REPORTS SHALL BE S	UBMIT	TED QUART	BRLY: THE FI	RST REPOR	T IS DUE	lanuary 28, 2001.	
Whole Effluent Toxicity (WET) Test	* 8	urvival		e Specia ditions		once/year	grab
MONITORING REPORTS SHALL BE S	UBMIT	TED ANNUAL	LLY; THE FIRE	ST REPORT	IS DUE OC	tobar 28, 2001.	
Dutfall # 10 - Stormwater			T	T		······	
?low		cfe	•		•	cnce/quarter**** e	24 hr. stimate
Dil and Grease		mg/L	20		15	once/quarter****	grab
Settleable Solids		mL/L/hr	2.0		1.0	once/quarter****	grab
0H - Units		90	***		***	once/quarter****	â r øp
otal Suspended Solids		mg/L	*		•	once/quarter****	grab
NONITORING REPORTS SHALL BE SU THE NO DISCHARGE OF FLOATING SO							E SHALL
. STANDARD CONDITIONS						······	
ADDITION TO SPECIFIED CONDITIK TANDARD CONDITIONS DATED Oct HOUGH FULLY SET FORTH HEREIN.							

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Page 6 of 11 Permit No. MO-0004871

A. EFFLUENT LIMITATIONS AND MONITORING REQUIREMENTS (continued) * Monitoring requirement only.

** Reserved

*** pR is measured in pR units and is not to be averaged. The pE is limited to the range of 6.0-9.0 pE units.

**** Intake Total Suspended Solids values should be utilized to calculate "net" effluent limitations. (Effluent value - influent value = net value).

***** Sample once per quarter in the months of February, May, August, and November.

Note 1 - The percent of concurrent receiving-stream flow that exceeds a 5°F increase shall be computed weekly and the results reported quarterly. Complete and uniform mixing shall be assumed, using the following formula:

\$ stream flow = <u>average daily btus/hour</u> exceeding 5°F increase stream flow (cfs) x 11,200*

USGS stream-flow records for the Missouri River at Kansas City shall be used.

*11,200 is 3,600 sec/hr x 62.4 lb/ft³ x 5°F 100

C. SPECIAL CONDITIONS

1. Whole Effluent Toxicity (WET) tests will be conducted as follows:

	SUMMARY O	F WET TESTING FOR 7	THIS PERMIT	
OUTFALL	A.E.C. ¥	FREQUENCY	SAMPLE TYPE	MONTH
#002, #004, #005, #006, & #007	10*	See Special Conditions	24 hr. Composite	January

Whole Effluent Toxicity (WET) tests will be required for Outfalls #004 and #005 only if biocides are used. The WET test will only be required in the first year if the initial test passes. If the WET test does not pass in the first year, the test must be run <u>annually for the duration of the permit</u> or until biocide use is discontinued.

An initial WET test will be required for Outfalls #002, #006, and #007. The WET test will only be required in the first year if it passes at all effluent concentrations. If the WET test does fail at any concentration in the first year, the rest must be run annually for the duration of the permit on Outfall #002, #006 and #007.

- a. Test Schedule and Follow-Up Requirements
 - (1) Perform a single-dilution test in the months and at the frequency specified above.

If the test passes the effluent limit do not repeat test until the next test period. Submit results with the annual report. If the test fails the effluent limit a multiple dilution test shall be

performed within 30 days, and biweekly thereafter until one of the following conditions are met:

- (a) THREE CONSECUTIVE MULTIPLE-DILOTION TESTS PASS. No further tests need to be performed until next regularly scheduled test period.
- (b) A TOTAL OF THREE MULTIPLE-DILUTION TESTS FAIL. DNR's letter. This plan must be approved by DNR before the TIE or TRE is begun. A schedule for completing the TIE or TRE shall be established in the plan approval.

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- C. SPECIAL CONDITIONS (continued)
- 1. Whole Effluent Toxicity (WET) (continued)
- a. Test Schedule and Follow-Up Requirements (continued)
 - (2) The permittee shall submit a summary of all test results for the test series to the Planning Section of the WPCP, DNR, Box 176, Jefferson City, MO within 14 days of the third failed test. DNR will contact the permittee with initial guidance on conducting a toxicity identification evaluation (TIE) or toxicity reduction evaluation (TRE). The permittee shall submit a plan for conducting a TIB or TRE to the Planning Section of the WPCP within 60 days of the date of DNR's letter. This plan must be approved by DNR before the TIE or TRE is begun. A schedule for completing the TIE or TRE shall be established in the plan approval.
 - (3) Upon DNR's approval, the TIE/TRE schedule may be modified if toxicity is intermittent during the TIE/TRE investigations. A revised WET test schedule may be established by DNR for this period.
 - (4) If a previously completed TIE has clearly identified the cause of toxicity, additional TIEs will not be required as long as effluent characteristics remain essentially unchanged and the permittee is proceeding according to a DNR approved schedule to complete a TRE and reduce toxicity. Regularly scheduled WET testing as required in part b. (1) will be required during this period.
 - (5) In addition to the WET test summary report required in part (2), all failing test results shall be reported to DNR within 14 days of the availability of results.
 - (6) All WET test results for the reporting period shall be summarized and submitted to DNR by the end of the following October. When WET test sampling is required to run over one DMR period, each DMR report shall contain information generated during the reporting period.
 - b. PASS/FAIL procedure and effluent limitations
 - (1) To pass a single-dilution test, mortality observed in the ABC test concentration shall not be significantly different (at the 95% confidence level; p = 0.05) than that observed in the upstream receiving-water control. The appropriate statistical tests of significance will be those outlined in the most current USEPA acute toxicity manual or those specified by the MDNR.
 - (2) To pass a multiple-dilution test:
 - (a) the computed percent effluent at the edge of the zone of initial dilution (AEC) must be less than three-tenths (0.3) of the LC₅₀ concentration for the most sensitive of the test organisms, or,
 - (b) all dilutions equal to or greater than the AEC must be nontoxic. Failure of one multiple-dilution test is considered an effluent limit violation.

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Page 8 of 11 Permit No. MO-0004671

C. SPECIAL CONDITIONS (continued)

- 1. Whole Effluent Toxicity (WET) (continued)
 - c. Test Conditions
 - (1) Test species: Cariodaphnia dubia and fathead minnows, Pimephales promelas. Organisms used in WET testing should come from cultures reared for the purpose of conducting toxicity tests and should be cultured in a manner consistent with the most current USEPA guidelines. All test animals should be cultured as described in EPA-600/4-90/027.
 - (2) Test period: 48 hours at the "Acceptable Bffluent Concentration" (AEC) specified above.
 - (3) When dilutions are required, upstream receiving stream water will be used as dilution water. If upstream water is unavailable or if mortality in the upstream water exceeds 10%, "reconstituted" water will be used. Procedures for generating reconstituted water will be supplied by the Department of Natural Resources (DNR).
 - (4) Tests should be initiated immediately after the sample is collected, but tests must be initiated no later than 36 hours after collection.
 - (5) Single-dilution tests will be run with:
 - (a) Effluent at the AEC concentration;
 - (b) 100% receiving-stream water (if available), collected upstream of the outfall at a point beyond any influence of the effluent; and reconstituted water.
 - (c)
 - (6) Multiple-dilution tests will be run with: (a)
 - 100%, 50%, 25%, 12.5%, and 6.25% effluent, unless the AEC is less than 25% effluent, in which case dilutions will be 4 times the AEC, two times the AEC, AEC, 1/2 AEC and 1/4 AEC.
 - (b) 100% receiving-stream water (if available), collected upstream of the outfall at a point beyond any influence of the effluent; and
 - (c) reconstituted water.
 - (7) If reconstituted-water control mortality for a test species exceeds 10t, the entire test will be rerun.
- 2. Report as no-discharge when a discharge does not occur during the report period.
- This permit may be reopened and modified, or alternatively revoked and reissued, to: з. (a) Comply with any applicable effluent standard or limitation issued or approved under Sections 301(b)(2)(C) and (D), 304(b)(2), and 307(a)(2) of the Clean Nater Act, if the effluent standard or limitation so issued or approved:
 - contains different conditions or is otherwise more stringent than any (1) effluent limitation in the permit; or
 - (2) controls any pollutant not limited in the permit.
 - (b) Incorporate new or modified effluent limitations or other conditions, if the result of a waste load allocation study, toxicity test or other information indicates changes are necessary to assure compliance with Missouri's Water Quality Standards.
 - (c) Incorporate new or modified effluent limitations or other conditions if, as the result of a watershed analysis, a Total Maximum Daily Load (TMDL) limitation is developed for the receiving waters which are currently included in Missouri's list of waters of the state not fully achieving the state's water quality standards, also called the 303(d) list.

The permit as modified or reissued under this paragraph shall also contain any other requirements of the Clean Water Act then applicable.

4. There shall be no discharge of polychlorinated biphenyl compounds.

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C. SPECIAL CONDITIONS (continued)

- 5. Discharge of wastewater from this facility must not alone or in combination with other sources cause the receiving stream to violate the following:
 - (a) Water temperature and temperature differentials specified in Missouri Water Quality Standards shall be met.
- 6. Any pesticide discharge from any point source shall comply with the requirements of the Federal Insecticide, Fungicide, and Rodenticide Act, as amended (7 U.S.C. 136 et. seq.) and the use of such pesticides shall be in a manner consistent with its label.
- 7. Neither free available chlorine nor total residual chlorine may be discharge from any unit for more than two hours in any one day.
- An upset provision, identical to the upset provision set forth at 40 CSR 122.41(n), is hereby incorporated in this permit.
- 9. Changes in Discharges of Toxic Substances

The permittee shall notify the Director as soon as it knows or has reason to believe:

- a. That any activity has occurred or will occur which would result in the discharge of any toxic pollutant which is not limited in the permit, if that discharge will exceed the highest of the following :notification levels:"
 - (1) One hundred micrograms per liter (100 ug/L);
 - (2) Two hundred micrograms per liter (200 ug/L) for acrolein and acrylonitrile; five hundred micrograms per liter (500 ug/L) for 2, 5 dinitrophenol and for 2-methyl-4, 6-dinitrophenol; and one milligram per liter (1 mg/L) for antimony;
 - (3) Five (5) times the maximum concentration value reported for the pollutant in the permit application;
 - (4) The level established in Part A of the permit by the Director.
- b. That they have begun or expect to begin to use or manufacture as an intermediate or final product or byproduct any toxic pollutant which was not reported in the permit application.
- 10. Permittee is to abandon the domestic waste facilities described herein and shall connect the tributary waste load to trunk sewers within 90 days of notice of availability if trunk sewers operated by one of the authorities outlined in Section (3) (B) 1 or 2 of Clean Water Commission Regulation 10 CSR 6.010 are made available to the site during the time a valid discharge permit exists.
- 11. Sludge and Biosolids Use for Domestic Wastewater Treatment Facilities
 - a. Permittee shall comply with the pollutant limitations, monitoring, reporting, and other requirements in accordance with the attached permit Standard Conditions.

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C. SPECIAL CONDITIONS (continued)

12. Use or Disposal of Ash from Power Plants

- a. Disposal of ash is not authorized by this permit.
- b. This permit does not pertain to permits for disposal of ash or exemptions for beneficial uses of ash under the Missouri Solid Waste Management Law and regulations.
- c. This permit does not authorize off-site storage, use of disposal of ash in regard to water pollution control permits required under 10 CSR 20-6.015 and 10 CSR 20-6.200.
- d. Ash stored in on-site treatment ponds (ash ponds) shall not cause a discharge to subsurface waters of the state. Ash ponds which have a leakage rate exceeding the limitations under 10 CSR 20-8.020 and 10 CSR 20-8.200 are discharges to waters of the state and must by authorized by permit.
- e. An annual report shall be submitted by January 28 each year for the previous calendar year period. The report shall include the quantity of ash generated; the cumulative quantity of ash stored on-site at the end of the year, including ash ponds; the quantity of ash sold or given away to each customer, and the intended use of the ash.
- 13. General Criteria. The following water quality criteria shall be applicable to all waters of the state at all times including mixing zones. No water contaminant, by itself or in combination with other substances, shall prevent the waters of the state from meeting the following conditions:
 - a. Waters shall be free from substances in sufficient amounts to cause the formation of putrescent, unsightly or barmful bottom deposits or prevent full maintenance of beneficial uses;
 - b. Waters shall be free from oil, scum and floating debris in sufficient amounts to be unsightly or prevent full maintenance of beneficial uses;
 - c. Waters shall be free from substances in sufficient amounts to cause unsightly color or turbidity, offensive odor or prevent full maintenance of beneficial uses;
 - d. Waters shall be free from substances or conditions in sufficient amounts of result in toxicity to human, animal or equatic life;
 - E. There shall be no acute toxicity to livestock or wildlife watering;
 - f. Waters shall be free from physical, chemical or hydrologic changes that would impair the natural biological community;
 - g. Waters shall be free from used tires, car bodies, appliances, demolition debris, used vehicles or equipment and solid waste as defined in Missouri's Solid Waste Law, section 260.200, RSMo, except as the use of such material is specifically permitted pursuant to section 260.200-260.247;
- 14. Once per year, permittee will inspect soil covered ash pile to ascertain that erosion has not occurred and that vegetation is adequate to control erosion. This should be submitted to the department annually.

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SUMMARY OF TEST METHODOLOGY FOR WHOLE-EFFLUENT TOXICITY TESTS

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Whole-effluent-toxicity test required in NFDES permits shall use the following test conditions when performing single or multiple dilution methods. Any future changes in methodology will be supplied to the permittee by the Missouri Department of Natural Resources (MDNR). Unless otherwise specified by MDNR, procedures should be consistent with <u>Methods for Measuring the Acute Toxicity of Effluents and Receiving Waters to</u> <u>Freshwater and Marine Organisms</u>, <u>BPA/600/4-90/027</u>.

Test conditions for Ceriodaphnia dubia:

Test duration: Temperature: Light Quality: Photoperiod: Size of test vessel: Volume of test solution: Age of test organisms: No. of animals/test vessel: No. of replicates/concentration: No. of organisms/concentration: Feeding regime: Aeration: Dilution water:

Endpoint:

Test acceptability criterion:

Test conditions for (Pimephales promelas) :

Test duration: T mperature: Light Quality: Photoperiod: Size of test vessel: Volume of test solution: Age of test organisms: No. of animals/test vessel: No. of replicates/concentration:

No. of organisms/concentration:

Feeding regime: Aeration:

Dilution water:

Endpoint:

Test Acceptability criterion:

25 ± 2°C Ambient laboratory illumination 16 h light, 8 h dark 30 mL (minimum) 15 mL (minimum) <24 h old 5 20 (minimum) None (feed prior to test) None Upstream receiving water; if no upstream flow, synthetic water modified to reflect effluent hardness. Mortality (Statistically significant difference from upstream receiving water control at ps 0.05)

90% or greater survival in controls

48 h 25 ± 2°C Ambient laboratory illumination 16 h light/ 8 h dark 250 mL (minimum) 200 mL (minimum) 1-14 days (all same age) 10 4 (minimum) single dilution method 2 (minimum) multiple dilution method 40 (minimum) single dilution method 20 (minimum) multiple dilution method None (feed prior to test) None, unless DO concentration falls below 4.0 mg/L; rate should not exceed 100 bubbles/min. Upstream receiving water; if no upstream flow, synthetic water modified to reflect effluent hardness. Mortality (Statistically significant difference from upstream receiving water control at ps 0.05) 90% or greater survival in controls

Date of Fact Sheet: June 21, 2000

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STANDARD CONDITIONS FOR NPDES PERMITS ISSUED BY THE MISSOURI DEPARTMENT OF NATURAL RESOURCES MISSOURI CLEAN WATER COMMISSION AUGUST 15, 1994

PART III - SLUDGE & BIOSOLIDS FROM DOMESTIC WASTEWATER TREATMENT FACILITIES

SECTION A - GENERAL REQUIREMENTS

- This permit pertains to sludge requirements under the Missouri Clean Water Law and regulations and incorporates applicable federal sludge disposal requirements under 40 CFR 503. The Environmental Protection Agency (EPA) has principal authority for permitting and enforcement of the federal sludge regulations under 40 CFS 503 until such time as Missouri is delegated the new EPA sludge program. EPA has reviewed and accepted these standard sludge conditions. EPA may choose to issue a separate sludge addendum to this permit or a separate federal sludge permit at their discretion to further address federal requirements.
- These PART III Standard Conditions apply only to sludge and biosolids generated at domestic wastewater treatment facilities, including public owned treatment works (POTW) and privately owned facilities.
- 3. Sludge and Biosolids Use and Disposal Practices.
 - a. Permittee is authorized to operate the sludge and biosolids treasment, storage, use, and disposal facilities listed in the facility description of this permit.
 - b. Permittee shall not exceed the design studge volume listed in the facility description and shall not use studge disposal methods that are not listed in the facility description, without prior approval of the permitting authority.
 - Permittee is authorized to operate the storage, treatment or generating sites listed in the Facility Description section of this permit.
 - d. A separate operating permit is required for each operating location where sludge or biosolids are generated, stored, treated, or disposed, unless specifically exempted in this permit or in 10 CSR 20, Chapter 6 regulations. For land application, see section H, subsection 3 of these standard conditions.
- 4. Sludge Received From Other Facilities
 - a. Permittees may accept domestic wastewater sludge from other facilities including septic tank pumpings from residential sources as long as the design sludge volume is not exceeded and the treatment facility performance is not impaired.
 - b. The permittee shall obtain a signed statement from the sludge generator or hauler that certifies the type and source of the sludge.
 - c. Sludge received from out-of-state generators shall receive prior approval of the permitting authority and shall be listed in the facility description or special conditions section of the permit.
- 5. These permit requirements do not supersede nor remove liability for compliance with county and other local ordinances.
- These permit requirements do not supersede nor remove liability for compliance with other environmental regulations such as odor emissions under the Missouri Air Pollution Control Law and regulations.
- 7. This permit may (after due process) be modified, or alternatively revoked and reissued, to comply with any applicable sludge disposal standard or limitation issued or approved under Section 405(d) of the Clean Water Act or under Chapter 644 RsMo.
- 8. In addition to these STANDARD CONDITIONS, the department may include shudge limitations in the special conditions portion or other sections of this parmit.
- 9. Alternate Limits in Site Specific Permit.
 - Where deemed appropriate, the department may require an individual site specific permit in order to authorize alternate limitations:
 - a. An individual permit must be obtained for each operating location, including application sites.
 - b. To request a site specific permit, an individual permit application, permit fees, and supporting documents shall be submitted for each operating location. This shall include a detailed shudge/biosolids management plan or engineering report.
- 10. Exceptions to these Standard Conditions may be authorized on a case-by-case basis by the department, as follows:
 - a. The department will prepare a permit modification and follow permit public notice provisions as applicable under 10 CSR 20-6.020, 40 CFR 124.10, and 40 CFR 501.15(a)(2)(ix)(E). This includes notification of the owners of property located adjacent to each land application site, where appropriate.
 - b. Exceptions cannot be granted where prohibited by the federal sludge regulations under 40 CFR 503.
- 11. Compliance Period

Compliance shall be achieved as expeditiously as possible but no later than the compliance dates under 40 CFR 503.2.

140	WATER POLLUTION C					
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oecermin property	ation has been made under m gather and evaluate the inform	y direction or superv nation used to deter	nine these requir	rements have be	en met. I am aware that t	here are significant
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		MISSOURI DEPARTMENT OF NATURAL RESOURCES DIVISION OF ENVIRONMENTAL QUALITY NPDES MONITORING REPORT FOR NON-MUNICIPAL WASTEWATER DISCHARGES	ARTMENT OF N IVIRONMENTAL	POR POR	ALITY LITY	SOUR	CES I-MUN	IICIPAL	L WAST	lewat	ER DI	ISCHARGES			
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		Report results of all analyses, even if performed more frequently than required by Part A of the permit. Report results of all analyses, even if performed more frequently than required by Part A of the permit. File a report even if discharge is intermittent and no discharge occurred during the monitoring period for the dates the facility was checked, and sign the report. NOTE: If a discharge occurs any time during Under "Sample Type" Indicate whether sample analyzed was: (a) grab sample; (b) 24-hour compos of sample required for each parameter.	es, even if perfor rge is intermitter is checked, and s icate whether sa h parameter,	med n tt and lign th mple	nore fr no dis le repol analyza	squently charge c t. NOTE xd wes:	than rai occurrad 5 If a dis (a) grat	quirad by I during t scharge o sampte;	Part A o the monit ocurs an (b) 24-h	l the per oring per / time du our com	nit riod. Co ring the posite s	mplete the identification monitoring period, it n ample, or (c) modified	Report results of all analyses, even if performed more frequently than required by Part A of the permit. Report results of all analyses, even if performed more frequently than required by Part A of the permit. File a report even if discharge is intermittent and no discharge occurred the monitoring period. Complete the identification section, write "ND" in the appropriate columns for the dates the facility was checked, and sign the report. NOTE: if a discharge occurs any time during the monitoring period, it must be reported. Under "Sample Type" indicate whether sample analyzed was: (a) grab sample; (b) 24-hour composite sample; or (c) modified composite sample. NOTE: See permit for type of sample required for each parameter.	ropriate columns s permit for type	
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Revised

October 1, 1980

PART I. GENERAL CONDITIONS SECTION A - MONITORING AND REPORTING

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Representative Sampling t.

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- Sumples and measurements taken as required herein shall be а. representative of the nature and volume, respectively, of the monitored discharge. All samples shall be taken at the outfall(s), and unless specified, before the effluent joins or is diluted by any other body of enter of substance.
- Monitoring results shall be recorded and reported on forms provided Ь. by the Department, postmarked no later than the 28th day of the month following the completed reporting period. Signed copies of these, and all other reports required herein, shall be submitted to the remeative Department Regional Office, the Regional Office address is indicated in the cover letter transmitting the permit,

Schedule of Compliance

No later than fourier (14) calendar days following each date identified in the "Schedule of Compliance", the permittee shall submit to the respective Department Regional Office as required therein, either a report of progress or, in the case of specific actions being required by identified dates, a written notice of compliance or noncompliance. In the latter case, the notice shall include the cause of noncompliance, any remedial actions taken, and the probability of mosting the next scheduled requirements, or if there are no more entered and an analysis and a such associations will be a such as ch as a such as a such as a such as permit

Definitions 3.

Definitions as set forth in the Missouri Clean Water Law and Missouri Clean Water Commission Definition Regulation 10 CSR 20-2.010 shall soply to terms used herein.

Test Procedures

Test procedures for the analysis of pollutan shall be in accordance with the Mictouri Clane Water Commission Effluent Regulation 10 CSR 20-7015.

Recording of Results ٩.

- For each measurement or sample taken pursuant to the requirements of this permit, the permittee shall record the following information:
 - the date, exact place, and time of sampling or measurements, ന the individual(s) who performed the sampling or measurements;
 - (iii) the date(s) analyses were performed; (iv) the individual(s) who performed the analyses;
 - the analytical techniques or methods used; and (v)
 - (vi) the results of such analyses.
- The Federal Clean Water Act provides that any person who falsifies, transers with, or knowingly renders inscructs any monitoring device or method required to be maintained under this permit shall, upon conviction, be punished by a fine of not more than \$10,000 per violation, or by imprisonment for not more than six (6) months per violation, or both
- Calculations for all limitations which require averaging of measurements shall utilize an arithmetic mean unless otherwise C. specified by the Director in the permit.

Additional Monitoring by Permittee б.

If the permittee menitors any pollutant at the location(s) designated herein more frequently than required by this permit, using approved analysical methods as specified above, the results of such monitoring shall be included in the calculation and reporting of the values required in the Monitoring Report Forms. Such increased frequency shall also be indicated.

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Records Retendon 7.

Records Resentation. The permittee shall retain records of all monitoring information, including all calibration and maintenance records and all original strip chart recording for continuous monitoring instrumentation, copies of all reports required by this permit, and records of all data used to complete the application for this this permit, and records of 24 man used to complete the sympathod for this permit, for a period of at least three (3) years from the date of the sample, measurement, report or application. This period may be extended by request of the Department at any time.

SECTION B - MANAGEMENT REQUIREMENTS

- Change in Discharge 2
 - All discharges authorized herein shall be consistent with the terms and All machanges automotions have a solution of charge of any polinizant not authorized by this permit or any polinizant identified in this permit more frequently than or at a level in excess of that authorized shall constitute a violation of the permit.
 - Any facility expensions, production increases, or process modific which will result in new, different, or increased discharges of pullutants shall be reported by submission of a new NPDES application at least sixty (60) days before each such changes, or, if they will not violate the effluent limitations specified in the permit, by notice to the Department at least thirty (30) days before such changes.

Noncommune Notification

- If, for any reason, the permittee does not comply with or will be unable It to employ with any daily maximum effluent limitation specified in this permit, the permittee shall provide the Department with the following information, in writing within five (5) days of becoming sware of such conditions:
 - (i) a description of the discharge and cause of noncompliance, and the period of noncompliance, including exact dates and times or, (ii) if not corrected, the anticipated time the noncompliance is expected to continue, and steps being taken to reduce, eliminate and prevent 'recurrence of the noncomplying discharge. Twenty-four hour reporting. The permittee shall report any
- ъ. noncompliance which may endanger beach or the environment. Any information shall be provided orally with 24 hours from the time the permittee becomes aware of the circumstances. A written submission shall also be provided with five (5) days of the time the permittee becomes sware of the circumstances. The Department may waive the written report on a case-by-case basis if the oral report has been received within 24 hours.

Facilities Operation

Parameter operation Permittees shall operate and maintain facilities to comply with the Missouri Clean Water Law and applicable permit conditions. Operators or supervisors of operations at publicly owned or publicly regulated wassewater treatment facilities shall be certified in accordance with 10 CSR 209.020(2) and any other applicable law or regulation. Operators of other wastewater treatment facilities, water contaminant source or point sources, shall, upon request by the Department, demonstrate that wastewater treatment equipment and facilities are effectively operated and maintained by competent personnel.

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Adverse Impact

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The permittee shall take all necessary steps to minimize any severae impact to waters of the state resulting from acacompliance with any effluent limitations specified in this permit or set forth in the Missouri Clean Water Law and Regulations (bereinafter the Law and Regulations), including such acorderated or additional monitoring as necessary to determine the Galife and impact of the noncomplying discharge.

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SIBLEY GENERATING STATION		_		350-290	
ADORESS 33200 EAST JOHNSON ROAD	слу SIBL	EY	STATE MO		^{ZIP} 64088
2.00 CURRENT OWNER					
AQUILA, INC.				PHONE E-MAIL	816-467-3321 steve.brooks@
ADDRESS 20 WEST 9 TH				aquila. STATE MO	z⊮ 64105
3.00 CONTINUING AUTHORITY: (If same	as owner, write			<u> </u>	<u> </u>
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SIBLEY GENERATING STATION		MO-0004871	816-650-2900	
ADDRESS	CITY	I	STATE	ZIP
33200 EAST JOHNSON ROAD	SIBLEY		MO	64088
6.00 FUTURE OWNER				
NAME			TELEPHONE N	JMBER
KANSAS CITY POWER & LIGHT COMP	ANY		816-556-2	200
ADDRESS	CITY		STATE	ZIP
1201 WALNUT STREET	KANSA	SCITY	мо	64106-212
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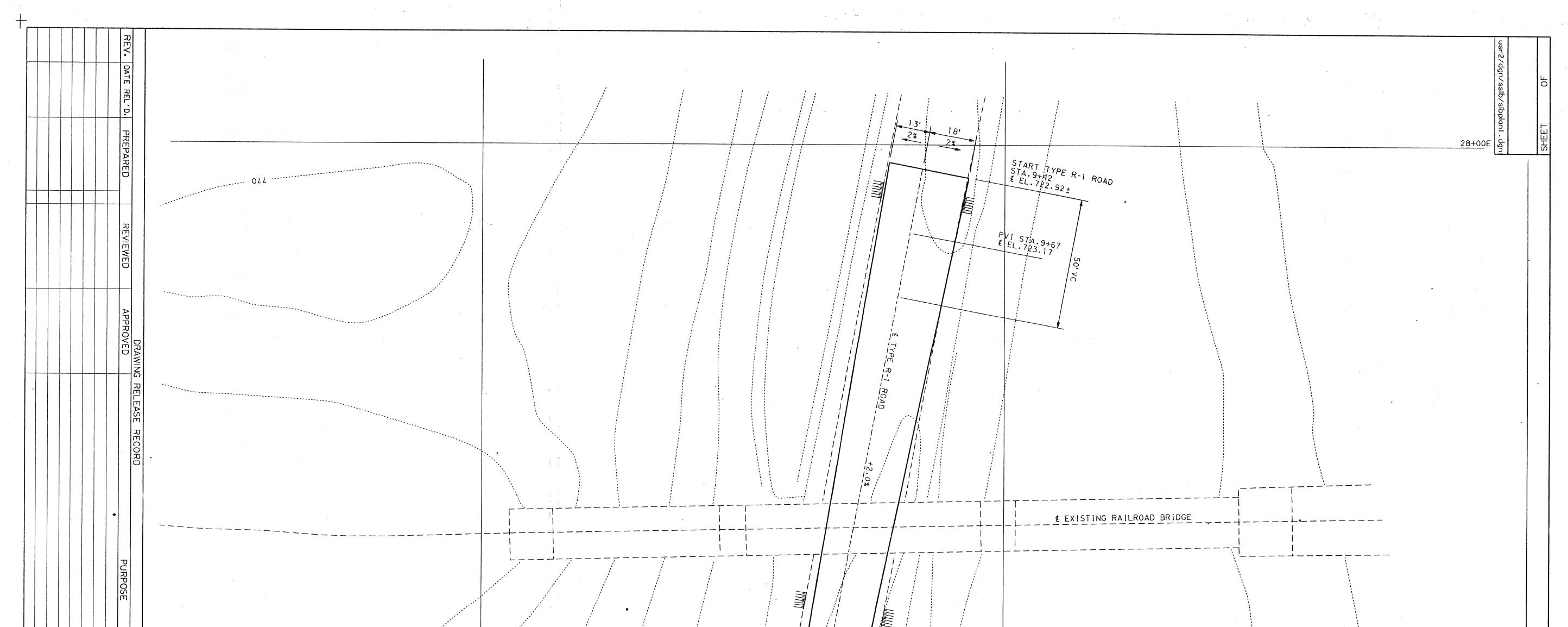
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MISSOURI PUBLIC SERVICE SIBLEY GENERATING STATION CONSTRUCTION PERMIT FOR FLY ASH POND MODIFICATIONS

As part of its acid rain compliance plan at the Sibley Generating Station, Missouri Public Service (MPS) is planning to switch from a high-sulfur Illinois coal to a low sulfur western coal blend by the year 1995. The Sibley Generating Station is located along the Missouri River in Jackson County approximately one-half mile east of Sibley, Missouri.

Although the Sibley Generating Station will not begin burning the blended coal on a permanent basis until 1995, construction for modifying plant systems to burn the blended fuel will begin in September of this year. As part of the plant modifications, the existing fly ash handling and pond disposal system will be altered. These fly ash pond modifications will require a construction permit. Proposed fly ash pond and ash disposal system modifications are as follows.

1. Fly Ash Handling System Modifications:

Precipitator ash will be pneumatically conveyed from the plant to a new fly ash silo located at the west end of the existing fly ash pond. Precipitator ash is currently sluiced from the plant and discharged directly into the west end of the fly ash pond. New ash lines will be routed along the existing ash piping corridor.

Economizer ash will continue to be sluiced to the fly ash pond through the existing ash conveying system. Slag will continue to be sluiced to existing dewatering pond facilities located west of the plant.

2. Fly Ash Pond and Disposal Modifications:

The western side of the fly ash pond will be filled with slag or soil for siting the new fly ash silo (see construction drawings accompanying this letter). An area approximately 75 feet by 120 feet will be reclaimed for silo placement. The silo foundation will be placed on driven steel piles. The existing ash sluice lines will be extended in a concrete pipe trench to the relocated west pond slope.

Precipitator ash can be handled three ways from the silo to provide disposal flexibility; 1) the fly ash can be mixed with water and sluiced into the fly ash pond; 2) the fly ash can be loaded dry onto bulk trucks for potential sell; or 3) the fly ash can be conditioned with water in a pugmill and loaded onto trucks for disposal at the existing fly ash landfill.

Several improvements were made to the fly ash pond as part of pond cleanout and ash landfill operations in 1988 and 1989. The cleanout and landfill operations were permitted through MDNR waste management program. As part of this construction permit application, MPS is proposing to revise the existing permit to incorporate these improvements. Existing fly ash pond improvements (see Dwg. Y5) made as part of the pond cleaning project are as follows:

1. Additional Pond Overflow Pipe:

A pond overflow pipe was placed north of the existing fly ash pond outfall structure. The pipe discharges into the limestone bed structure just north of where the existing pond overflow pipe enters the structure (See Drawing Y8).

The new overflow pipe was placed at a lower elevation than the existing outfall to enable lowering of the fly ash pond water level. The pond water level is lowered during pond cleanout operations to facilitate dewatering and removal of deposited ash. The overflow pipe is provided with adjustable risers to allow fluctuation of the water level. This enables the pond level to be incrementally increased as the pond is filled which promotes better distribution of deposited ash.

2. <u>Center Dewatering Dike</u>:

An earthen dewatering dike was constructed across the center of the fly ash pond. The dike divides the pond into an east and west cell, and enables the west cell to be taken out of service, dewatered, and cleaned. The center dike also acts as a weir to improve sedimentation of ash in the west cell. Care was taken during construction of the center dike to avoid excavation of the pond's clay liner. Deposited ash was removed as the earthen dike was extended.

3. Fly Ash Sluice Line Extension:

Two 16-inch diameter High Density Polyethylene (HDPE) pipes were placed abovegrade along the outer shoulder of the south fly ash pond dike. The pipes discharge into the east pond cell so that the west cell is bypassed during pond cleaning operations. The HDPE extension pipes are connected to the existing fiberglass ash lines during pond cleanings with a flanged connection.

4. Floating Silt Fences:

Floating silt fences are placed along the flow path of the east cell during pond cleaning operations when the fly ash sluice line extensions are used. The silt fences filter the pond flow to improve pond discharge quality. The silt fences consist of a geotextile fabric suspended from a series of floats.

5. Shot Rock Work Pads:

Work pads constructed out of quarried limestone were placed in the west pond cell to access the center of the fly ash pond for removal of deposited fly ash. Rock is transferred between work pads as required to extend pads to desired cleanout locations. Deposited ash is removed as the pads are extended. Care is taken not to excavate into the clay liner as the rock is placed.

6. Landfill Return Water Line:

A 12-inch diameter HDPE pipe was placed from the landfill sedimentation pond to the fly ash pond. Landfill stormwater runoff and leachate overflows from the sedimentation pond into the return water line where it drains by gravity to the fly ash pond and is discharged through NPDES permitted Outfall 007. The return water line runs both above and below grade along the fly ash haul road. The routing and function of this line was included in the landfill operation permit application.

7. Pond pH Adjustment:

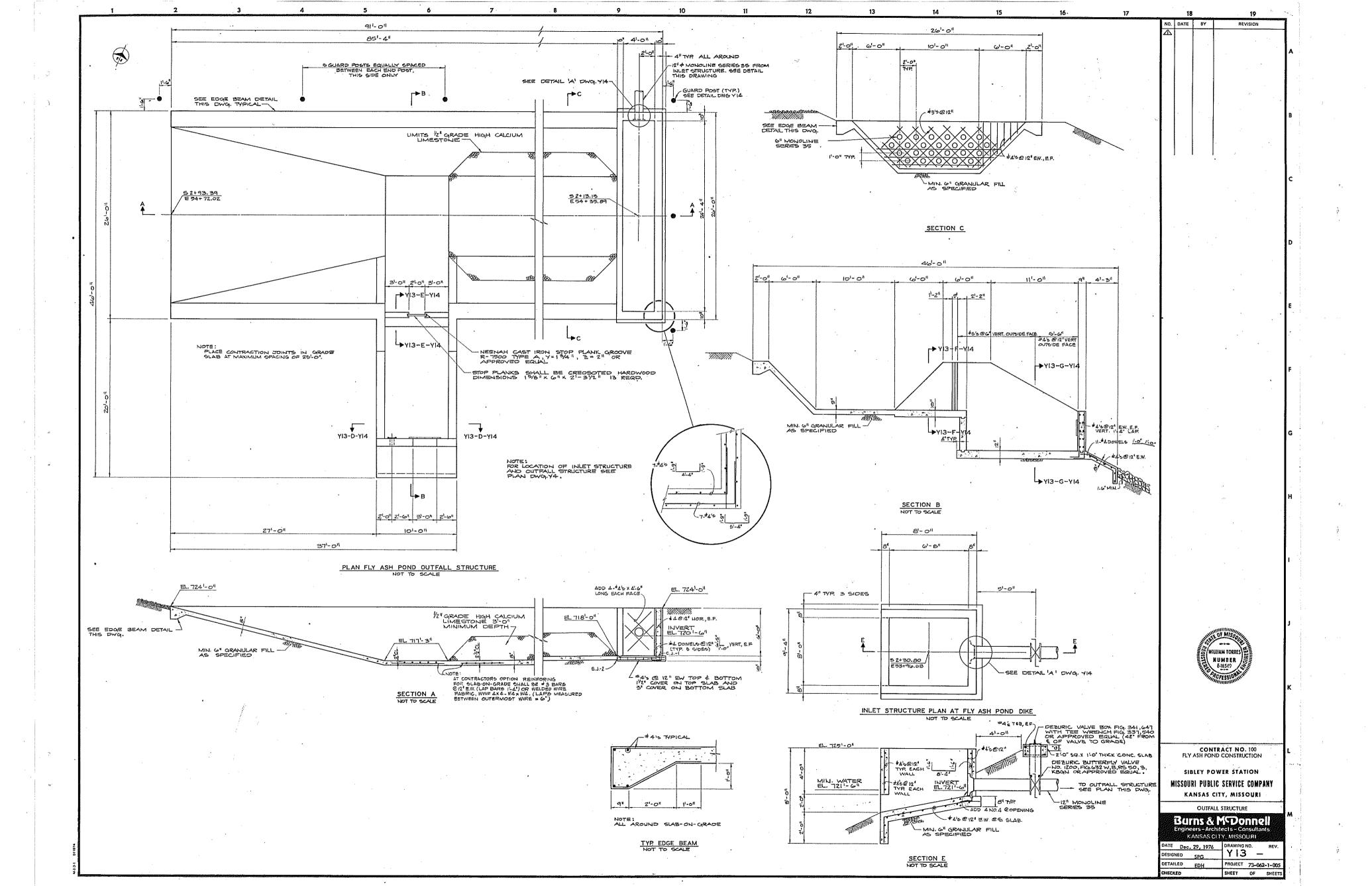
The method of pH adjustment in the fly ash pond was modified due to ongoing pluggage problems occurring in the limestone bed structure. The structure was constructed when the pond was built in 1976. Overflow from the pond flowed through a limestone bed in the structure to raise the pH. However, lower pH pond water reacted with the limestone and formed a gel which plugged the limestone bed.

Pond pH adjustment is now performed at the plant by chemical injection. Lime is occasionally added to the fly ash pond when pond pH is low. Fly ash pond overflow continues to flow through the limestone bed structure without the limestone bed. The NPDES sampling point continues to be at the limestone bed structure discharge.

The fly ash pond modifications are not anticipated to have an adverse effect on pond performance. Though the fly ash silo, center dewatering dike and work pads consume a small percentage of the fly ash pond storage capacity, the treatment capability of the pond has been enhanced by the center dike, additional overflow pipe and silt fences. No significant increase in flow to or solids loading in the pond is anticipated. Historically the fly ash pond has met NPDES effluent limitations and should continue to meet these limits in the future provided periodic removal of deposited ash continues in the west pond cell.



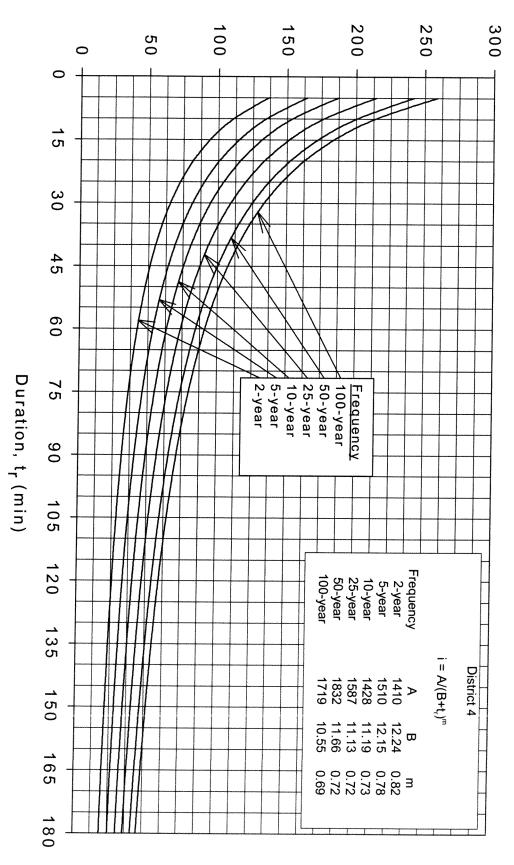
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Calculation Shee

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$i = \frac{1719}{(10.55 + 1440)^{.69}} = 11.32$	
3' - 11.32/2 = 2.05' of F After storm	OK





Intensity, i (mm/hr)

in juin 116177

MEMORANDUM

January 26, 1977

То:	Bill	Torres	<─
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From: Patrick Goeke

Re: Subsurface Recommendation for Fly Ash Pond Missouri Public Service - Sibley Project: 73-062-1-005

I. DRILLING AND TESTING RESULTS

Subsurface Investigation: Fly Ash Pond

The subsurface investigation for the proposed Ash Disposal Pond consisted of nineteen auger borings with bag samples taken at approximately 5 foot intervals. Laboratory testing included classification tests and strength tests. The resistivity survey conducted by staff geologists was unreliable due to the heterogeneous deposits in the river valley. The locations of the borings are shown on the attached drawings.

The borings in the fly ash pond indicate that the soil is an alluvial deposit consisting mainly of clean sands, silty sands, and silts of low plasticity. Some highly plastic and varved clays were found. These clay deposits are usually isolated lenses. The amount and distribution of clay found on the site will not be sufficient to prevent seepage from the pond.

To prevent seepage from the pond, an impervious liner will be required.

Subsurface Investigation: Borrow Area

Five preliminary borings were drilled in the field in the vicinity of line E 75+00. Each boring was drilled approximately 20 feet with bag samples taken at 5 foot intervals. These borings indicate that at least 20 feet of clayey silts (loess) exist over the site.

Laboratory tests were run on bag samples obtained from the borrow area. Atterburg limit tests indicate that the soil is a CL type soil with a liquid limit from 37 to 46 and a plastic index from 14 to 21.

Standard proctor tests indicate that this material has a maximum dry density of 103 pcf and an optimum moisture content of 18%.

Four permeability tests were run on combined samples with the calculated

permeability coefficient (k) ranging from 10^{-6} to 10^{-7} cm/sec. These samples were compacted to approximately 90% of maximum density.

One sieve and hydrometer test is being run with no results as of this date.

As of this date, final drilling for contract 100 is complete. Seven 30 foot borings were drilled in the proposed borrow area as shown on Drawing No. 3. The borings indicate that the soil in the borrow area is as good as that found in the preliminary borings. Laboratory tests will be assigned this week. When the laboratory tests are complete, the subsurface investigation work for this contract will be concluded.

II. DESIGN RECOMMENDATIONS

Liner Requirements

The preliminary tests run on samples from the borrow area indicate that the soils in the borrow area will be suitable for use as a pond liner.

Liquid Limits:	ranges from 44 to 37		
Plastic Limits:	ranges from 22 to 24		
Plastic Index:	ranges from 13 to 21		
Maximum Dry Density:			
Permeability:	10 ⁻⁶ to 10 ⁻⁷ cm/sec		
Hydrometer Analysis:	Incomplete		

In discussing the problem with Dr. Roy Leonard, he felt that the loess from the borrow area would provide an adequate liner if it is compacted to $92\% \pm 5\%$ of the maximum dry density. Moisture should be held between optimum and optimum plus 4%.

The thickness of the liner will be dependent on the seepage requirements set down by the state.

Dike Requirements

Construction of dikes between Sta. 0+00 and Sta. 23+50 will be as shown in Figure #1.

Construction of dikes between Sta. 23+50 and Sta. 51+00 will be as shown in Figure #2.

-2-

The following requirements shall apply:

<u>Type A soil</u> shall be limited to soil taken from the designated borrow areas. Type A sections of the dike should be compacted using sheeps foot rollers to $92\% \pm 5\%$ of the maximum dry density as determined by the Standard proctor. Moisture control is necessary and should be held between optimum and optimum plus 4%. Compactions will be in 6" uncompacted lifts.

<u>Type B material</u> can be any material removed from the pond area as waste material. Type B sections of the dike shall be compacted in 6" uncompacted lifts. Compaction shall be specified by a performance specification with the contractor making 5 passes with a sheeps foot roller.

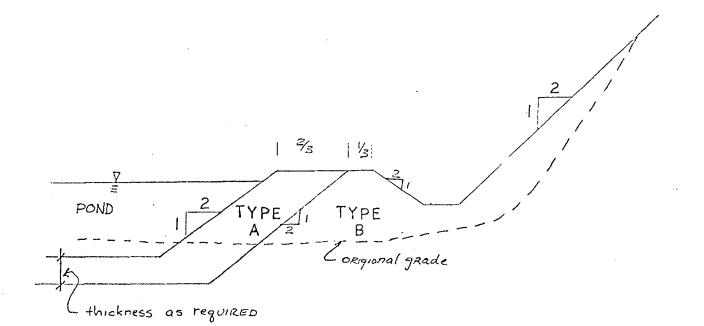


FIGURE I STA 0+00 TO 23+50

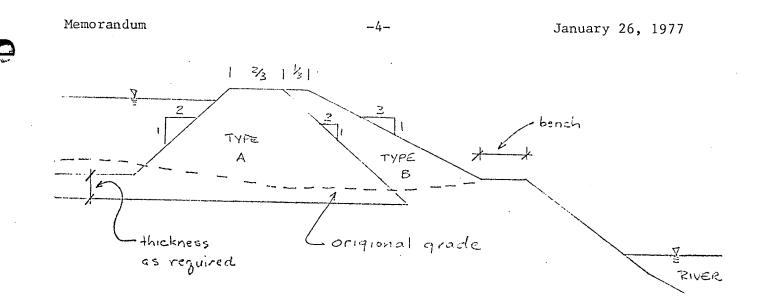


FIGURE 2 STA 23+50 TO 51+00

III. ASH POND DIKE STABILITY

A preliminary analysis of the stability of the proposed dikes for the fly ash pond has been completed. Three locations considered to be the least stable were investigated. The stations investigated were 31+00, 34+50 and 46+00.

Sta. 31+00

The factor of safety for the dike depends on the soil values given the loess fill and the underlying strata. Test samples from boring AP-5 indicate that the underlying clay strata has an undrained shear strength of 300 psf. The sand strata has an estimated value of 30° for the friction angle.

The loess fill was given a cohesion of 500 psf and a \emptyset of 10 degrees. Subsequent direct shear test on a remolded sample of loess indicates that the loess may act as a sand with a \emptyset of 26[°] and a cohesion of 100 psf.

For the 2:1 dike at Sta. 31+00 without a bench the factor of safety was 0.89 for the clayey loess ($\phi = 10^{\circ}$, c = 500). The factor of safety decreased to 0.91 for the sandy loess ($\phi = 26^{\circ}$, c = 100).

When the dike is moved away from the river to provide a 15 foot bench between the dike and the river bank, the factor of safety for the clayey

January 26, 1977

loess dike increases to 1.90. For the sandy loess fill the factor of safety with the 15 foot bench was computed to be 1.77.

Sta. 46+00

The soil at Sta. 46+00 is similar to that of Sta. 31+00 except for a decrease in the thickness of the clay layer. The strength values for the soil remain the same.

For the 2:1 dike without a bench, the factor of safety was computed to be 1.36 for the clayey loess. With sandy loess, the factor of safety decreased to 1.21. The addition of a 15 foot bench increases the factor of safety additionally.

Sta. 34+50

Two borings were taken approximately 150 feet from Sta. 34+50. Boring AP-7, to the east, consisted of 20 feet of poorly graded medium sand. Boring AP-9, to the west, consisted of 9 feet of sandy silty, overlying 11^+ feet of medium stiff silty clay (c = 500 psf). Dikes were analyzed with clayey loess. No Bench

The sand was estimated to have a \emptyset of 28[°]. The computed factor of safety for the sand profile was found to be 1.31.

When analyzing the profile with an 11 foot clay layer overlying sand, the factor of safety decreased to 1.01.

15 Foot Bench

When analyzing the sand profile with a 15 foot bench, the factor of safety was computed to be 1.56. The same profile with an 11 foot clay layer, resulted in a factor of safety of 1.15.

The minimum factor of safety for a 2:1 dike consisting of sandy loess constructed on the clay profile with a 15 foot bench was found to be 1.07.

The above analysis was primarily directed at a deep failure circle which moves large masses of soil on long failure arcs.

The stability of the dikes on 2:1 slopes has been studied. It was determined that the minimum factor of safety for loess dikes with $\phi = 26^{\circ}$ and

c = 100 psf was 1.60. The minimum factor of safety with $\phi = 10^{\circ}$ and c = 500 psf was computed to be 2.23.

-6-

Affect of Clay Seams on Slope Stability

In analyzing the data from the slope stability programs, it can be seen that the presence of subsurface clay seams can decrease the stability of the dike slopes. The shear strength of samples tested indicate that the undrained shear strength is 300 to 500 psf.

Taking into consideration the deposition process in an alluvial valley, it is to be anticipated that the clay found in some of the borings are plugs. These clay plugs can be bridged by the width of the dike base and not adversely affect the stability of the slopes.

By controlling the placement rate of the fill, the pore pressure in the clay can be reduced and the shear strength of the clay increased.

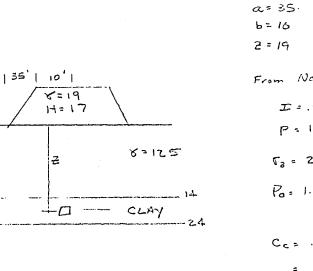
Conclusions:

- The stability of 2:1 dikes made from loessial type soils has an adequate factor of safety against shallow (slope) failure circles.
- Providing a minimum bench of 15 feet between the toe of the dike and the top of the river bank increases the factor of safety of the slope.
- The factor most incluencing the factor of safety is the presence of compressible clay seams.

By controlling the rate of fill, the possibility of a slope failure due to increased pore pressures is reduced. The dikes should be constructed in a manner such that all portions of the dikes are about the same height.

Settlement Considerations

For normally loaded clays, the settlement due to an increased load can be predicted based on the Compression Index $-C'_c$ (Terzaghi and Peck - Article 13).



$$-7- January 26, 1977$$

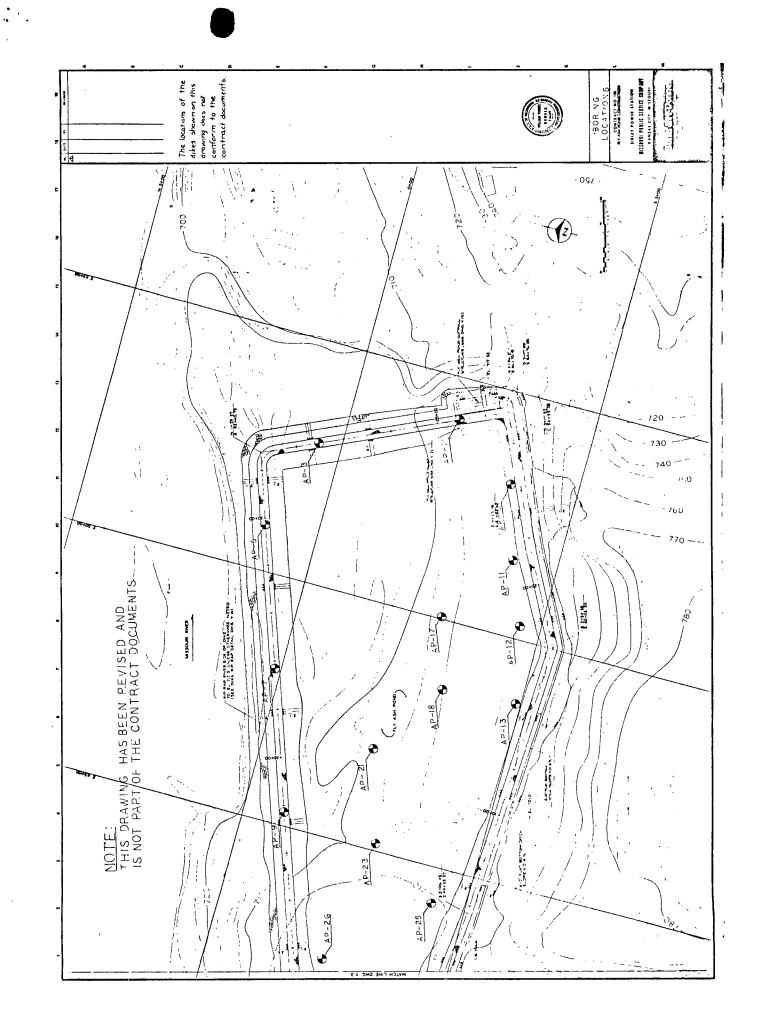
$$a = 35. A_{e} = 1.8 B_{3} = .52 Z = 19 B_{3} = .52 Z = 19 B_{3} = .52 Z = 19 B_{3} = .52 B_{3} = .52 B_{3} = .70 $

S= H Cc log. B+ AP I+es log. Po 5 = 10 432 log 1.72 1.98 log 1.02 = , 53 feet = 6 inches

Possible settlement of the dike is 6 inches and will occur at unpredictable locations due to the nature of the deposits.

e= . 98

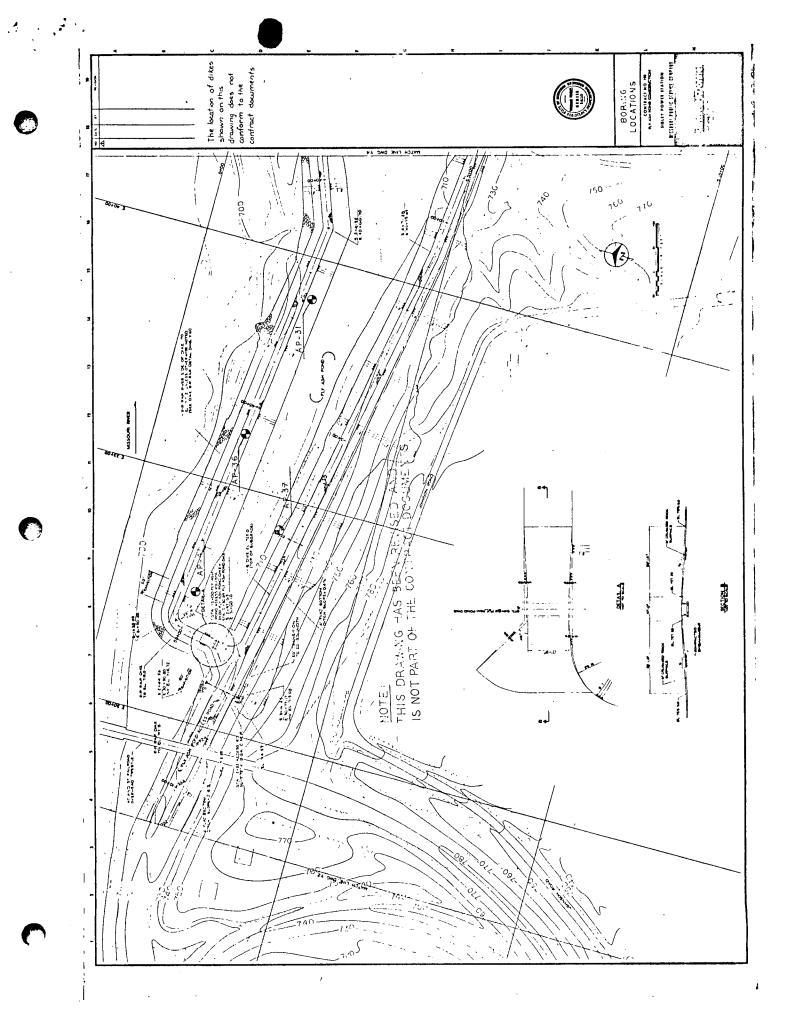
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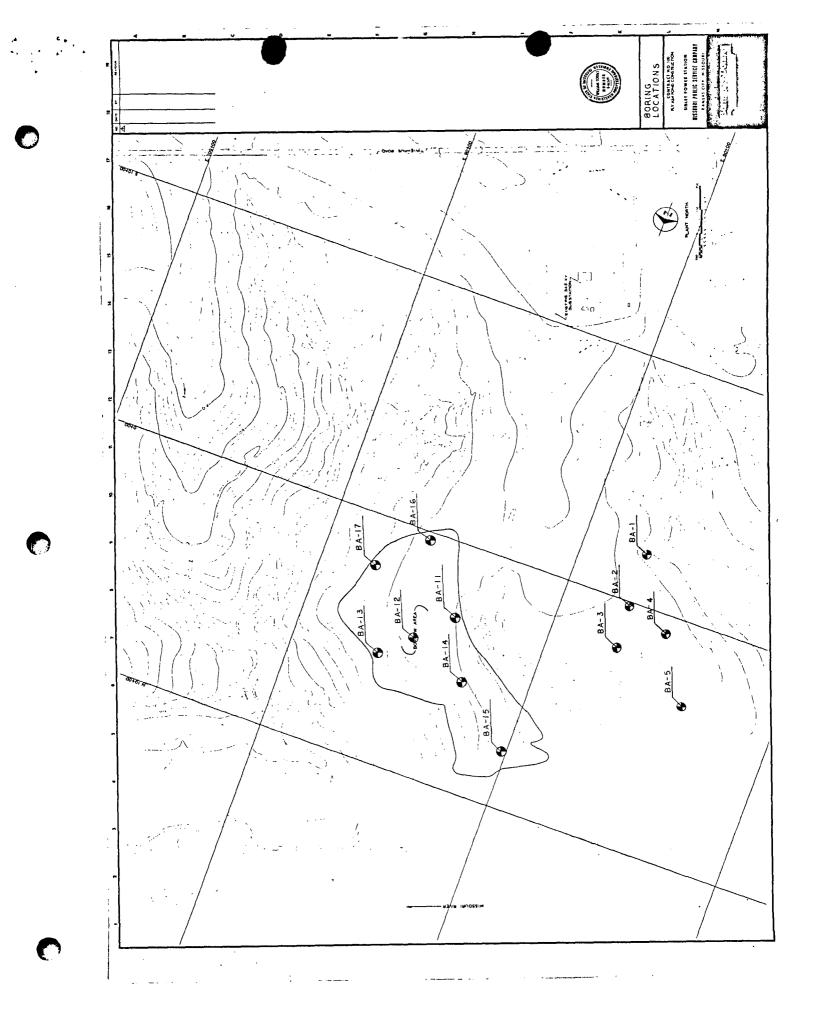


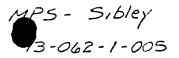
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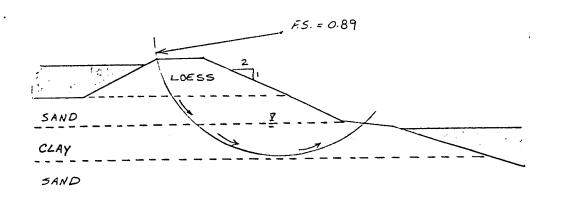




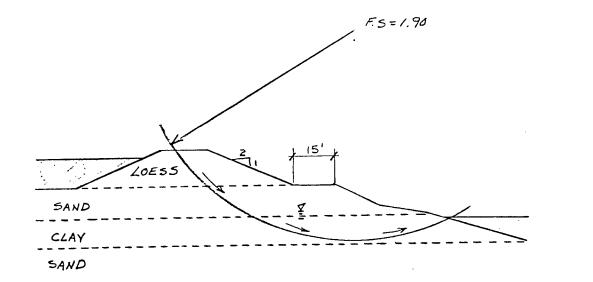


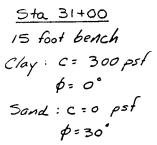
JAN 73, 1977

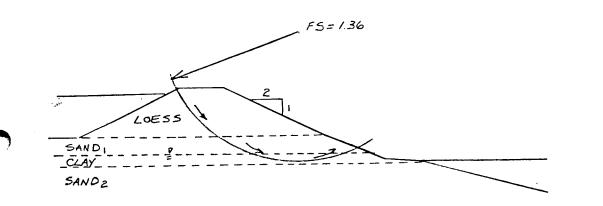
Summary of dike analysis



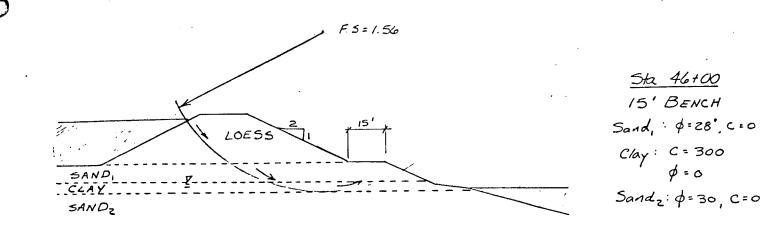
<u>Sta 31+00</u> No BENCH Clay: C: 300 psf \$ 0° Sand: C = 0 psf \$ = 30°



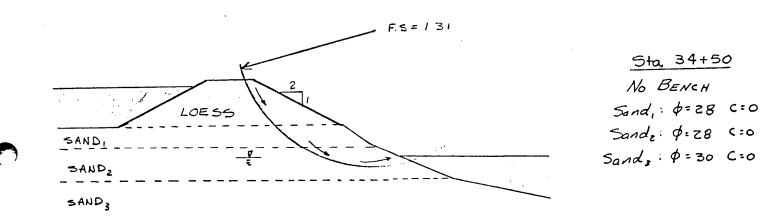


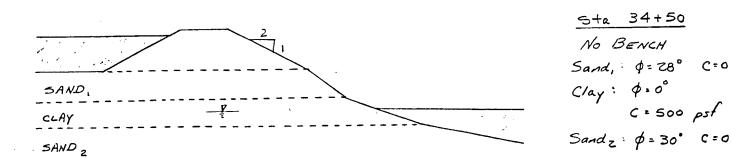


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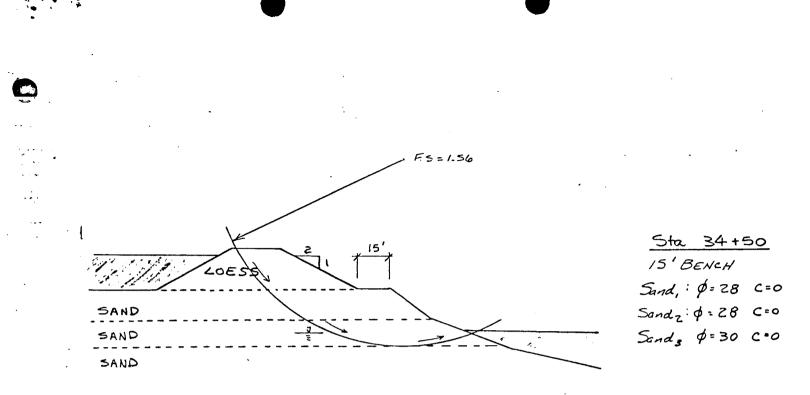




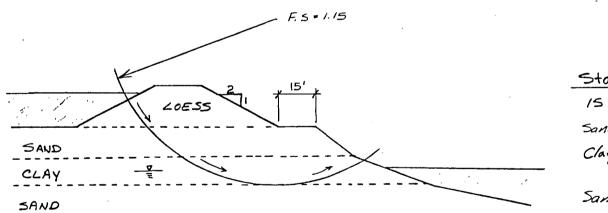
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15' BENCH
5and, : \$=28 C=0
Clay: C=500pst
φ=0
Sand: \$= 30° c=c

3

Breach Impact Analysis: Sibley Generating Plant Ash Settling Ponds

Facility Description

There are two ponds at the KCP&L Company Greater Missouri Operations Sibley Generating Plant that receive coal combustion products. One is small, about 500 cubic yards and settles out slag. The other settles out fly ash and is about 361,000 cubic yards in capacity. Since both ponds are routinely dredged, no solid material is permanently deposited in the ponds. The ponds contain varying levels of water depending upon rainfall and operations. Discharge from both ponds is regulated under the plant's NPDES permit.

Breach Scenarios

The ponds are located alongside the Missouri River. Any surface release would be contained on the property, which is bounded by low bluffs on three sides, or it would go to the Missouri River after traveling across the land between the ponds and river. Flow toward the bluff area would be against a rising terrain so would have negligible impact. Flow toward the river would result in water runoff of the released water that did not soak into the ground at the river and solids deposited on the river bank and into the river. Due to the cementious nature of the solid material in the ponds, the solid material is not expected to be flowable; it would simply slump toward the river. Some solid material would be carried by the water outflow by erosion of the surface of the solid material. For a release toward the river, a significant failure of the ground between the pond and river would have to occur. There appears to be little or no trigger to cause the magnitude of ground failure.

Even though a release is unlikely, an impact is calculated based on the total instant release of the full capacity of both ponds into the river with no residual left on land. The calculations are based on a lower river level of 15.6 feet at Kansas City against a flood stage at that station of 32 feet. The impact of a release to the river would be greatest at lower flows.

Impact Calculations

Total capacity of both ponds is 361,500 cubic yards. The length along the river of the combined ponds is approximately 2700 feet. River flow is taken as 2 miles per hour with a flow rate of 74,884 cubic feet per second. The surface area of the river along the ponds scales to be approximately 675,000 square feet.

Total pond Capacity \div surface area of adjoining river = rise in river due to sudden total release.

 $(361,500 \text{ cubic yards x } 27) \div 675,000 \text{ square feet} = 14.46 \text{ feet increase in depth}$. This would not put the river into flood stage along the plant and the effect would rapidly dissipate.

The result of a total release would be a momentary rise in the river. The amount of the rise in river would be dependent on the level of the river at the time, the flow rate, and the speed of release. The north side of the river across from the ponds is a low marshy area which would absorb any wave action from the release while most of the surge would simply spread out up and down the river. At higher river levels the impact would create a much lower rise in the river because of the resulting higher river flow volumes and wider expanse of the river into low areas across from the plant which would dilute the impact of the release because of the greater volume of water in the river and much greater surface area of the river at higher levels. While seemingly counter intuitive, the higher the river level, the

lower the impact of any release. The aerial photo of the river, with the plant outlined, shows the river at high level. The old channel marshy area north of the river is covered showing the river over twice as wide adjacent to the plant than it was for the calculations.

The impact to the river would be a layer of inert ash along the bank and an addition of water to the river which would be absorbed quickly. No environmental damage or property damage should result. The area south of the river is occupied by the plant which is surrounded by bluffs, so any rise would be contained in the plant. The area north of the river is mostly fields, as the attached aerial shows.

There is no known scenario that could result in the immediate release of all the material. Much of the solids would not flow and remain in the plant area. The ponds are routinely dredged so the amount of material available for release would be much lower than the calculated case.

MISSOURI PUBLIC SERVICE COMPANY

KANSAS CITY, MISSOURI

SIBLEY POWER STATION, SIBLEY, MISSOURI

SUBSURFACE INFORMATION (BOOK NO. 1) (FLY ASH POND AND BORROW AREA)

NOTICE

THERE IS NO EXPRESS OR IMPLIED GUARANTEE AS TO THE ACCURACY OR COMPLETENESS OF THE INFORMATION AND DATA CONTAINED IN THIS DOCUMENT, NOR OF THE INTERPRE-TATION THEREOF BY MISSOURI PUBLIC SERVICE COMPANY, THE BURNS & McDONNELL ENGINEERING COMPANY, KANSAS CITY, MISSOURI, OR ANY OF THEIR REPRESENTATIVES.

THE SUBSURFACE INFORMATION AND DATA CONTAINED HEREIN DO NOT FORM A PART OF ANY CONTRACT DOCUMENT ISSUED BY THE MISSOURI PUBLIC SERVICE COMPANY.

> Burns & McDonnell Engineers - Architects - Consultants KANSAS CITY, MISSOURI 1977 73-062-1-005

Date

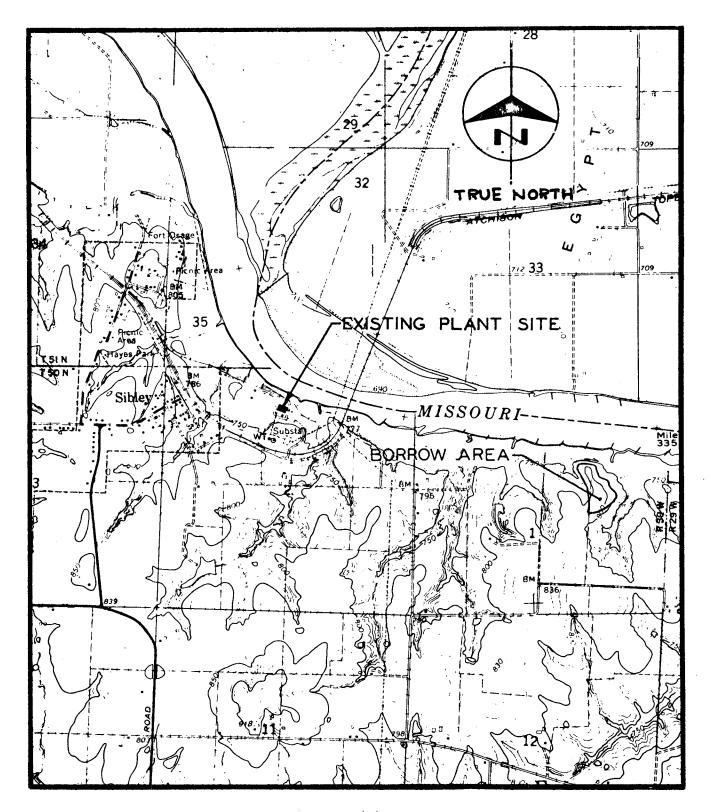
Burns & McDonnell Engineering Company P.O. Box 173 Kansas City, Missouri 64141

Re: Sibley Power Station Contract 100 Project: 73-062-1-005

The undersigned acknowledges receipt of the SUBSURFACE INFOR-MATION requested for the contract identified above and acknowledges that such SUBSURFACE INFORMATION must be returned to Burns & McDonnell to obtain refund of deposit on the Contract Documents.

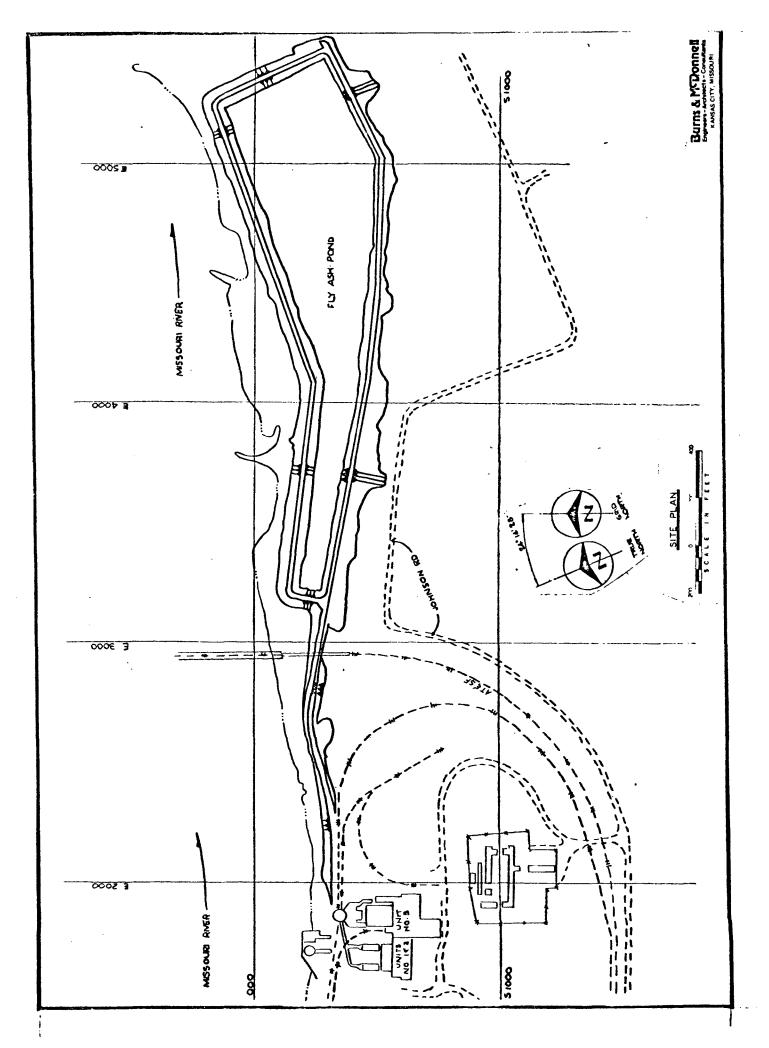
The undersigned further acknowledges and agrees there is no express or implied guarantee as to the accuracy or completeness of the information and data received, nor of the interpretation thereof by the Owner, Burns & McDonnell Engineering Company, or any of their representatives; and, the subsurface information and data received herein DO NOT form a part of any contract document issued by the Owner.

Company	 	
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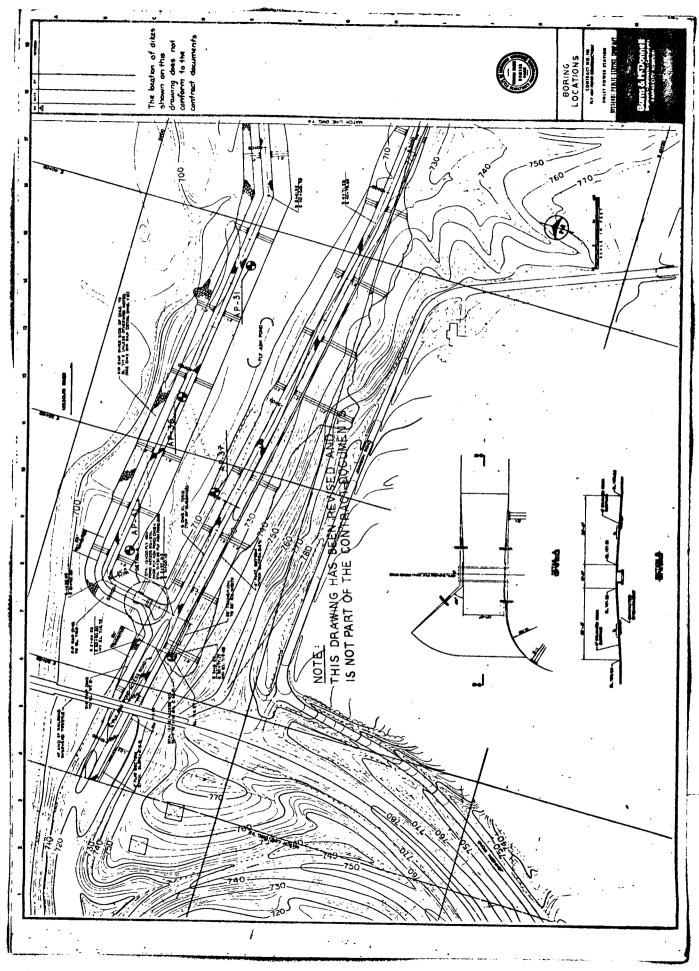


VICINITY MAP

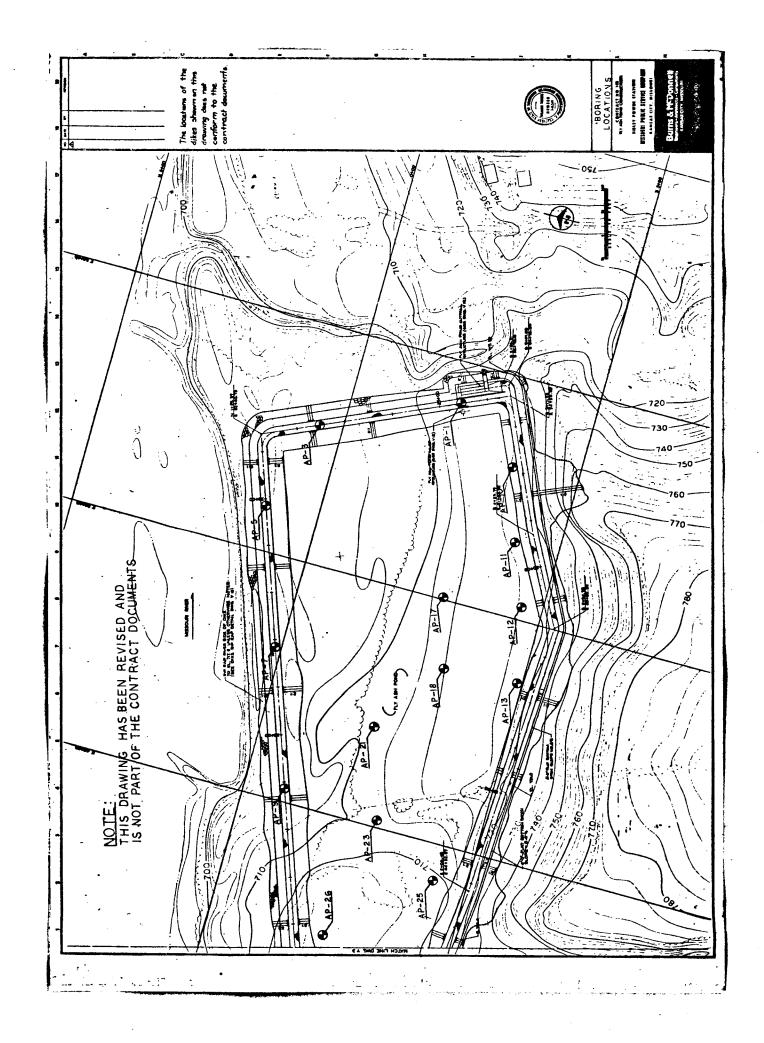


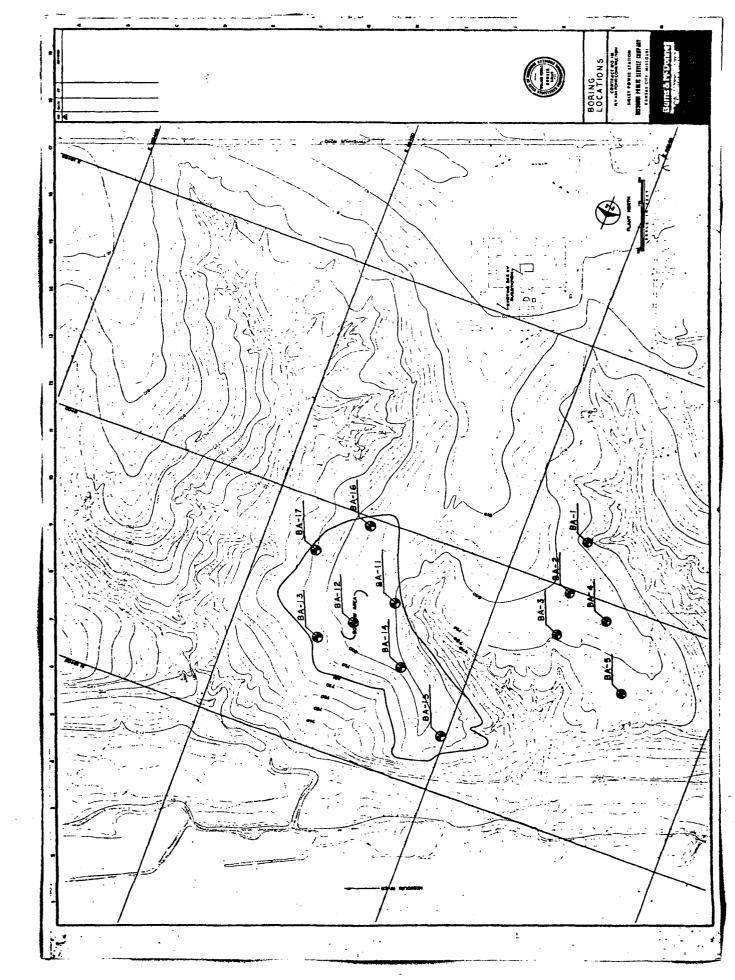


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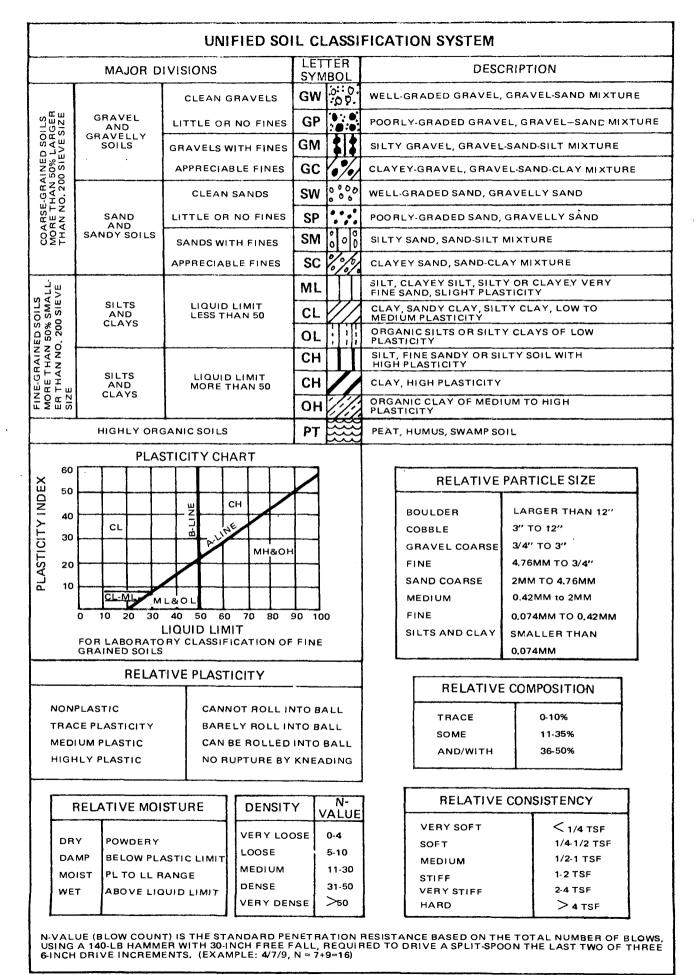
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BURNS & McDONNELL DRILLING LOGS

The material classifications and stratagraphic sequence presented herein reflect the observations of personnel present during drilling and sampling operations. The boring logs are based on <u>VISUAL</u> classifications and constitute only an opinion of the personnel making the observation. The Unified Soil Classification system is used for all soil descriptions.



JOB NO.	73-062-1-005	PROJECT.	1PS Ash Pon	d				. Hole	NO. AP-	1		
GROUND	ELEV	LOCATION N							т			
DRILLI TYPE	NG HOLE	Overburden Footage	Bedrock Footage	Övere	DURDEN		Core xes	4	% Core Ecovery	WATER TABLE		
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DRILLING	_{s Co.} Layne We	stern		DRHLLER(S). Jack Highley								
DRILLING	CME-55			Penetr	ation T	EST						
DRILLING	12/76			INSPEC	TOR(S).	Jo	hn Z	Zey				
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Burns & Moonnell

Form]-2-1-1A

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Jos No. 73-062-1-005 MES Ash Pond. HOLEN AP-3. Description 53:000 Ns. 48280 E Superior Signed State	n yn synadd y ffiliai yn yfar al rywladai y f		n a de la companya d I		a a fa she fa she ka a she ka a she ka s	LUU	والألادية بالجريدين	مي م			
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DRILLING COLayne.Western	DRILLING	HOLE									
DRILLING RIG	Auger	20.0	20.0	0		4					Dry
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DEFTM DESCRIPTION OR RECOV SAMPLE REMARKS 0 CLASS BLOWS & LOSS NO. NO. NO. 2 Sillty sand, medium dense, nonplastic, damp, light brown 0 0 - - 6	DRILLING DAT	τ <u>ε 12/76</u>			INSPEC	TOR (S)	John	Zey	<u></u>		
2 Silty sand, medium dense, nonplastic, damp, light brown 4 6 8 10 10 12 Silty clay, medium stiff, medium plasticity, wet, blue gray, trace of sand 16 18 20 20		Desc	RIPTION		OR		RECOV.		SAMPLE	Remarks	
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		D	RILLIN	l G	LOG							
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DRILLING	CoLayne.Wes	tern		DRILLE	R(S)	Jack	High	ley				
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122673			Burns & P Engineers-Archite	Consultant	!		_	-		Form J-2-1-1A		

с.

AP-7 PROJECT. MPS Ash Pond Јов No. 73-062-1-005 LOCATION. 53165 N. 47832 E 1 1 SHEET . 0 F DRILLING Ησιε OVERBURDEN BEDROCK OVERBURDEN NO. CORE % CORE WATER DEPTH FOOTAGE BOXES RECOVERY TABLE SAMPLES TYPE FOOTAGE 17'? 0 4 20.0 ---------Auger 20.0 DRILLER(S) Jack Highley DRILLING CO. Layne Western PENETRATION TEST. SPT DRILLING RIG. CME-55 John Zey DRILLING DATE 12/76 INSPECTOR(S) ... Log CORE Box or DEPTH DESCRIPTION NO. REMARKS OR RECOV. SAMPLE CLASS BLOWS & Loss NO. 0 ٠ Sand, poorly graded, medium 2 dense, medium grained, damp, light brown 4 6" 5-SS-1 6 8 Same - moist 10" 10 ss-2 10 12 14 15 S-3 8" 16. Same - wet, higher silt Hole caved content, gray 18 below 17' Same - saturated 7" 20 SS-4 20 Total Depth = 20.0'

DRILLING LOG

DRILLING LOG MPS Ash Pond AP-9 73-062-1-005 JOB NO. PROJECT HOLE NO. LOCATION. 53192 N. 47533 E 7.97..... SHEET GROUND ELEV ... DRILLING HOLE OVERBURDEN BEDROCK WATER OVERBURDEN NO. CORE % Core ΤΥΡΕ Depth FOOTAGE FOOTAGE SAMPLES BOXES RECOVERY TABLE 0 20.0 20.0 4 Dry Auger Jack Highley Layne Western DRILLING CO. .. DRILLER(S) ... DRILLING RIG. CME-55 PENETRATION TEST. DRILLING DATE 12/76 TO. John Zey INSPECTOR(S) BOX OR SAMPLE LOG CORE Depth DESCRIPTION NO. REMARKS RECOV. & Loss 0 R CLASS BLOWS 0 No. 2 Silty sand, medium dense, 4 nonplastic, damp, light brown, fine grained 5 1 6 8 10 _ 2 10 12 14 Silty clay, medium stiff, medium plasticity, moist, 15-3 blue gray, some sand 16 18 20_ 4 20 Total Depth = 20.0' 122673 Burns & MDonneil

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Form J-2-1-1A

.HOLE NO. AP-10 PROJECT. MPS Ash Pond JOB NO. 73-062-1-005 52,618 N; 48,133 E 1 1 716 LOCATION 0 F GROUND ELEV. SHEET No. Core Boxes % CORE DRILLING OVERBURDEN Overburden WATER HOLE BEDROCK RECOVERY TABLE DEPTH FOOTAGE SAMPLES TYPE FOOTAGE 13.0' 0 2 13.0' Dry____ Auger DRILLING CO. Layne Western DRILLER(S). Jack Highley DRILLING RIG. CME-55 PENETRATION TEST. SPT INSPECTOR(S) John Zey LOG CORE BOX OR DEPTH DESCRIPTION NO. RECOV. SAMPLE REMARKS 0 R· CLASS BLOWS & Loss No. 0 Silty clay, medium stiff, medium plasticity, moist, dark brown 2 Sandy silt, medium dense, 4 4 ---1 damp, light brown 6 8_ 2 8 Silty clay, medium stiff, medium plasticity, 10 moist brown 12 Broken rock 14 Auger refusal 16 Total Depth = 13.0' 18 20

DRILLING LOG

R sing Physics and collected and re-]
JOB NO.	73-062-1-005	PROJECT. ME	S Ash Pond	· · · · · · · · · · · ·			<u></u>	. HOLE	NO. AP-1	1
		LOCATION	2,640 N, 47	designed and the second					T <u>1</u>	
DRILLING Type	B HOLE Depth	Overburden Footage	Bedrock Footage		URDEN PLES		Core xes		% CORE ECOVERY	WATER Table
Auger	20.0	20.0	0	5						Dry
DRILLING C	co. Layne We	stern		DRILLE	r(s)	Jack	High	ley		
DRILLING R	_{Rig.} СМЕ-55			PENETR	ATION T	EST			16 48 49 49 49 49 48 48 48 48 48 48 48 48 48 48 48 48 48	
DRILLING D	DATE 12/76			INSPEC	TOR (5).	John	Zey	7 		
DEP TH	DESC	RIPTION	· · · · · · · · · · · · · · · · · · ·	LOG OR CLASS	No. B⊾o₩s	CORE RECOV. & LOSS		BOX OR SAMPLE NO.	Remarks	
2	Silty clay, medium plast trace of san	icity, mois					1	1		
4	Clayey silt,	moist, bro	own				3_	2	LL=37	PI=/2
6 1 1 8 1 8 1	Silty sand,	medium dens	se,							-
	low plastici brown						10	3		
	Same - gray,	, wet								
	Total Depth	20.0'					20	5		
122673			Rame & M				-			Form J-2-1-1A

r and a state of the day	ala serie a fait a f	D F	RILLIN	G	LOG		والبر فتتسوي			
JOB NO	73-062-1-005	Ркојест	PS Ash Pon	<u>d</u>		ø a 11 11 a 11 11 11		. HOLE	NO. AP	-12
GROUND E	LEV	LOCATION	2,661 N, 4	7,836	E			. Ѕнее	τ. <u>1</u>	of1
DRILLIN Type	NG HOLE Depth	Overburden Footage	Bedrock Footage		URDEN		CORE		CORE COVERY	WATER Table
Auger	20.0	20.0	0	4						Dry
DRILLING	co. Layne Wes	tern		DRILLE	r(s)	Jack	Hig	hley		
DRILLING	RIGCME-55			PENETR	ATION T	EST			••••••••••••••••••••••••••••••••••••••	*********
DRILLING	DATE. 12/76			INSPEC	TOR (\$)	John	Zey			
DEP TH	Desc	RIPTION		LOG OR CLASS	NO. BLOWS	CORE RECOV. & LOSS		BOX OR SAMPLE	REMARKS	
0	Clayey silt,	moist, dk.	brown		020#3	a LUSS		NO.		
2		and Arith Charles and an ann an Arith Charles and Arith Charles and Arith Charles and Arith Charles and Arith C	<u></u>	$\left \cdot \right \cdot \left \cdot \right $			1 1 1			
4 6 8 10 12	Silty sand, non plastic, fine to medd Silty clay, plasticity, sand	damp, brow um grained medium stil	7m, Ef, low				5 	1		
14				• • •			15-	3		
	Sandy clay, plasticity, fine grained Total Depth	moist brown d		00000			20	4		
122673			Borns & M				[1		Form J-2-1-1A

şinan yara talaşı yara birdi		DI	RILLIN	G	LOG						
JOB NO.	73-062-1-005	PROJECT. MP	S Ash Pond	***		17 19 29 10 10 10 10 10 10		. HOLE	AP-13		
GROUND	ELEV. 717	LOCATION. 52	,682 N, 47	,687 I	2			Ѕнее	т <u>1</u>	. OF	
DRILLI Type		Overburden Footage	Bedrock Footage		DURDEN		Core xes		% CORE ECOVERY	WATER Table	
Auge	20.Q	20.0	<u>0</u>		<u>+</u>				Dry		
DRILLING	_{g Co.} Layne Wes	tern		DRILLE	R(S)	lack H	igh1	ey	18 19 19 18 18 18 18 18 18		
DRILLING	_{g Rig} CME-55		14 17 19 19 19 19 19 19 19 19 19 19 19 19 19	PENETR	ATION T	EST		14 es se se +2 14 se se			
DRILLING	g date 12/76			INSPEC	TOR(S).	John	Zey	7 			
Dер тн 0	Desc	RIPTION	· ·	LOG OR CLASS	NO. Blowis	CORE RECOV. & LOSS		BOX OR SAMPLE NO.	Remark	s	
	Silty sand, moist light		se,				111				
2 -							-				
4 -	Clayey sand	, medium de	nse,								
	medium plas						5	1	LL= 30	, PI=18	
6 -											
8 -				·			-				
- -	Silty clay, to high pla										
10 -	brown						10 -	2			
- - 12 -							-				
12 -							-				
14 -		1						2			
	Silty clay, medium plas						15	3			
16 - -	brown						-				
18 -											
-				1				,			
20 -	Total Depth	$= 20.0^{\circ}$					20	4			
	ICTUI DEPTH										
							-				
										:	
22673	· · · · · · · · · · · · · · · · · · ·			L	L	L	1	1	L	Form 1-2-1-1A	

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JOB NO. 73	-062-1-005	PROJECT. MP	S Ash Pond	·····				. HOLE	NO. AP-1	.7	
GROUND ELEV	713	LOCATION	. <u>811 N. 4</u> 7	. 858 1	5		u 	". SHEE	т1	of 1	
DRILLING Type	Ноце Дерти	Overburden Footage	BEDROCK Footage		DURDEN	1	Core xes		% CORE ECOVERY	WATER Table	
Auger	20.0	20.0	0		3					14 '	
DRILLING CO.	Layne Wes	tern		DRILLER(S). Jack Highley							
DRILLING RIG	₆ CME-55		PENETRATION TEST.								
DRILLING DA	τε. 12/76			. INSPEC	TOR(S).	John	Zey		ne ur ar në rë ir ir ar ar et e	* * * * * * * * * * * * *	
Dep тн О	Desc	-	Log or Class	NO. Blows	CORE RECOV. & LOSS		BOX OR SAMPLE NO.	Remarks			
2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Clayey sand medium plas brown, very	tic, moist,					5	1	LL= 90 PI= 70		
10	Silty sand, medium plas brown, fine	ticity, wet					10	2			
	Silty clay, medium plas						15 <u>-</u>	3			
	Sand, silty medium to c brown Total Depth	oarse grain									
<u>ווווווו</u>											

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JOB NO	73-0	62-1-005	MPS	S Ash Pond		LUG				AP	-18
			PROJECT	821 N / 7	710 17			• • • •		1	1
DRILLI	NG	714	Overburden	831 N. 47.	OVERE	URDEN	No.	CORE	%	CORE	OF
TYPE Auge		Dертн 20.0	F00TAGE 20.0	FOOTAGE O	SAMI	PLES 4	Bo	X E S	RE	COVERY	TABLE Dry
					••••••			ъ и	<u></u>		
			SLEIN		DRILLE	R (S)			Lentey		*****
DRILLING	G RIG	CME-55									** ** ** ** ** ** ** ** ** **
DRILLING	G DATE	12/76	TO	• •• •• •• •• •• •• •• •• •• •• •• •• •		TOR (S).	John	Zey		*******	
Dертн О		DESC	RIPTION		Log or Class	NO. Blows	CORE RECOV. & LOSS		BOX OR Sample NO.	REMARKS	
2								11111			
4	med		medium sti: icity, mois sand				-	5 1	1		
8 -											
	med	ium plast	medium sti: icity, mois trace of s	st,				10	2 3		·
18 - 20 -	wet		medium den: ray, very	se,				20	4		
	Tot	al Depth	20.0'								
22673				Barns & M Engineer-Archite	Donnell						Form]-2-1-1A

DRILLING LOG HOLE NO. AP-21 JOB NO. 73-062-1-005 PROJECT. MPS Ash Pond 1 LOCATION 53,000 N, 47,585 E GROUND ELEV. 711 Sheet 0 F DRILLING NO. CORE % CORE WATER HOLE OVERBURDEN BEDROCK OVERBURDEN Boxes RECOVERY TABLE SAMPLES TYPE Dεртн FOOTAGE FOOTAGE 0 20.0 4 20.0 Dry Auger DRILLER(S) Jack Highley DRILLING CO. Layne Western DRILLING RIG. CME-55 PENETRATION TEST. INSPECTOR(S) John Zey DRILLING DATE. 12/76 TO. LOG CORE BOX OR **DEP TH** DESCRIPTION NO. RECOV. SAMPLE REMARKS 0R CLASS BLOWS & Loss 0 NO. Sandy silt, medium dense, low plasticity, moist, 2 light brown Silty sand, medium dense, 4 low plasticity, moist, light 5 – 1 brown, very fine grained 6 8 Silty clay, medium stiff, medium plasticity, moist, 10-2 brown, some sand 10 12 Same - blue gray trace of sand 14 15-3 16. Silty sand, medium dense, 18 low plasticity, wet, blue gray 20 4 20 Total Depth = 20.0

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Barns & McDonnell

		DF	RILLIN	G		L <u>0</u> G	a sala siyi ka matanga				
Јов No	73-062-1-005	PROJECT.	MPS Ash P	ond		•	uf ag as yp et as ag a		. HOLE	AP-2	23
GROUND ELE	711 *	N Location	53,005, E	47	,44	48			. Sheet	1	of1
Drilling Type		Overburden Footage	BEDROCK FOOTAGE			URDEN		CORE XES	%	CORE	WATER TABLE
Auger	20.0	20.0	0			4				 	Dry
DRILLING C	_{co.} Layne We	stern	** # 15 *\$ \$\$ ** ** ** ** ** ** ** **	DRI	LLE	R(S),	Jack	High	ley	****	
	Rig. СМЕ-55										
	DATE 12/20/76	то. 1	2/20/76	INS	PEC	TOR(S).	с.А.	Buł	1 r		
Depth		RIPTION		L C 0		NO.	CORE Recov.		BOX OR SAMPLE	REMARKS	
					155	BLOWS	& Loss		NO.		
2		·									
4											
4 _											
	Light brown	clayey silt	, some					5	1		
6 -	fine sand, m soft, low dr	oist, low p									
-	5010, 10w di	y strength									
8								-			
10								10-	2		
12						ļ					
14 _	0	- 11	fino	Π	Π						
-	Gray clayey sand, moist	to wet, low	v plasticit	У				15	3		
	Gray silty o	lay, moist	to wet,	$ \ge $	Ľ	<u> </u>	<u> </u>	-=			
18	-stiff, with			Ī	ĪĪ	 	<u> </u>	-	<u> </u>		
	Gray sand si wet to satur		of clay,	. .	$\left \cdot \right $						-
20				ŀ.	•	4		20_	4		
	Total Depth =	= 20.0 ^t				1					
-											
							1			r.	
					-	<u> </u>	<u> </u>]		Form J-2-1-1A
122673			Burns & M	Dor	nei	1					COTT J-2-1-1A

		DI	RILLIN	G		LOG					
Јов No. 73-	062-1-005	MP Project	'S Ash Pond	• •• •• ••	****				HOLE	A	P-25
GROUND ELEV		LOCATION. N			280)			SHEE	, <u>1</u>	. OF
DRILLING TYPE	HOLE Depth	Overburden Footage	BEDROCK Footage		VERB	URDEN PLES	1	Core xes	97	CORE	WATER TABLE
Auger	20.0	20.0	0			+		-			11.0
DRILLING CO	Layne Wes	tern		Dri	LLE	r(s)	Jack	Hig	ghley		
DRILLING RI	_{с. СМЕ-55}	* ** ** ** ** ** ** ** ** ** ** **		Pen	ETR	ATION T	EST			• •• •• •• •• •• •• •• ••	
DRILLING DA	τε. 12/76			INS	PEC	TOR(S).	C.A.	Buh	r		****
Depth	DESC	RIPTION		_ c	OG R ASS	NO. BLOWS	CORE RECOV. & LOSS		BOX OR Sample No.	Remarks	5
	Brown clayey sand, damp t plasticity								1		
	Brown silty sand, moist, plasticity	clay, traco, very stif	e of fine f, medium						2	LL=6 PI =4	- 1
	Brown sand s wet, medium			•••	•••				3		
	Light brown trace of co saturated, plasticity	arse sand,	wet to	•							
	Gray medium medium dens Total Depth	ity, wet to		•••••	••••				4		
122673			Barns & M					-			Form J-2-1-1A

الاجتبار الأكريب المراجع ورجعها			RILLIN	IG	LOG					and the part of	
Јов No7	d	•	14 eq es es as es es es		. Hole	HOLE NO. AP-26					
		E 47,	220	• • • • • • • • • • •		. Shee	. SHEET OF 1				
DRILLING TYPE	Hole Depth	Overburden Footage	Bedrock Footage	Overburden No. Core Samples Boxes			6 CORE COVERY	WATER Table			
Auger	20.0	20.0	0	4			14.0				
DRILLING CO	Layne Wes	tern		DRILLER(S). Jack Highley							
DRILLING RI	_{G.} CME-55			PENETR	ATION T	EST		** ** ** ** ** ** **			
DRILLING DATE 12/76 TO.					INSPECTOR(S). C.A. Buhr						
DEPTH						CORE RECOV. & LOSS		BOX OR SAMPLE NO.	REMARKS		
	Brown clayey moist, firm,						-				
2	Brown silty moist, hard, plasticity	clay, trace	of sand,								
4	Gray-brown c of fine sand plasticity,	, very stil	ff, medium						LL: 77 PI =51		
8 10	Gray, sandy moist to wet	silt, some , firm	clay,								
16 18 20	Gray sandy s wet to moist low plastici with gray si Total Depth	ty Ity clay so	dium to				20	4			
2673										Form J-2-1-1.	

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	and a second						-			}		
JOB NO. 73-	062-1-005	PROJECT. ME	PS Ash Pond	<u></u>				. HOLE	NO. AP	-31		
and a second										OF1		
DRILLING TYPE	HOLE Depth	Overburden Footage	Bedrock Footage	OVERBURDEN NO. COR Samples Boxes				E % CORE Recovery		WATER TABLE		
Auger	20.0	20.0	0	4 12.75								
DRILLING CO.	DRILLING CO Layne. Western					DRILLER(S). Jack Highley						
DRILLING RIG	. CME-55			PENETRATION TEST. SPT								
DRILLING DAT	ΓE	,TO,		INSPECTOR(S) John Zey								
DEPTH DESCRIPTION O				LOG OR CLASS	NO. Blows	CORE RECOV. & LOSS		BOX OR Sample No.	REMARKS	5		
	Silty sand, non plastic,			•								
4	Same - wet,	gray			⁸ 15/4	18°	5	SS-1	-	-		
	Same - damp,	, brown				12"		ST-2		2.5 pi=2.6		
	Same - wet,	gray to bro	own	•••••			15	ST-3	Qp =	1		
		= 20.0"					20	ST-4				
122673			Barns & M					<u> </u>		Form J-2-1-1A		

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JOB NO.,	/3-062-1-005	.н					HOLE NO. AP-36				
GROUND E	ELEV706	3,463 N, 46	, 661	E	* =* =* == == == =* =		. SHEE	<u>† </u>	0F		
DRILLI Type		Overburden Footage	BEDROCK Footage		Overburden No. Core Samples Boxes			9 Ri	WATER TABLE		
Auge	er 20.0	20.0	0	4					15'		
				1							
DRILLING	_{co} Layne Wes	stern		DRILLE	r(s)	Jack	Hi	ghley			
DRILLING	RIG. CME-55			PENETRATION TEST. SPT							
DRILLING	DATE. 12/76			INSPECTOR(S) John Zey							
Depth	Desc	RIPTION		LOG OR	NO.	CORE Recov.		BOX OR SAMPLE	REMARKS	6	
0				CLASS	BLOWS	& Loss		No.			
	Sandy silty			H							
2 🗖	medium dense moist, light		LICILY,	H							
			and the second secon	###		-					
4 -											
-	Silty sand,					18"	5_	ST-1	Qp =		
6]	plastic, moi very fine gr		brown,	· . · .					12.25	PI=0	
4	very time gi	ailleu		; · : •			1				
8 -				<u> </u>							
Ē					1		-				
10				1/	2/2	0"		SS-2			
~ 1	Silty clay,			\square	2/2/2		^				
E	plasticity v of sand	vet, gray t	Lace	1/							
					1						
										·	
				h.m.	<u> </u>		<u> </u>		_	0.05	
1	Silty sand,						15-	ST-3	Qp = 20 =	2.25	
	plasticity, fine to med:								γ = ·	93 pcf	
-	TTHE LO MEG	tum grained		 			=	1			
18 🗖				· ` ·			=				
-								l			
20 _	Same	<u></u>		[. • .			20_	ST-4	Qp =	1.75	
-	Total Depth	$= 20.0^{1}$				}]	8=0	io pef	
						Ì	=	1	с., .		
· 1					Ţ		=	ł			
-] ·	{		
-							-	4			
-							-	1			
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Form J-2-1-1A

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JOB NO.	73-062-1-005	PROJECT. ME	S Ash Pond	***			** ** ** :	. Hole	NO AP-	37
GROUND E	GROUND ELEV. 709' LOCATION N 53,947, E						т 1	1		
DRILLI TYPE		Overburden Footage	BEDROCK Footage	OVER	VERBURDEN NO. CORE				% CORE ECOVERY	WATER Table
Auge	er 17.5	17.5	0	3						
DRILLING	_{G Co.} Layne We	estern		DRILLE	r(s)	Jack	: Hig	ghley		
DRILLING	_{с Rig} СМЕ-75	ak an m 44 at		PENETR	ATION T	EST			** ** ** ** ** ** ** ** ** **	
DRILLING	g date. 12/76		• • • • • • • • • • • • • • • • • • •	INSPECTOR(S). C.A. Buhr						
DEPTH	DEPTH DESCRIPTION				NO. Blows	CORE RECOV. & LOSS		BOX OR SAMPLE NO.	REMARKS	
2	Brown silty clay, trace of fine sand, moist, firm to stiff, medium plasticity									
4	Brown clayey silt, some sand, moist to wet, soft, medium plasticity									
6			ngandan oleh degelako kerenteka atalah kerenteka kerenteka kerenteka kerenteka kerenteka kerenteka kerenteka k				5	1		
8 _										
10	Gray sandy s clay, moist low plastic:	to wet, so					10	2		
12				•						
14 =										
								53		
18	Refusal at	17.5'					17			
								1		
122673		<u> </u>	Burns & M		L	1	<u> </u>	1	1	Form J-2-1-1A

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GROUND ELEV. DRILLING TYPE Auger DRILLING CO. DRILLING RIG DRILLING DAT DEPTH 0 2 2 3 4 5 5 6 6 7	filty sand,	LOCATION 53,6 OVERBURDEN FOOTAGE 20.0 Stern	30 N, 46,3 Bedrock Footage 0	10 E Overburi Sample 4 Driller(s Penetrati Inspector Log Or	DEN NO. S B)Jac.	Core oxes k Hig n Zey	SHEE		F 1 WATER TABLE Dry
DRILLING TYPE Auger DRILLING CO. DRILLING RIG DRILLING DAT DEPTH 0 2 2 3 4 3 5 4 5 0	носе DEPTH 20.0 	Overburden Footage 20.0 stern	BEDROCK FOOTAGE O	OVERBURI SAMPLE 4 DRILLER(S PENETRATI INSPECTOR LOG OR	DEN NO. S B Jac Jac Jac Joh Recov	CORE OXES k Hig n Zey	Re shley Box or SAMPLE	CORE COVERY	Water Table Dry
TYPE Auger DRILLING CO. DRILLING RIG DRILLING DAT DEPTH 0 2 2 3 4 3 5 4 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	DEPTH 20.0 Layne.We 5	Footage 20.0 stern	Footage O	SAMPLE 4 DRILLER(S PENETRATI INSPECTOR LOG OR	S B 	oxes k Hig n Zey	Re shley Box or SAMPLE	COVERY	TABLE Dry
DRILLING CO. DRILLING RIG DRILLING DAT DEPTH 0 2 2 3 4 5 5 6 6 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Layne We CME-55 12/76 Desc	stern		DRILLER (S PENETRATI INSPECTOR LOG OR	on Test (s)Joh No. Core Recov	n Zey	BOX OR SAMPLE		
DRILLING RIG DRILLING DAT DEPTH 0 2 2 3 4 5 5 6 6 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	5. <u>CME-55</u> <u>FE. 12/76</u> D E S C Silty sand, 5			PENETRATI INSPECTOR LOG OR	on Test (s)Joh No. Core Recov	n Zey	BOX OR SAMPLE		
DRILLING DAT	Desc		· · · · · · · · · · · · · · · · · · ·	INSPECTOR Log Or	(s) Joh No. Core Recov	n Zey	BOX OR SAMPLE		
Dep тн 0 2 - 2 - 5 4 - п	Desc Silty sand,			LOG OR	NO. RECOV		BOX OR SAMPLE	Remarks	
0 2 2 3 4 1 8 0 1 8	filty sand,	RIPTION		OR	NO. RECOV		SAMPLE	REMARKS	
s s s							110.		
6 - b	prown	medium dens damp, ligh				5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1		
m	Clayey sand, medium plast light brown					10	2		
	Silty clay, nedium to hi noist, blue Fotal Depth	.gh plastic: gray, some	ity,			20	4		

DRILLING LOG

		، معالم مقال کرد از این این کرد. ا		KILLIN		LUG					
JOB NO.	73-00	62-1-005	PROJECT	Borrow An	ea				HOLE	B	A-1
GROUND	ELEV		LOCATION						. SHEET	·1	of1
DRILLI	ING	HOLE DEPTH	Overburden Footage	BEDROCK Footage	Overe	URDEN	No. Box	CORE	%	CORE	WATER TABLE
4" Aug		.24.5	24.5			-	_	-			-
	L	Layne-We					Jack	Hig	hlev		
					DRILLE	R(S),,,,	4				
DRILLIN	G RIG	CME		•							
DRILLIN	G DATE.	12/16/76		* #* ** ** ** ** ** ** ** ** ** ** ** **	INSPEC	TOR(S).	John	Zey			
. Dep th		Desc	RIPTION		LOG OR CLASS	NO. Blows	CORE RECOV. & LOSS		BOX OR SAMPLE	REMARKS	
-		<u> </u>					a 2055		No.		
								=			
					V/			_			
5 -		wn clayey sand mois	silt with	trace	///			-		-	
		sanu mors	L		V//			-			
					V//.						
	•				\langle / \rangle			=			
	1				///						
10 =	1				///			111			
	<u> </u>	<u> </u>			¥//						
	4				///						
	1				\mathbb{V}/\mathbb{I}			11			
	1				V//			1			
15 -					\mathbb{V}/\mathbb{V}						
					///			-			
		wn silty sand very	clay with t moist	race	\langle / \rangle						
					V//	ļ					
20 _					///	1					
					V//	1					
						1					
-	1				1//	1					
		. _ ·	0/ 5			1					
25 -	1 Tot	al Depth	= 24.5			1					
									1		
	1	*** *			<u> </u>				1		
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	D	RILLIN	G	LOG	a a sua di sua	1. K. M. 1.		4	
JOB NO. 73-062-1-005	PROJECT. MPS	- Borrow A	Area		18 14 14 18 18 18 14 14 14	• •• •• •	. Hole	BA-	-2
GROUND ELEV	LOCATION						SHEE	r 1	of1
DRILLING HOLE TYPE DEPTH	Overburden Footage	BEDROCK Footage		URDEN PLES		Core xes		CORE COVERY	WATER Table
4" Auger 20	20		<u></u>			- <u></u>			
DRILLING CO Layne-	Western	• • • • • • • • • • • • • • • • •	DRILLE	a(s)	Jack	Hig	hley	•••••	
DRILLING RIG CME			PENETR	ATION T	EST				
DRILLING DATE 12/16/	76 _{то}	a # 10 10 co	INSPEC	TOR(S).	John	Zey	****		
ДЕРТН ДЕ	SCRIPTION		LOG OR CLASS	NO. BLOWS	CORE RECOV. & LOSS		BDX OR Sample No.	REMARKS	;
of sand mo	y clay with t								

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Form J-2-1-1A

						an a	-	, and a subscription of the subscription of th	BA-	3
JOB NO. 73	-062-1-005	PROJECT. MP	5 – Borrow	Area		18 at 10 at 10 in 14 a		. Hole	No	
	••••••	LOCATION	** ** ** ** ** ** ** ** ** ** ** **				and the second sec		т 1	DF
DRILLING TYPE	Hole Depth	Overburden Footage	Bedrock Footage		URDEN PLES		Core xes		6 CORE COVERY	WATER Table
4" Auger	20	20						<u></u>		
DRILLING CO	Layne-West	ern	** ** ** ** ** ** ** ** ** ** ** ** **	DRILLE	r(s)		Jack	Highl	ley	
DRILLING RI	GCME			PENETR	ATION T	EST			1 60 Fr 40 46 11 47 49 61 47 69	
DRILLING DA	_{τε} 12/16/76			. INSPEC	TOR(S).	Joł	n Z	ey		
Dep th	······································	RIPTION		Log or Class	NO. Blows	CORE RECOV. & LOSS		BOX OR Sample No.	REMARKS	
10 10 15 20	Frown clayey of sand moist Brown silty of sand very Fotal Depth =	t clay with t moist								

70	062-1-005	MPS				an di Gibio di			BA	-4
JOB NO. / 3-	062-1-005	PROJECT. PROJECT	- Borrow A	11 CA				HOLE	No. BA	
free and the second sec										OF
DRILLING Type	HOLE Depth	Overburden Footage	Bedrock Footage		URDEN PLES		CORE XES		6 CORE COVERY	WATER Table
4" Auger	20	20								
DRILLING CO.	Layne-West	tern		DRILLE	R(S)	Jack	High	ley	• • • • • • • • • • • •	
DRILLING RIC	_{G.} CME		• • • • • • • • • • • • • • • • • • • •	PENETR	ATION T	EST				
DRILLING DAT	те. 12/16/76.		• • • • • • • • • • • • • • • • • • •	INSPEC	TOR(S).	John	Zey			
Depth	DESC	RIPTION		LOG OR CLASS	NO. B∟ows	CORE RECOV. & LOSS		BOX OR SAMPLE NO.	REMARKS	
5 10 15 20	rown clayey f sand mois Grown clayey of sand very	silt with moist								

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			<u>AILLIN</u>		LUG				
Јов No. 73-0	062-1-005	PROJECT.	PS - Borrow	Area		*********	Hole	BA	-5
GROUND ELEV.		LOCATION				18 14 15 15 15 15 16 16 10 10 40 40	Shee	т 1	OF
DRILLING Type	HOLE Depth	Overburden Footage	Bedrock Footage		URDEN	No. Co Boxes		% Core ecovery	WATER Table
4" Auger	20	20						~-	
DRILLING CO.	Layne-West			DRILLE	r(s)	Jack H	ighley		
DRILLING RIC	G. CME			PENETR	ATION T	EST		** ** ** ** ** ** ** ** **	
DRILLING DAT	т <u>е. 12/16/76</u>			INSPEC	TOR(S).	John	Zey		
Depth	Desc	RIPTION		LOG OR CLASS	NO. Blows	CORE RECOV. & LOSS	BOX OR Sample NO.	REMARKS	
	Frown clayey of sand mois Fotal Depth	t	trace						Form 1-2-1-1A

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Paratana and			D	RILLIN	I G	LOG					
JOB NO.	73-	-062-1-005	PROJECT	MPS - Bor	row Ai	ea			.HOLE	NO	<u>-11</u>
GROUND	ELEV.	800	LOCATION						. Ѕнее	т <u>l</u>	of1
DRILLI		HOLE Depth	Overburden Footage	BEDROCK Footage		URDEN		Core xes		% Core ecovery	WATER Table
4" Aı	ıger	29	29		6) 		_			
DRILLIN	G Co.	. Layne-Wes	tern		DRILLE	r(s)	Jack	High	ley		
DRILLIN	G RIG	Tractor R	ig		PENETR	ATION T	EST			ee at 15 ee ee at 15 at as 1	
DRILLIN	G DAT	<u>. 1/77</u>			INSPEC	TOR (5) .	Patr	ick	Goeke		
D ερ τη		DESC	RIPTION		LOG OR CLASS	NO. Blows	CORE RECOV. & Loss		BOXOR SAMPLE NO.	Remarks	
5	(Brown silty dry to damp stiff							1		
5 1 1 1 1 1 1 1 1 1 1 1 1 1		Same moist,	medium st	lff					2 3		
15		Same - beco	ming very s	silty					4		×
		Brown claye moist, soft	y silt to medium	stiff		_			5	becomi to dri	ng easier 11
									6		
30		Total Depth	h = 29.0'								
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IOD NO	73-062-1-00	D PROJECT MPS	- Borrow	Area				Hour		A-12
			ويسترك مستعملين البرغيان والمراجع والمتعاونين	<u> </u>		ad eo os a, os os os os	e 14 25 1	a an ann an Anna an An		
DRILLIN		UCATION	BEDROCK		URDEN		CORE		т <u>і</u> % Core	OF 1 WATER
TYPE	G HOLE DEPTH	FOOTAGE	FOOTAGE		PLES		XES		CORE ECOVERY	TABLE
4" Aug	ger 29	29	0		5				4	
DRILLING	co. Layne-W	estern		DRILLE	R(S),	Iack H	igh	ley		
DRILLING	RIG. Tractor	Rig		PENETR	ATION T	EST				****
DRILLING	DATE. 1/77		*	INSPEC	TOR(S).	Patri	ck (Goeke		** ** ** ** ** ** ** **
Depth	Des		LOG OR CLASS	NO.	CORE Recov.		BOX OR SAMPLE, NO.	REMARKS		
	Dark brow	n silty clay		V				1		
	dry to da	mp, medium s	tiff							
5 -										
								2		
10		silty clay								
	dry, very	stiff						3		
15								4		
		-								
		wn silty clay	ÿ					4		
20 =	moist, pl	astic								
	Becoming	very silty		F				- 5		
				H						
25 _				Ħ						
				Ħ	1			6		
30 =	Total Den	th = 29.0'								
	Teter pop									
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JOB NO.	73-0	062-1-005	PROJECT. MP	S - Borrow	Area				. Hole	NO. BA-	13	
GROUND E	Ξιεν.,		LOCATION	** ** ** ** ** ** ** ** ** ** ** **					. Shee	T 1	of1	
DRILLI Type		Ноге Depth	Overburden Footage	Bedrock Footage	OVERF	URDEN		Core xes		CORE	WATER Table	
4" Au	ger	29	29	0	(5		-				
DRILLING	G Co.	Layne-We	stern	10 18 10 10 10 10 10 10 10 10 10 10 10 10 10	DRILLE	r(s)	Jack	Hig	ghley			'
Drilling	RIG,	Tractor R	ig	** ** 19 ** ** ** ** ** ** ** ** ** **	PENETR	ATION T	EST,			****		
DRILLING	DATE		TO	· · · · · · · · · · · · · · · · ·	INSPEC	TOR(S).	Patr	ick	Goeke			
D ер тн		Desc	RIPTION		Log or Class	NO. Blows	CORE RECOV. & LOSS		BOX OR Sample No.	Remarks		
	De	d brown of	1+		\square							
		ed brown si amp, medium							1			
-												
5 -												
	S .	ame - light	brown					-			 	
	36	ime – itgur	DIOWII						2			
10 =								-				
	Li	ight brown	silty clay					-				
-		amp, medium							3			
-								-				
15 _	be	ecoming ver	y silty									
								_	4			
-								-				
20 _	6				T			-				
	29	ame			H4			-				
					Ħ			-	5			
25					H							
	L	ight brown oist, mediu	very silty	clay	H			-				
	ш	orse, mealt	W SLILL		IH			-	6			
					HH							
30	T	otal Depth	= 29.0'					_				
										- - 		
								-				
122673								-	1	<u>_</u>	Form J-2-	

Burns & McDonnell Engineers-Architects-Consultants Form J-2-1-1A

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	72 062 1 005		RILLI.						NO. BA-	14
	73-062-1-005	PROJECT. MPS				· ·		•		
GROUND E DRILLIN TYPE 4" Au	DEPTH	Location, Overburden Footage 29	Bedrock Footage O	Overe Sami	URDEN PLES	NO.	CORE	%	CORE COVERY	WATER TABLE
	co. Layne-Wes	tern		DRILLE	R(S)	Jack	Higl	ley		
DRILLING	RIG. Tractor R	lig		PENETR	ATION T	EST				
DRILLING	DATE 1/77) al ad ab ab ac	. INSPEC	TOR(S).	Patri	ck (Goeke		
D ер тн	Desc	RIPTION		Log or Class	NO. Blows	CORE RECOV. & LOSS		BOX OR Sample No.	REMARKS	
	Dod brown of							1		
10	Red brown si	LILY CIAY						2	-	
- - - - - - - - - - - - - - - - - - -	Light brown damp medium							3		
11111	becoming mo:	ist, plasti	c					4		
	Same							5		
25	Light brown moist, medi	um to soft,						6		
30	Total Depth	- 23.0								

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JOB NO.	73-0	62-1-005	PROJECT.	°S - Borrov	/ Area				HOLE	No. B	A-15
	LEV	7001	LOCATION							1	0F
DRILLI TYPE	NG	Hole Depth	OVERBURDEN Footage	BEDROCK FOOTAGE	OVERE	URDEN	No.	CORE	%	CORE	WATER TABLE
4" Au	iger	29	29	0		6					
RILLING	6 Co. L	ayne-West	ern		DRILLE	R(S)	Jack	Higl	nley	* * * * * * * * * * *	
	RIG. T	ractor									
					†		Patri				
DEPTH			RIPTION	an as as ak his as as as as as as an array ar	LOG OR CLASS	NO. BLOWS	Core Recov.		BOX OR SAMPLE	REMARKS	
				·····		BC0#3	& Loss		NO.		
					1/			-	1		
					1			-			
5 -		brown si			1			-			
Ę	dam	p, medium	STIII					-			
								-	2		
10 -								-			
-								· -			
									3		
15 =											
10 <u>-</u>								-			
									4		
4			silty clay					-			
20 _		y to damp y stiff						-			
						4		-	5		
						1		-			
25 _					1]		-			
								-	6		
30 -	Tot	al Depth	= 29.0"	-							
	100	~-r on									

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		D	RILLIN	IG I	LOG				National and a state of the state	
Јов No. 73	-062-1-005	PROJECT	1PS - Borro	w Area	l <u></u>	1 f 1 11 11 11 11 11 11	14 14 1	. HOLE	NO. BA-	16
GROUND ELEV.	805±	LOCATION								оғ
DRILLING TYPE	HOLE Depth	Overburden Footage	Bedrock Footage		URDEN PLES	No. Box	CORE		CORE	WATER Table
4" Auger	29	29	0			 			******	
DRILLING CO.	Layne-Wes	stern		DRILLER	R(S)	Jack	Hig	hley	**	
DRILLING RIG	Tractor			PENETR	ATION T	EST		• •• •• •• •• •• ••	** ** ** ** ** ** ** ** **	
DRILLING DAT	re. 1/77			INSPEC	ror(s).	Patr	ick	Goeke		
DEPTH	Desc	RIPTION		Log or Class	NO. Blows	CORE RECOV. & LOSS		BOX OR SAMPLE NO.	Remarks	
-				1			-			
								1		
	Brown, silty	v clav						-		
	lamp, medium						4			
				\sim			=			
							Ξ	2		
							-			
				\square			Ξ			
							Ξ			
-							=	3		
15							-			
							-			
	Brown, silty	v clav					-	4		
I	noist, soft	to medium					-			
20										
							-	5		
25							-			
							-			
							1.1	6		
30	Total Depth	= 29.0'								
-							-			i
							_			
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DRILLING LOG

JOB NO.	73-062-1-005	PROJECT.	MPS - Borro	w Are	3	d 10 10 10 10 10 10 10 10	•••••	. Hole	NoB	A-17
GROUND E	LEV. 790±	LOCATION						. Sheet	T <u>1</u>	of <u>1</u>
DRILLIN TYPE	NG HOLE Depth	Overburden Footage	Bedrock Footage		BURDEN PLES	No. Box			CORE COVERY	WATER Table
4" Aug	er 29	29	0		6					
DRILLING	co. Layne-Wes	tem		DRILLE	r(s)	Jack I	ligh	ley		
DRILLING	Rig Tractor.			PENETR	ATION T	EST	_ <u>_</u>			
DRILLING	DATE 1/77		· · · · · · · · · · · · · · · · · · ·	INSPEC	TOR(S).	Patri	ck (oeke		
DEP TH	DESC	RIPTION		LOG OR CLASS	NO. BLowis	CORE RECOV. & LOSS		BOX OR SAMPLE NO.	Remarks	
- - - - - - - - - - - - - - - 	Brown silty	clay						1		
	damp, medium						1111111111	2		
- - - - - - - - - - - - - - - - - - -								3		
20 -	Tan silty cl medium to so							4		
25	Becoming ve	ry silty						5		
								6		
30	Total Depth	= 29.0°								
F					<u> </u>			l,		Form]-2-1-1A

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Form J-2-1-1A

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LABORATORY TEST RESULTS

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Project _	1 1	MPS - Ash Pond								Project No.	73-062-1-005
Laboi	ory .	Layne-Western		ИМАНУ	SUMMARY UF SUIL IESIS	I ES I S		-		Date Janua	January 1977
BER ING		DEPTH ОВ	CLASSIFICATION	3 č	DRY UNIT	АТ	ATTERBERG LIMITS	U	UNCONFINED	-INED SSION	REMARKS
808 808	MA2 MUN	ELEVATION		8	PCF .	LL	۲	E	TSF	% Е	
AP 1	-	0 - 1.5	Brown silty clay (CL)			43	20	23			
AP 5	3 ST	15.0	Blue-gray silty clay (CH)	36.2	82.1	58	20	38	0.31	18.0	
AP 5	ST 4	20.0	Blue-gray silty clay (CH)	41.4	77.4	56	25	31	.030	16.3	
AP 1	5	2.5 - 4.0	Brown silty clay (CL)			37	25	12			
AP 13		5.0	Brown sandy clay (CL-SC)			36	18	18			
AP 17		5.0	Brown sandy clay (CH)			91	21	70			
050373				Barn	Burns & McDonnell						J-1-2-1

Proie	Project MPS	5 - Ash Pond	pt							0	D*************************************	-062-1-005
Labo	Laboratory	Layne-Western		MMARY	SUMMARY OF SOIL TESTS	. TESTS				ĽŐ	Date January	-002-1-000 ry 1977
RING BING	мвев Мвев	DEPTH OR	CLASSIFICATION	∧ %	DRY UNIT WT	AT	ATTERBERG LIMITS	U	UNCONFINED	FINED		REMARKS
NN 08	IA2 UN	ELEVATION		2	PCF	Ŀ	ΡĽ	Id	TSF	ш %	· · · · · · · · · · · · · · · · · · ·	
AP 23	1	5.0	Light brown clayey silty (CL	(CII-ML)		34	24	10				
AP 25		5.0	Brown silty clay (CH)			66	23	43				
AP 26		5.0	Brown silty clay (CH)			77	26	51				
AP 31	ST 2	9.5 - 11.0	Brown silty sand (SM)			30	28	2				
AP 31	3 ST	14.5 - 16.0	0 Gray brown silty sand									
AP 31	ST 4	19.5 - 21.	.0 Gray brown silty sand	33.0	89.2		-					
050373				Burns Engineer	Burns & MCDonnell Engineer-Architects-Consultants		-	1	-		-	J-1-2-1

Proje	Project <u>MPS</u>	5 - Ash Pond Lavne-Western		MMARY	SUMMARY OF SOIL TESTS	TESTS				Proje Date	ct No. 7 <u>3</u> Janu	Project No. <u>73–062–1–005</u> Date January 1977
BER ING	BER PLE	DEPTH	CLASSIFICATION	3		AT	ATTERBERG LIMITS	U	UNCONFINED	INED SSION		REMARKS
ROR ROR	MA2 MUN	ELEVATION		%	PCF.	LL	Ъ	Ы	TSF	Е %		
AP 36	ST 1	4.5 - 6.0	0 Light brown silty sand (SM)			25	25	0				
AP 36	ST 3	14.5 - 16.0	.0 Silty sand	29.4	93.1				0.48	3.6		
AP 36	ST 4	19.5 - 21.	.0 Silty sand	30.4	0.06							
AP 37		5.0	Brown clayey silt			30	26	4				
050373				Burn	Burns & McDonnell	H						J-1-2-1

Burns & McDonnell Engineers-Architects-Consultants

Project _	tt MPS	I	Borrow Area								Droiact No.	73-062-1-005
Labo	۲	Layne-Western		UMMAR	SUMMARY OF SOIL TESTS	L TESTS	~			i ä	Date	January 1977
MBER RING	месе Мвев	DEPTH OR	CLASSIFICATION	≥ %	DRY UNIT	AT	ATTERBERG LIMITS	g	UNCONFINED COMPRESSION	Stor N N N N N	וג זכר	PERMEABLLITY CM/SEC
0N 80	iaz Un	ELEVATION		۹	PCF.	LL	ΒΓ	ā	TSF	ш %	Shea Dirre	
BA 1	1,2	0 - 10	CL			46	24	22				
BA 2	1,2 3,4	0 - 20	cL	22.3*	94.8 [*]	41	24	17				1.1 × 10 ⁻⁶
BA3 BA5	1,2,1,2		CL			40	23	17				
BA 4	1,2,3	0 - 15	ct	22.2*	94.6*	44	23	21		3	> >	3 x 10 ⁻⁷
								-				
BA-1 BA-3 BA-5	4,5 4 4		cı	21.7*	92.8*	37	23	14				5.5 x 10 ⁻⁶
050373				Burn: Engineers	Burns & MDonnell Engineers-Architecte-Consultants		-		* afte	r pern	after permeability test	y test J-1-2-1

Project _	ct MPS	S - Borrow Area		MMARY	SUMMARY OF SOIL TESTS	TESTS				Pr	Project No.	1	73-062-1-005
Labo	Laboratory _	KCTL						2		Ä	Date	Janua	January 1977
BER ING	. ยาย มาย	DEPTH	CLASSIFICATION	Χ.		AT	ATTERBERG LIMITS		UNCONFINED COMPRESSION	-INED SSION	5 Fi		PERMFABILITY CM/SEC
ROR	MAS MUN	ELEVATION		%	PCF	۲۲	٩L	Ы	TSF	ш %	> %		
BA-1 BA-3 BA-4	3 3		сг			38	24	14					
BA 11	2	5-10	CL			35	23	12					
BA 11	5	20-25	CI			39	22	17			18		
BA 12	1	0-5	cī			35	22	13					
BA 12	4	15-20	CL		92.1	37	20	17			23		$K = 3.11 \times 10^{-5}$
BA 13	2	5-10	Ċ			38	22	16					
050373				Barn	Burns & McDonnell	5							J-1-2-1

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Barns & McDonnell Engineer-Architects-Comutants

Project	Project <u>MPS</u> I aboratory F	<mark>S - Borrow Area</mark> KCTL		MMARY	SUMMARY OF SOIL TESTS	TESTS					Project No. Date Ja	o. <u>73-062-1-005</u> January 1977	
BER ING	ІВЕВ РГЕ	DEPTH	CLASSIFICATION	> ;		AT	ATTERBERG LIMITS	g	UNCONFINED	UNCONFINED	5 (1	PERMEABILITY CM/SEC	TY
ROR	MA2 MUN	ELEVATION		%	PCF.	LL	٦٢	F	TSF	Е %	>%		
BA 14	4	15-20	CL			38	22	16					
BA 15	1	0-5	CL		94.2	32	22	10			21	K = 2.10 x	10-5
BA 15	4	15-20	CL			35	21	14					
BA 16		0-5	cr			33	23	10					
BA 16	4	15-20	CL			40	22	18					
BA 17	2	5-10	CL		99.4	36	19	17			21	K = 2.11 =	10_5
050373					Burns & MCDonnell Engineers-Architects-Consultants	R							J-1-2-1

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		s,			╱ _{┝╴┣╶┝┝} ┥╴┤ ┥╴┠╶╞╾┥╴┥	┥╇╍╄╌┦┈┥╺┽╌╽ ┿╋╼┿┿╅╺┿╍┝╼┨	┥┥	╴╻╌╏╶ ┧╌┝╴┥ ╼┝╍┠ ━━╋╼╋╋╋╋╋	$\frac{1}{1}$	
		TONS/SQ FT	<u></u> ↓ - ↓ - ↓	41	·↓·↓·↓·↓·↓·↓·	╶╁╸╂╸┠╸┨╶╂┉╂╼┠ ╴┨╴┫╺┾╴┨╺┼╸┽╵┪	╼╅╍╉╴╋ ╴╈╴┢╼┥	╴┝╍╁╴┾╸┧╍┽╸╄╍╋ ╴╷╷╎╶┾╶┥╌┽╼┿┍╋		
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٥	🛛 Controlled-strain									
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		🛛 Undistur	hed				1	T	· ·	
1y1	e of specimen	Remolded	r		t No.	Test No.		Test No.	Test No.	
	Water content		v 0	3(0.2%		%	%		%
Initial	Void ratio		e _o							
Ĩ'n	Saturation		s _o		%		%	%		%
	Dry density, lb/cu	ft	γ _d	8	2.1					
	e to failure, min		^t f							
Unc t	onfined compressive ons/sq ft	strength,	qu	0	.3/					
Und	rained shear strengt	h, tons/sq ft	^s u							
Ser	sitivity ratio	•	^S t							
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LL	57.7	PL /9.7			PI 🗦	38.0		G _s		
	cimen cm Spe	ight /3.28-4	m	Projec		SOURI		······		
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Sketch of specimen after failure (<u>TEST TYPE</u> (Check one) Controlled-stress						
C	, 	-	AXL	L STRAIN, ϵ ,	, %	
Type of specimen SUndis	turbed	l Te	est No.	L STRAIN, ¢, Test No.	Test No.	Test No.
Type of specimen SUndis Remol Water content	turbed ded	1 Te 70 4	<u></u>			Test No. ¢
Type of specimen SUndis Remol Water content Void ratio	turbed ded w	Te To To	est No. 1.4 \$	Test No. 4	Test No.	%
Type of specimen S Undis Remol Water content Void ratio Saturation	turbed ded w e	I Te	rst No. 1.4 % %	Test No.	Test No.	
Type of specimen SUndis Water content Void ratio Saturation Dry density, lb/cu ft	turbed ded e S 7	4 Te 70 4 0	est No. 1.4 \$	Test No. 4	Test No.	%
Type of specimen SUndia Water content Void ratio Saturation Dry density, lb/cu ft Pime to failure, min Dronfined compressive strength,	turbed ded v e S 7 t	Te o 4	rst No. 1.4 % %	Test No. 4	Test No.	%
Type of specimen S Undis Water content Remol Water content Saturation Dry density, lb/cu ft Dry density, lb/cu ft Prime to failure, min Inconfined compressive strength, tons/sq ft	turbed ded y e S 7 t t	Te o 4 o o	rst No. 1.4 % % 77.4	Test No. 4	Test No.	%
Type of specimen S Undis Water content Image: Remol Water content Image: Remol	turbed ded y e S 7 t t g ft	i Te	rst No. 1.4 % % 77.4	Test No. 4	Test No.	%
Type of specimen SUndis Water content Void ratio Saturation Dry density, lb/cu ft Fime to failure, min Inconfined compressive strength, tons/sq ft Indrained shear strength, tons/sq Sensitivity ratio	turbed ded y e S 7 t t g ft	Te o 4 o - d - f - u C	rst No. 1.4 % % 77.4	Test No. 4	Test No.	%
Type of specimen Undis Remol Water content Void ratio Saturation Dry density, lb/cu ft Pime to failure, min Inconfined compressive strength, tons/sq ft Indrained shear strength, tons/sq Sensitivity ratio Classification $\subset H$ PL 24.0	turbed ded v e S ft ft s	Te o 4 o - d - f - u C	<pre>st No. 1.4 \$ 77.4 2.30</pre>	Test No. 4	Test No.	%
Type of specimen S Undis Remol Water content Void ratio Saturation Dry density, lb/cu ft Time to failure, min Jnconfined compressive strength, tons/sq ft Jndrained shear strength, tons/sq Sensitivity ratio Classification CH LL C.S. PL 24.0 Specimen cm Specimen	turbed ded y e S 7 t t c ft S cm [i Te o 4 o 7 d 7 u C	PI 3	Test No. * * /. <u>2</u>	Test No. %	5
Type of specimen S Undis Remol Water content Void ratio Saturation Dry density, lb/cu ft Time to failure, min Jnconfined compressive strength, tons/sq ft Jndrained shear strength, tons/sq Sensitivity ratio Classification CH LL C.S. PL 24.0 Specimen cm Specimen	turbed ded y e S 7 t t c ft S cm [i Te o 4 o 7 d 7 u C	PI 2	Test No. %	Test No. % % G ₅ Job No	5
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Type of specimen S Undis Water content Remol Water content Saturation Dry density, lb/cu ft Saturation Dry density, lb/cu ft Inconfined compressive strength, tons/sq ft Indrained shear strength, tons/sq Sensitivity ratio Classification CH LL Specimen Inam 7.23	turbed ded y e S 7 t t c ft S cm [a Te	PI 2 PI 2	Test No.	Test No. % % G ₅ Job No	5 5 5 7- 4

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BURNS & MCDONNELL ENGINEERING COMPANY

FORM J-1-17C

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ļ	Sketch of specimen after failure <u>TEST TYPE</u> (Check one) Controlled-stress	COMPRESSIVE STRESS, ¢, TONS/SQ FT					
	🔀 Controlled-strain	0	/	2 AXIA	L ŠTRAIN, E,	, % ⁵	6
Ty	pe of specimen	🖸 Undistur	bed	Test No.	Teat No.	Test No.	The at
Ту	pe of specimen	S Undistur Remolded	.	Test No.	Test No.	Test No.	
	pe of specimen Water content Void ratio	Undistur Remolded	₩0	Test No. 29.4 %	Test No. %		Test %
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	Water content Void ratio	Remolded	₩ ₀ e ₀	29.4 \$ \$			
H Initial	Water content Void ratio Saturation Dry density, lb/cu ft me to failure. min	Remolded	r≱o eo So	29.4 \$	¢		%
d H Initial	Water content Void ratio Saturation Dry density, lb/cu ft	Remolded	ν _o e _o S _o γ _d	29.4 \$ \$	¢		%
Initial	Water content Void ratio Saturation Dry density, lb/cu ft me to failure, min confined compressive st	Remolded	v _o e _o S _o γ _d t _f	29.4 \$ \$ 93.1	¢		%
un Initial	Water content Void ratio Saturation Dry density, lb/cu ft me to failure, min confined compressive st tons/sq ft	Remolded	$ \begin{bmatrix} w_{0} \\ e_{0} \\ S_{0} \\ 7_{d} \\ t_{f} \\ q_{u} $	29.4 \$ \$ 93.1	¢		%
Initial Du Se	Water content Void ratio Saturation Dry density, lb/cu ft me to failure, min confined compressive st tons/sq ft drained shear strength,	Remolded	ν e S γ t q s	29.4 \$ \$ 93.1	¢		%
Initial Initial	Water content Void ratio Saturation Dry density, lb/cu ft me to failure, min confined compressive st tons/sq ft drained shear strength, nsitivity ratio assification	□ Remolded rength, tons/sq ft	ν _o eo S _o γ _d t _f α _u S _u S _t	29.4 \$ \$ 93.1	¢		%
Initial Initial	Water content Void ratio Saturation Dry density, lb/cu ft me to failure, min confined compressive st tons/sq ft drained shear strength, nsitivity ratio assification P ecimen cm Speci	<pre> Remolded rength, tons/sq ft rel</pre>	ν _o e _o S _o γ _d t _f q _u S _u S _t	29.4 \$ \$ 93.1 0.4.2	\$ \$	G _S	%
Du Du Du Du U Du U Du U Du U Du U Du U	Water content Void ratio Saturation Dry density, lb/cu ft me to failure, min confined compressive st tons/sq ft drained shear strength, nsitivity ratio assification P ecimen cm Speci	E Remolded	ν _o e _o S _o γ _d t _f q _u S _u S _t	29.4 \$ \$ 93./ 0.43 PI roject N:	\$ \$	G _s	%
Du Du Du Du U Du U Du U Du U Du U Du U	Water content Void ratio Saturation Dry density, lb/cu ft me to failure, min confined compressive st tons/sq ft drained shear strength, nsitivity ratio assification P ecimen cm Speci am 7.24 in. Heigh	E Remolded	Wo eo So 7d tr qu Su St	29.4 \$ \$ 93./ 0.45 PI PI Troject M: 7/1/2, rea	\$ \$ 155041 (1555)		%
Initial Du Du Du Un Se LL	Water content Void ratio Saturation Dry density, lb/cu ft me to failure, min confined compressive st tons/sq ft drained shear strength, nsitivity ratio assification P ecimen cm Speci am 7.24 in. Heigh	E Remolded	$ \begin{array}{c} \mathbf{w}_{0} \\ \mathbf{e}_{0} \\ \mathbf{s}_{0} \\ \mathbf{r}_{1} \\ \mathbf{q}_{1} \\ \mathbf{s}_{1} \\ \mathbf{s}_{1} \\ \mathbf{s}_{2} \\ \mathbf{s}_{2} \\ \mathbf{s}_{3} \\ \mathbf{s}_{4} \\ \mathbf{s}_{4} \\ \mathbf{s}_{5} \\ \mathbf{s}_{6} \\ s$	29.4 \$ \$ 93.1 0.4.2 PI PI PI	* * /* /:::::::::::::::::::::::::::::::	G ₅ 	2 2

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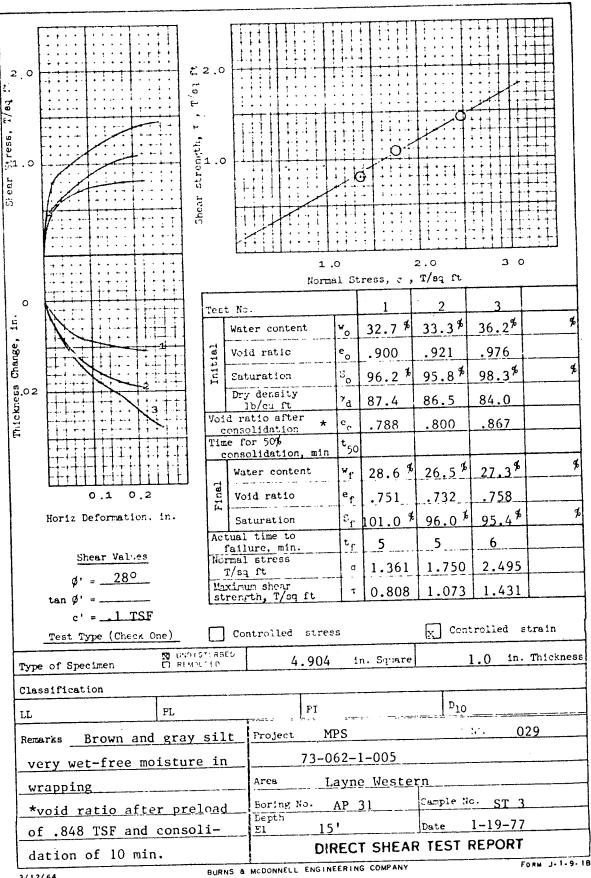
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		Void ratio e .840	.800 .882
	Initia	Cuturation 50 71.0 *	81.4 \$ 65.2 \$
		Dry density Deven ft 74 90.3	92.3 88.3
	E	a ratio after <u>ecolidation</u> * ^c e .804 e for 50% t	.765 .860
		onsolidation, min 50	
	0.1 0,2		24.8 [‡] 24.5 [¢] [¢]
	Horiz Teformation, in.		.701 .749
		$\begin{array}{c c} \text{Saturation} & \text{S}_{1} & 89.4 \\ \hline \text{ual time to} & \\ \hline \text{allure, min.} & \text{t}_{1} & 6 \\ \end{array}$	93.7 [*] 86.7 [*] [*] 6 6.5
	Shear variaes Ne:	tal stress /c1 ft = 1.068	1.581 2.127
	y = y	inu chorn	1.109 1.607
	c' =		
	50 1 M (4 5 1 - H (4		X Controlled strain
	Type of Specimen Distance Classification ML	4.904 in Spare	1.0 in. Thickness
	$\begin{array}{c} \text{Classification} & 1012 \\ \text{LL} & 30.3 \\ \text{HL} & 27.7 \end{array}$	FT 2.6	D ₁₀
	Remarks _ Grayish brown clay		::. 029
	silt with numerous wood	73-062-1-005	
	fragments	Area Layne Western	
	*void ratio after preload	Foring No. AP 31	ample No. ST 2
	of .554 TSF and consoli-		ate 1-19-77
	dation of 10 min.	DIRECT SHEAR	TEST REPORT

3/12/64

BURNS & MCDONNELL ENGINEERING COMPANY



	mul Streps, c . T/og St
H 22 Anter centent	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Yoid ratio	°o .842 .775 .768
	³ 0 51.6 ¹ 55.4 ⁴ 56.2 ¹ ⁴
2 3. <u>3.</u> <u>3./ea.rt</u>	<u>'4 90.2 93.6 93.9</u>
S Dry density Q Dry density Dry density Dry density	°c .813 .761 .761
.01 Time for 50% consolidation, min	
Water content	Y: 27.0 1 27.2 1 25.7 4 1
0,1 0.2 Void ratio	f .820 .768 .747
Horiz Deformation, in. Enturation	°: 87.3 ^t 93.9 ^t 91.2 ^t t
Actual time to Shear Values Normal stress	t _f .4 36
$\frac{1}{340}$	
tan \$' = Maximum shear strength, T/sq ft	- 0.517 0.893 1.280
$c' = \frac{0.5}{0.5}$	
Test Type (Check (ne) Controlled stre	ss X Controlled strain
Type of Specimen CLERN (190) 4.904	in. Opare 1.0 in. Thickness
Classification ML	
LL 25.0 FL 25.0 FT	<i>O p</i> ₁₀
	MPS 029
Inclaring Indi offic	.062-1-005
	ayne Western
	AP 36 Congle Se. ST 1
(Lort)	
	ft. Date 1-5-77
Di	RECT SHEAR TEST REPORT

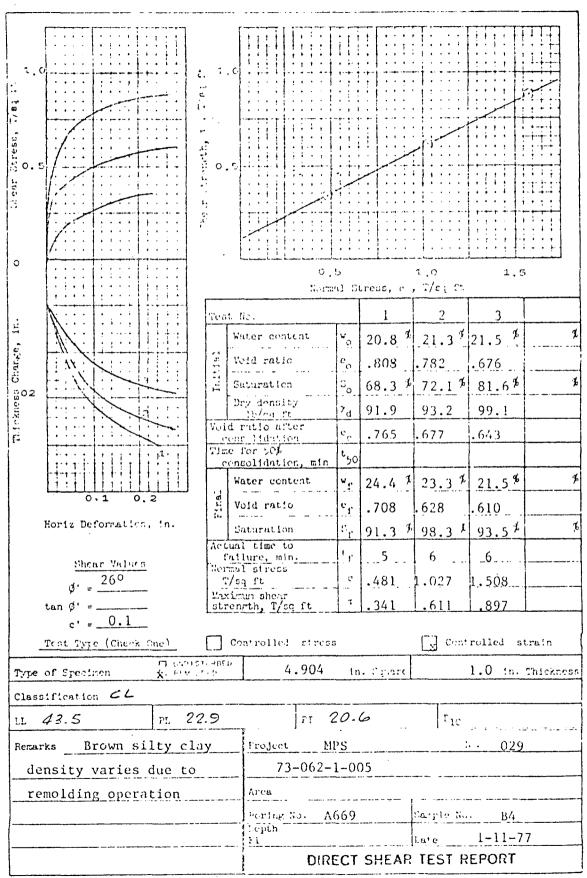
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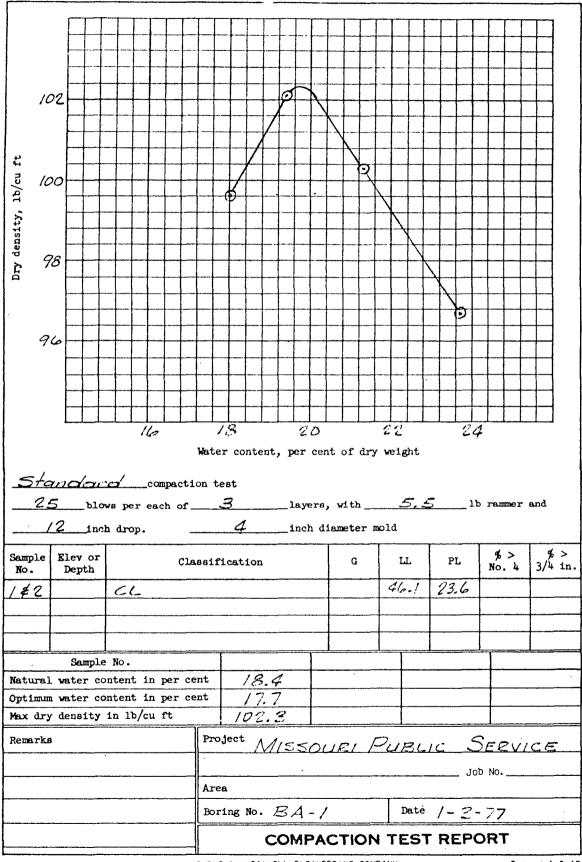
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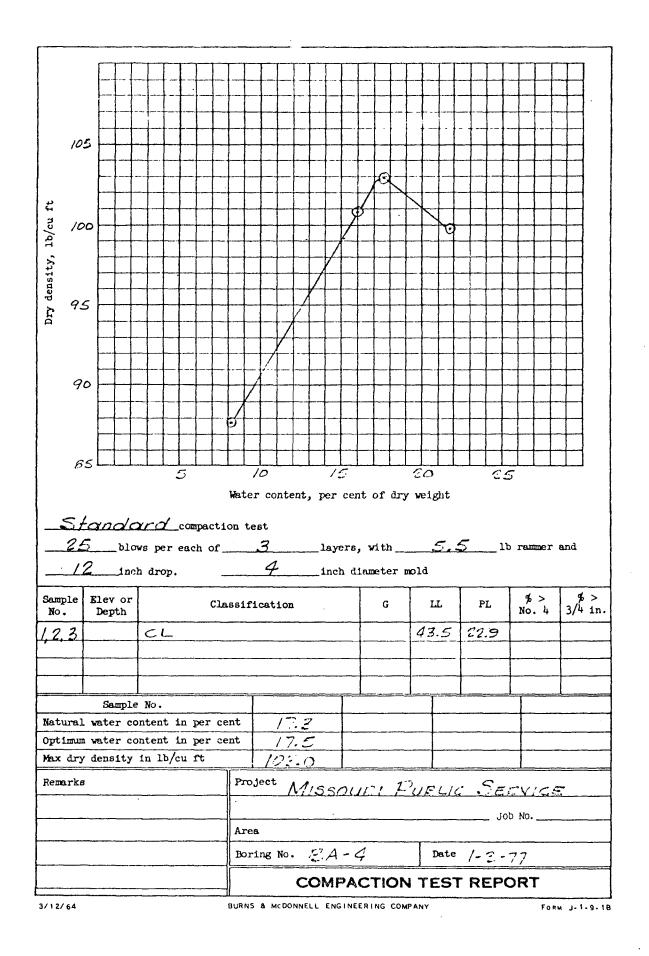
FORM J-1-9-18

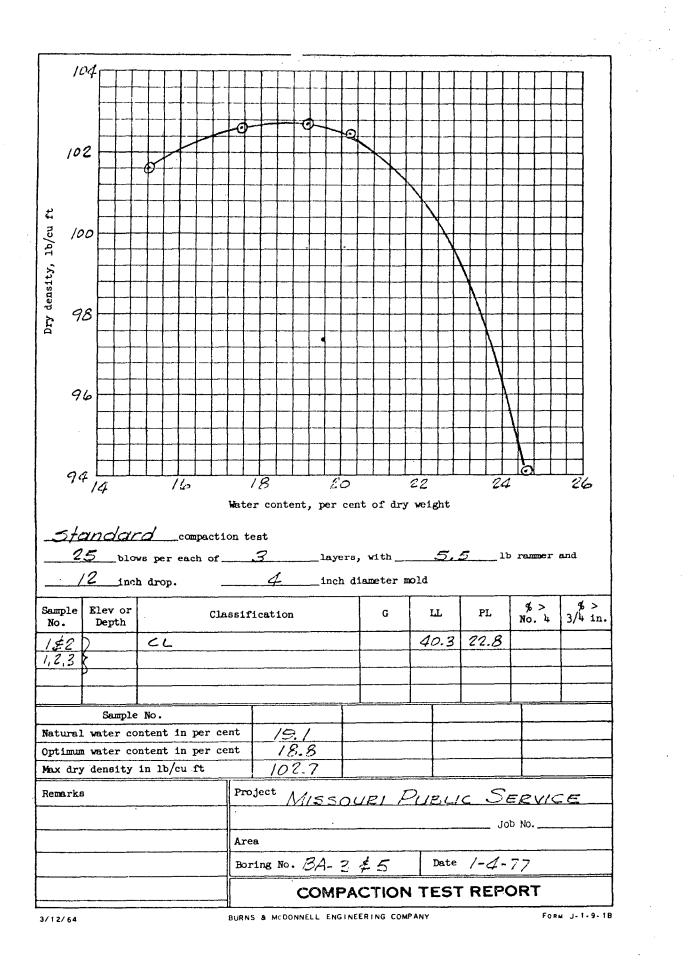


3/12/64

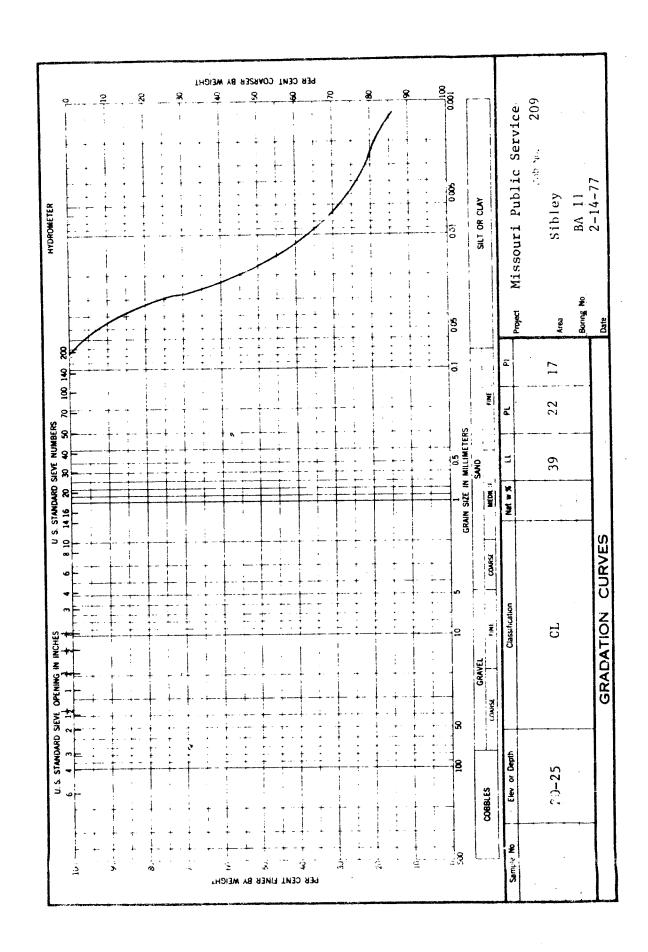
BURNS & MCDONNELL ENGINEERING COMPANY

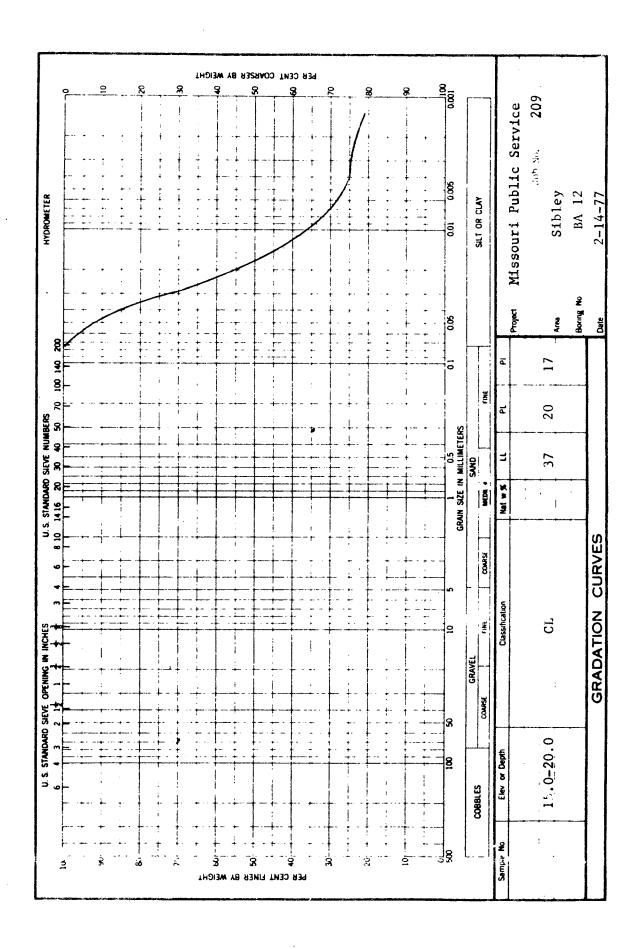
FORM J-1-9-18



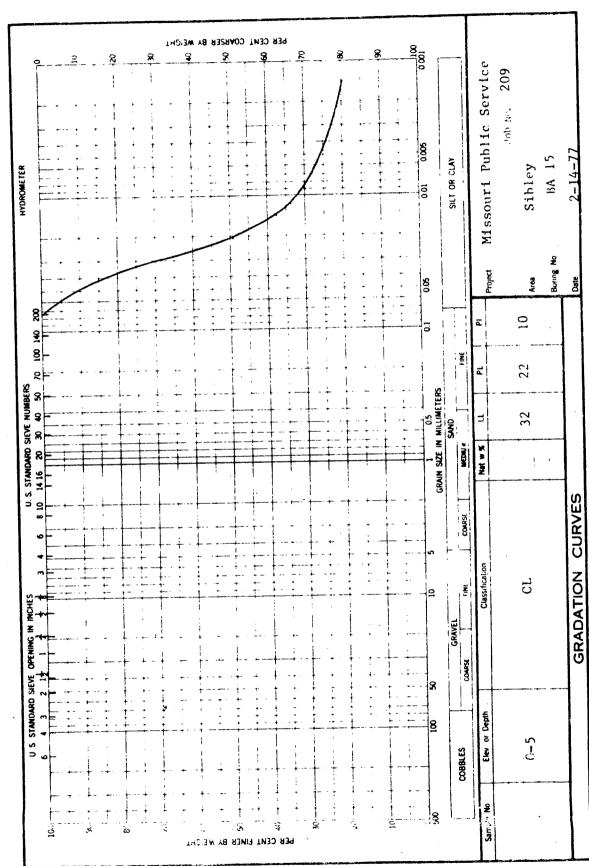


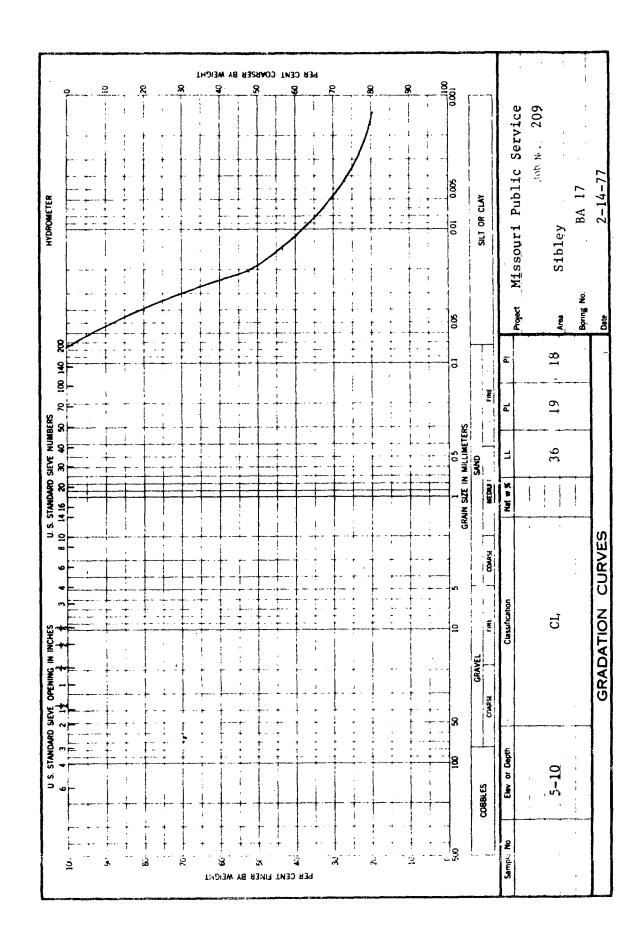
KANSAS CITY TESTING LABORATORY





KANSAS CITY TESTING LABORATORY





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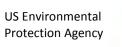
Site Name:	Sibley Generating Station	Date:	22 Sept 2010
Unit Name:	Fly Ash Pond	Operator's Name:	Kansas City Power and Light
Unit I.D.:		Hazard Potential Classification:	High 🗌 Significant 🗌 Low 🔀
	Inspector's Name:	Michael McLaren, Andrew Cue	eto

Check the appropriate box below. Provide comments when appropriate. If not applicable or not available, record "N/A". Any unusual conditions or construction practices that should be noted in the comments section. For large diked embankments, separate checklists may be used for different embankment areas. If separate forms are used, identify approximate area that the form applies to in comments.

	Yes	No	7	Yes	No
1. Frequency of Company's Dam Inspections?	X weekly		18. Sloughing or bulging on slopes?		х
2. Pool elevation (operator records)?	X		19. Major erosion or slope deterioration?		Х
3. Decant inlet elevation (operator records)?	Х		20. Decant Pipes:		
4. Open channel spillway elevation (operator records)?	n/a		Is water entering inlet, but not exiting outlet?		Х
5. Lowest dam crest elevation (operator records)?	725′		Is water exiting outlet, but not entering inlet?		Х
6. If instrumentation is present, are readings recorded (operator records)?		х	Is water exiting outlet flowing clear?	Х	
7. Is the embankment currently under construction?		х	21. Seepage (specify location, if seepage carries fines, and approximate seepage rate below):		
8. Foundation preparation (remove vegetation, stumps, topsoil in area where embankment fill will be placed)?	х		From underdrain?		х
9. Trees growing on embankment? (If so, indicate largest diameter below)		х	At isolated points on embankment slopes?		х
10. Cracks or scarps on crest?		Х	At natural hillside in the embankment area?		Х
11. Is there significant settlement along the crest?		Х	Over widespread areas?		Х
12. Are decant trashracks clear and in place?		N/A	From downstream foundation area?		Х
13. Depressions or sinkholes in tailings surface or whirlpool in the pool area?		х	"Boils" beneath stream or ponded water?		х
14. Clogged spillways, groin or diversion ditches?		N/A	Around the outside of the decant pipe?		Х
15. Are spillway or ditch linings deteriorated?		N/A	22. Surface movements in valley bottom or on hillside?		х
16. Are outlets of decant or underdrains blocked?		х	23. Water against downstream toe?		х
17. Cracks or scarps on slopes?		х	24. Were Photos taken during the dam inspection?	х	

Major adverse changes in these items could cause instability and should be reported for further evaluation. Adverse conditions noted in these items should normally be described (extent, location, volume, etc.) in the space below and on the back of this sheet.

Comments





Coal Combustion Waste (CCW)

Impoundment Inspection

Impoundment NPD	ES Permit	n/a		INSPECTOR	Michael McLaren, Andrew Cueto							
Impoundme	Date ent Name	22 Sept 2010 Fly Ash Pond										
Impoundment EP	Company PA Region											
(Field Office Name of Impo	undment	Missouri Department of Natural Resources										
<u> </u>	mpouname	·	e jorm unde	r the same imp	oounament NPI	DES Permit numi	ber)					
ls v IMPOUND Nearest D	•	ICTION: Settli m Town Be:		into the	Yes	N D	_					
im Location:	poundmen	t:										
Longitude	39	DEG	10	MIN	34.06	SEC	w					
Latitude	94	DEG	10	MIN	36.52	SEC	N					
State MO County JACKSON												
Doe	es a state a	gency regulate If So V	this impour Vhich State		Yes Ssouri Departm	N nent of Natural F						



<u>HAZARD POTENTIAL</u> (In the event the impoundment should fail, the following would

occur):

LESS THAN LOW HAZARD POTENTIAL: Failure or misoperation of the dam results in no probable loss of human life or economic or environmental losses.

 \square

LOW HAZARD POTENTIAL: Dams assigned the low hazard potential classification are those where failure or misoperation results in no probable loss of human life and low economic and/or environmental losses. Losses are principally limited to the owner's property.

SIGNIFICANT HAZARD POTENTIAL: Dams assigned the significant hazard potential classification are those dams where failure or misoperation results in no probable loss of human life but can cause economic loss, environmental damage, disruption of lifeline facilities, or can impact other concerns. Significant hazard potential classification dams are often located in predominantly rural or agricultural areas but could be located in areas with population and significant infrastructure.



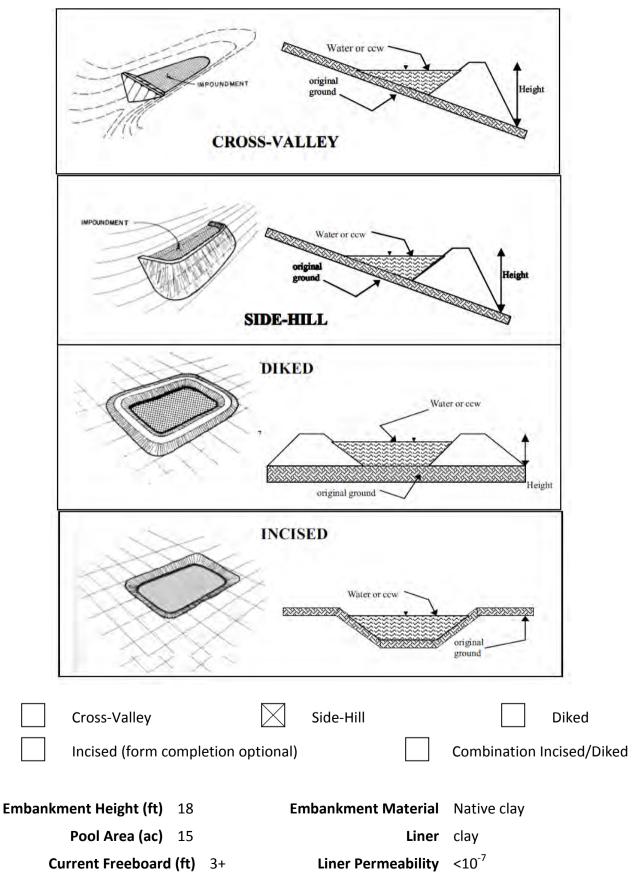
HIGH HAZARD POTENTIAL: Dams assigned the high hazard potential classification are those where failure or misoperation will probably cause loss of human life.

DESCRIBE REASONING FOR HAZARD RATING CHOSEN:

Pond would spill into Missouri River and be contained within the River's storage. There would be little to no environmental damage.

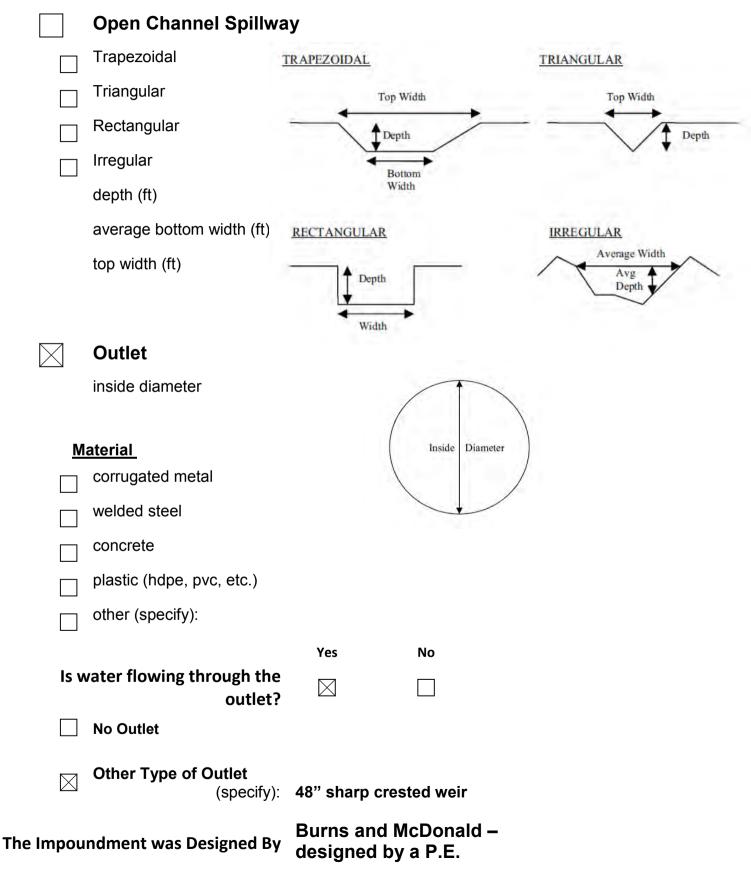


CONFIGURATION:





TYPE OF OUTLET (Mark all that apply)





	Yes	No
Has there ever been a failure at this site?		\square



	Yes	No
Has there ever been significant seepages at this site?		

	Yes	No
Has there ever been any measures undertaken to monitor/lower Phreatic water table levels based		
on past seepages or breaches at this site?		\boxtimes
If so, which method (e.g., piezometers, gw pumping,)?		



ADDITIONAL INSPECTION QUESTIONS

Concerning the embankment foundation, was the embankment construction built over wet ash, slag, or other unsuitable materials? If there is no information just note that.

No. Pond embankment was structurally designed and keyed into native soils that were cleared and grubbed.

Did the dam assessor meet with, or have documentation from, the design Engineer-of-Record concerning the foundation preparation?

Drawings were provided from Engineer-of-Record.

From the site visit or from photographic documentation, was there evidence of prior releases, failures, or patchwork on the dikes?

No.



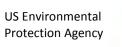
Site Name:	Sibley Generating Station	Date:	22 Sept 2010
Unit Name:	Slag Settling Pond	Operator's Name:	Kansas City Power and Light
Unit I.D.:		Hazard Potential Classification:	High Significant Low
	Inspector's Name:	Michael McLaren, Andrew Cue	eto

Check the appropriate box below. Provide comments when appropriate. If not applicable or not available, record "N/A". Any unusual conditions or construction practices that should be noted in the comments section. For large diked embankments, separate checklists may be used for different embankment areas. If separate forms are used, identify approximate area that the form applies to in comments.

	Yes	No	7	Yes	No
1. Frequency of Company's Dam Inspections?	X weekly		18. Sloughing or bulging on slopes?		х
2. Pool elevation (operator records)?	X		19. Major erosion or slope deterioration?		Х
3. Decant inlet elevation (operator records)?	Х		20. Decant Pipes:		
4. Open channel spillway elevation (operator records)?	r	n/a	Is water entering inlet, but not exiting outlet?		Х
5. Lowest dam crest elevation (operator records)?	7	24′	Is water exiting outlet, but not entering inlet?		Х
6. If instrumentation is present, are readings recorded (operator records)?		х	Is water exiting outlet flowing clear?	х	
7. Is the embankment currently under construction?		х	21. Seepage (specify location, if seepage carries fines, and approximate seepage rate below):		
8. Foundation preparation (remove vegetation, stumps, topsoil in area where embankment fill will be placed)?	х		From underdrain?		х
9. Trees growing on embankment? (If so, indicate largest diameter below)		х	At isolated points on embankment slopes?		х
10. Cracks or scarps on crest?		Х	At natural hillside in the embankment area?		Х
11. Is there significant settlement along the crest?		Х	Over widespread areas?		Х
12. Are decant trashracks clear and in place?		N/A	From downstream foundation area?		Х
13. Depressions or sinkholes in tailings surface or whirlpool in the pool area?		х	"Boils" beneath stream or ponded water?		х
14. Clogged spillways, groin or diversion ditches?		N/A	Around the outside of the decant pipe?		Х
15. Are spillway or ditch linings deteriorated?		N/A	22. Surface movements in valley bottom or on hillside?		х
16. Are outlets of decant or underdrains blocked?		х	23. Water against downstream toe?		х
17. Cracks or scarps on slopes?		х	24. Were Photos taken during the dam inspection?	х	

Major adverse changes in these items could cause instability and should be reported for further evaluation. Adverse conditions noted in these items should normally be described (extent, location, volume, etc.) in the space below and on the back of this sheet.

Issue #	Comments
1	Pond is incised into ground
2	
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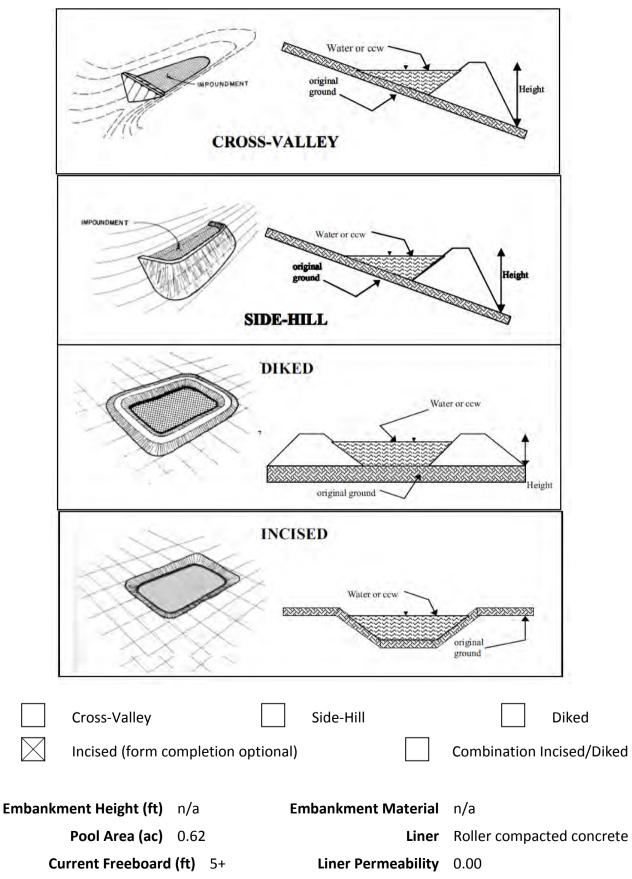
Coal Combustion Waste (CCW)

Impoundment Inspection

Impoundment NPDES Permit	n/a		INSPECTOR	Michael McL	aren, Andrew	Cueto
Date Impoundment Name	22 Sept 2010 Slag Settling					
Impoundment Company EPA Region	Kansas City I Region 7	Power an	d Light			
State Agency (Field Office) Address Name of Impoundment (Report each impoundme		ng Station	Slag Settling P	ond	DES Permit num	ber)
New 🖂	Update		,			,
Is impound	ment currently u w currently bein		into the	Yes	N D	_
IMPOUNDMENT FUR	NCTION: Settlin	g Pond				
Nearest Downstrea Nam	Wellin	gton, MO				
Distance f impoundmen						
Location:						
Longitude 39	DEG	10	MIN	44.37	SEC	w
Latitude 94	DEG	11	MIN	10.01	SEC	Ν
State MO			County JACk	SON		
				Yes	N	0
Does a state a	gency regulate t	his impour	ndment?	\boxtimes]
	If So W	hich State	Agency? Mis	ssouri Departm	ent of Natural F	lesources



CONFIGURATION:





HAZARD POTENTIAL (In the event the impoundment should fail, the following would occur):

N/A **LESS THAN LOW HAZARD POTENTIAL:** Failure or misoperation of the dam results in no probable loss of human life or economic or environmental losses.

LOW HAZARD POTENTIAL: Dams assigned the low hazard potential classification are those where failure or misoperation results in no probable loss of human life and low economic and/or environmental losses. Losses are principally limited to the owner's property.

SIGNIFICANT HAZARD POTENTIAL: Dams assigned the significant hazard potential classification are those dams where failure or misoperation results in no probable loss of human life but can cause economic loss, environmental damage, disruption of lifeline facilities, or can impact other concerns. Significant hazard potential classification dams are often located in predominantly rural or agricultural areas but could be located in areas with population and significant infrastructure.



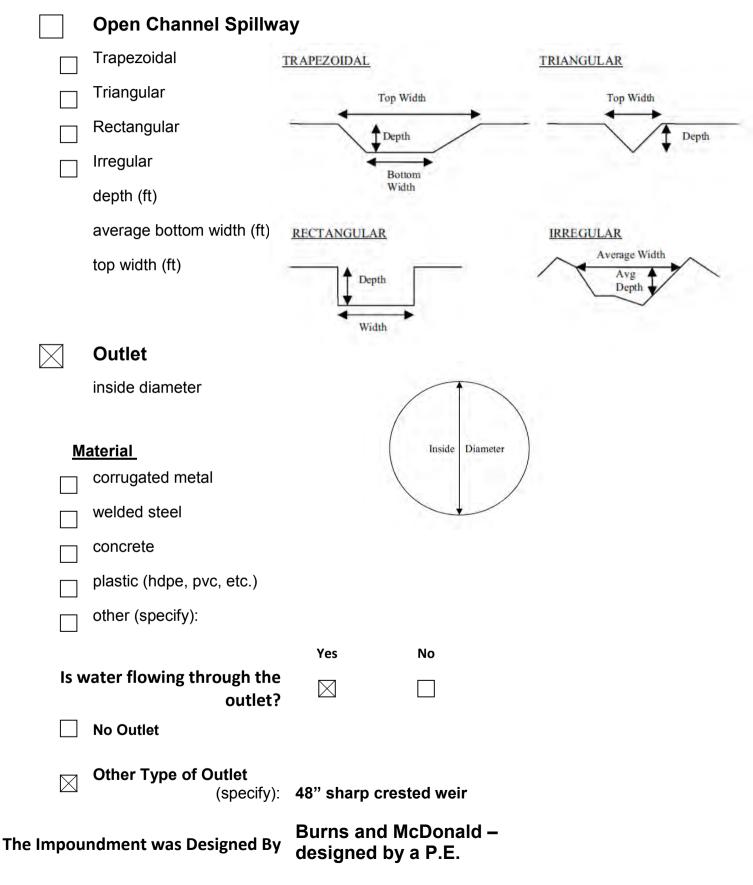
HIGH HAZARD POTENTIAL: Dams assigned the high hazard potential classification are those where failure or misoperation will probably cause loss of human life.

DESCRIBE REASONING FOR HAZARD RATING CHOSEN:

Pond is incised into ground and concrete lined.



TYPE OF OUTLET (Mark all that apply)





	Yes	No
Has there ever been a failure at this site?		\square



	Yes	No
Has there ever been significant seepages at this site?		

	Yes	No
Has there ever been any measures undertaken to monitor/lower Phreatic water table levels based		
on past seepages or breaches at this site?		\boxtimes
If so, which method (e.g., piezometers, gw pumping,)?		



ADDITIONAL INSPECTION QUESTIONS

Concerning the embankment foundation, was the embankment construction built over wet ash, slag, or other unsuitable materials? If there is no information just note that.

No. Pond was incised into bank.

Did the dam assessor meet with, or have documentation from, the design Engineer-of-Record concerning the foundation preparation?

Drawings were provided from Engineer-of-Record.

From the site visit or from photographic documentation, was there evidence of prior releases, failures, or patchwork on the dikes?

No.